STORMWATER REPORT

THORNDIKE PLACE DOROTHY ROAD ARLINGTON, MA

NOVEMBER 2020 REVISED: JUNE 2021

Owner/Applicant:

ARLINGTON LAND REALTY LLC 84 Sherman Street, 2nd Floor Cambridge, MA 02140

BSC Job Number: 23407.00

Prepared by:



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SECTION 1.0

PROJECT INFORMATION



1.01 PROJECT DESCRIPTION

Arlington Realty, LLC (The Applicant) is seeking to construct a new age restricted multi-family housing and assisted living development in Arlington, Massachusetts, hereinafter referred to as "the Project." The total property area is approximately 17.66 acres and is located off Dorothy Road near the intersection with Littlejohn Street. The project is bounded on the north by Dorothy Road, on the east by residential properties and Thorndike Field, and bounded on the south and west by Concord Turnpike (Route 2).

The Project consists of clearing and grubbing of the northwest section of the property and construction of one 4-story assisted living residential building with a lower level parking garage, six duplex townhouses with covered carports, as well as surface parking, walkways, utility services, and a stormwater management system. The buildings have a combined footprint of approximately 43,100 square feet.

The Project is designed to comply with the Massachusetts General Laws (M.G.L.) Chapter 40B, which allows developers to override certain aspects of municipal zoning bylaws by providing a certain percentage of affordable housing, as well as the Department of Environmental Protection's Stormwater Management Standards. There are wetland resource areas in the south, west and east portions of the property. The Project is concentrated in the northwest area of the property and minimizes impacts to the 100-foot wetland buffer zones, which are regulated by the Arlington Wetlands Bylaw as Adjacent Upland Resource Areas (AURA's). Part of the site is located within the 1% Chance Annual Flood as defined by FEMA which is regulated under the Wetlands Protection Act and the Arlington Wetlands Bylaw as Bordering Land Subject to Flooding (BLSF). Compensatory flood storage is proved at a 2:1 ratio as described in section 2.12 below.

1.02 PRE-DEVELOPMENT CONDITIONS

The existing site topography generally slopes southeast across the property towards the wetlands located on the property with slopes ranging from 0-15%. The current site is comprised of forest and the primary soil classification identified by the NRCS Web Soil Survey is udorthents (655), which accounts for the majority of the property and all of the project area. On November 25, 2020, BSC Group conducted three test pits on the site, the locations of which are noted on the Grading and Drainage plan, and the test pit logs are attached in Appendix D. The test pits consisted primarily of fill material to a depth of 9-11 feet generally conforming with the soils mapping. Even though the material was fill, all samples textured as sandy loam in test pits TP-1 and TP-2, closest to the proposed stormwater management systems. At the bottom of test pit TP-3, a layer of clay material was found. Based on the fill materials found, runoff calculations have been performed using curve numbers corresponding to Hydrologic Soil Group (HSG) C.

The existing site being largely undeveloped has no existing drainage facilities and the majority of the stormwater runoff is directed to the wetlands on the property. A small portion of the site discharges to the north to Dorothy Road.

1.03 Post-Development Conditions

The proposed stormwater management system has been designed in a manner that will meet or exceed the provisions of the Department of Environmental Protection (DEP) Stormwater Management Standards for a new construction project. The design is also in conformance the with Town of Arlington Zoning Bylaws.

Stormwater runoff from a portion of the 4-story building (approximately 15,900 square feet) will be temporarily detained on the roof of the building. This collected runoff will be released at controlled rates through roof drains to an underground infiltration system in the adjacent driveway and drop-off area. The majority of the 4-sotry building roof (approximately 16,800 square feet) will discharge at grade directly to the surface and flow overland towards the wetlands to the south.

Stormwater runoff from the site driveway and small parking/drop-off area at the main entrance to the building will be collected via a deep sump catch basin, conveyed through a water quality unit before being directed to the underground infiltration system. Stormwater runoff from the driveway into the garage below the building will be collected via a



trench drain and conveyed through a water quality unit before being directed to the underground system. Due to its elevation difference, this leg of the system has been provided with backflow preventer device. In addition, runoff from the townhouse and carport roofs, as well as the landscaped areas between the townhouses and 4-story building will be collected and routed to the underground infiltration area. This underground infiltration system provides for recharge to groundwater and provides peak flow rate attenuation. In larger storm events, this system will overflow through an outlet control structure to a flared end section with a rip-rap apron to the south.

Stormwater runoff from the townhouse driveways along Dorothy Rd will be collected via individual trench drains and routed to small underground infiltration chamber systems beneath each driveway. Each system is designed to completely hold and infiltrate the 100-yr, 24-hour rain event.

Although all soils sampled in test pits TP-1 and TP-2 were identified as sandy loam (see above), the infiltration rate for loam (0.52-inches per hour) has been used in the infiltration system design to account for the materials found being primarily fill. Based upon the test pit data performed in November 2020 (see above), the estimated seasonal high groundwater elevation ranges between elevations 0 and 2. As such the infiltration systems have been set with a bottom elevation of 6.0 and higher to provide the minimum 2-feet of clearance above groundwater and account for any groundwater fluctuations that may occur.

To provide emergency access to the sides and rear of the building, a reinforced grass access lane will be installed. A portion of this access lane will include a 6-foot wide, porous asphalt walkway to allow residents to have ADA/AAB accessible access the rear of the site. Both the reinforced grass and porous asphalt will allow stormwater runoff to freely infiltrate back to the ground and will result in negligible runoff.

Specifics of the project's compliance with the Stormwater Standards are discussed in detail in the following sections.



SECTION 2.0

DRAINAGE SUMMARY



2.01 Stormwater Standard 1 – New Stormwater Conveyances

Per Massachusetts Stormwater Management Standard #1, no new outfalls may discharge untreated stormwater directly to or cause erosion in wetlands or waters of the Commonwealth. No new untreated stormwater discharges are proposed. Rip-rap outlet protection sizing calculations are included in Section 6.0 of this Report.

2.02 Stormwater Standard 2 – Stormwater Runoff Rates

Watershed modeling was performed using HydroCAD Stormwater Modeling Software version 10.00, a computer aided design program that combines SCS runoff methodology with standard hydraulic calculations. A model of the site's hydrology was developed for both pre- and post-development conditions to assess the effects of the proposed development on the project site and surrounding areas.

In accordance with previous peer review comments received from BETA Group, Inc. dated March 4, 2021, and to account for impacts from climate change, stormwater runoff was modeled using data from the NOAA 14+ rainfall data. In accordance with BETA Group's letter, the following rainfall values have been used:

Storm Frequency	NOAA 14+ Rainfall (Inches)
2-year	3.64
10-year	5.79
25-year	7.49
50-year	8.72
100-year	10.35

As detailed in BETA Group's review letter, these values are greater than, in some cases significantly so, than the rainfall required by either the DEP's Stormwater Handbook or the Arlington Wetlands Bylaw.

The stormwater management system for the project has been designed such that the post-development conditions result in no increase to peak runoff rates off the property for the 2, 10, 25, 50, and 100-year, 24-hour storm events, as detailed in the table below.

Peak Flow Discharge Rates

Nodes 100L/100S - Total Flows

Storm Event	Pre-Development Peak Discharge Rate (cfs)	Post-Development Peak Discharge Rate (cfs)	Change in Peak Discharge Rate (cfs)
2-Year	3.0	2.9	-0.1
10-Year	7.7	5.7	-2.0
25-Year	11.8	8.6	-3.2
50-Year	15.0	11.8	-3.2
100-Year	19.2	15.9	-3.3

2.03 Stormwater Standard 3 – Groundwater Recharge

Groundwater recharge is provided on site via a large centralized underground structural infiltration system beneath the surface parking area to the north of the building, and smaller systems beneath each individual driveway of the duplex



townhouses. Overall, the project will result in no loss of annual recharge to groundwater as required by Standard 3. Refer to Section 6.0 of this Report for groundwater recharge information.

As the infiltration system has more than 2-feet but less than 4-feet separation to estimated seasonal high groundwater, a mounding analysis has been performed in accordance with the Hantoush Method to ensure that a groundwater mound does not extend into the bottom of the infiltration system preventing infiltration of the required recharge volume. This analysis is included in Section 6.0 of this Report.

2.04 Stormwater Standard 4 – TSS Removal

As a new development, the Project stormwater management system will achieve a TSS removal greater than 80%. The proposed stormwater management system has been designed to provide treatment of runoff in order to reduce suspended solids prior to discharge off-site through the implementation of the following best management practices:

- Deep Sump Hooded Catch Basins
- Proprietary Hydrodynamic Separators
- Underground Stormwater Infiltration Systems

The water quality volume is defined as the runoff volume requiring TSS Removal for the site, and is equal to 0.5-inches of runoff over the total impervious area of the post-development site. The required water quality volume for the project is provided in Section 6.0 of this Report

The underground infiltration system has been sized to treat the required water quality volume and calculations are included in Section 6.0 of this Report.

A long-term pollution prevention plan complying with the requirements of Standard 4 is included in Section 4.0 of this Report.

2.05 Stormwater Standard 5 – Land Uses with Higher Potential Pollutant Loads

This standard is not applicable as the project site is not a land use with higher potential pollutant loads (LUHPPL).

2.06 Stormwater Standard 6 – Stormwater Discharges to a Critical Area

This standard is not applicable as runoff from the project site does not discharge to a critical area.

2.07 Stormwater Standard 7 – Redevelopment Projects

This project is a new development and therefore has been designed to fully comply with the Stormwater Management Standards.

2.08 Stormwater Standard 8 – Sedimentation and Erosion Control Plan

Erosion and sedimentation controls are shown on the Project Plans. Additionally, a Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan is included in Section 3.0 of this Report.

2.09 Stormwater Standard 9 – Long Term Operation and Maintenance Plan

A Long-Term Operation and Maintenance Plan is included in Section 4.0 of this Report.

2.10 Stormwater Standard 10 – Illicit Discharges

There are no known illicit discharges on the project site and none are proposed. An illicit discharge compliance statement is included in Section 6.0 and will be signed by the Applicant prior to issuance of any permits.



2.11 Conclusion

The project has been designed in accordance with DEP Stormwater Management Standards and the Town of Arlington Wetlands Protection Bylaw and Regulations. Through the construction of the aforementioned stormwater systems, the project will provide peak rate attenuation, TSS removal and groundwater recharge.

2.12 Compensatory Flood Storage

A portion of the project site is located within the 1% Chance Annual Flood as defined by FEMA, which is regulated under the Wetlands Protection Act and Arlington Wetlands Bylaw as Bordering Land Subject to Flooding (BLSF). In order to protect the values provided by BLSF and prevent downstream flooding impacts, the project is required to provide compensatory flood storage on a 1-foot incremental basis to match whatever is lost due to the project's development. Further, Arlington requires compensatory flood storage to be provided at a 2 to 1 ratio for any flood storage lost. In order to provide this compensatory flood storage, the project will minimize the area of BLSF impacted and regrade a portion of the project property southeast of the proposed building as shown on the Plans. A breakdown of the flood storage impacts and compensatory storage provided is shown below:

Elevations	Existing Incremental Available Flood Storage (CU.FT.)	Incremental Available Flood Storage with No Compensatory Storage (CU.FT.)	Incremental Flood Storage Change w/No Compensatory Storage (CU.FT.)	Proposed Incremental Compensatory Storage (CU.FT.)	Ratio of Compensatory Storage to Storage Lost
5.0 - 6.0	67.0	0.0	-67.0	144.5	2.2
6.0 - 6.8	7,454.0	4,806.8	-2,647.2	5,990.0	2.3

As shown above, the project will exceed the 2 to 1 ratio of compensatory flood storage for all flood storage lost due to the project development. In addition, as shown on the Plans, the proposed compensatory storage is hydrologically connected to the flood plain impacted by the project. Therefore, the project as proposed meets the applicable requirements for BLSF in both the Wetlands Protection Act and the Arlington Wetlands Bylaw and Regulations.



SECTION 3.0

CONSTRUCTION PERIOD POLLUTION PREVENTION AND EROSION AND SEDIMENTATION CONTROL PLAN

3.0 CONSTRUCTION PERIOD POLLUTION PREVENTION AND EROSION AND SEDIMENTATION CONTROL PLAN

This Section specifies requirements and suggestions for implementation of a Stormwater Pollution Prevention Plan (SWPPP) for **Thorndike Place**, in Arlington, Massachusetts. The SWPPP shall be provided and maintained on-site by the Contractor(s) during all construction activities. The SWPPP shall be updated as required to reflect changes to construction activity.

The stormwater pollution prevention measures contained in the SWPPP shall be at least the minimum required by Local Regulations. The Contractor shall provide additional measures to prevent pollution from stormwater discharges in compliance with the National Pollution Discharge Elimination System (NPDES) Phase II permit requirements and all other local, state and federal requirements.

The SWPPP shall include provisions for, but not be limited to, the following:

- 1. Construction Trailers
- 2. Lay-down Areas
- 3. Equipment Storage Areas
- 4. Stockpile Areas
- Disturbed Areas

The Contractor shall NOT begin construction without submitting evidence that a NPDES Notice of Intent (NOI) governing the discharge of stormwater from the construction site for the entire construction period has been filed at least fourteen (14) days prior to construction. It is the Contractor's responsibility to complete and file the NOI, unless otherwise determined by the project team.

The cost of any fines, construction delays and remedial actions resulting from the Contractor's failure to comply with all provisions of local regulations and Federal NPDES permit requirements shall be paid for by the Contractor at no additional cost to the Owner.

As a requirement of the EPA's NPDES permitting program, each Contractor and Subcontractor responsible for implementing and maintaining stormwater Best Management Practices shall execute a Contractor's Certification form.

Erosion and Sedimentation Control

The Contractor shall be solely responsible for erosion and sedimentation control at the site. The Contractor shall utilize a system of operations and all necessary erosion and sedimentation control measures, even if not specified herein or elsewhere, to minimize erosion damage at the site to prevent the migration of sediment into environmentally sensitive areas. Environmentally sensitive areas include all wetland resource areas within, and downstream of, the site, and those areas of the site that are not being altered.

Erosion and sedimentation control shall be in accordance with this Section, the design drawings, and the following:

- □ "National Pollutant Discharge Elimination System General Permit for Discharges from Construction Activities (EPA Construction General Permit February 16, 2017).
- ☐ Massachusetts Stormwater Management Policy Handbook issued by the Massachusetts Department of Environmental Protection, January 2008.
- ☐ Massachusetts Erosion and Sediment Control Guidelines for Urban and Suburban Areas, A Guide for Planners, Designers and Municipal Officials, March 1997.

The BMP's presented herein should be used as a guide for erosion and sedimentation control and are <u>not</u> intended to be considered specifications for construction. The most important BMP is maintaining a rapid



construction process, resulting in prompt stabilization of surfaces, thereby reducing erosion potential. Given the primacy of rapid construction, these guidelines have been designed to allow construction to progress with essentially no hindrance by the erosion control methods prescribed. These guidelines have also been designed with sufficient flexibility to allow the Contractor to modify the suggested methods as required to suit seasonal, atmospheric, and site-specific physical constraints.

Another important BMP is the prevention of concentrated water flow. Sheet flow does not have the erosive potential of a concentrated rivulet. These guidelines recommend construction methods that allow localized erosion control and a system of construction, which inhibits the development of shallow concentrated flow. These BMP's shall be maintained throughout the construction process.

CONTACT INFORMATION AND RESPONSIBLE PARTIES

The following is a list of all project-associated parties:

Owner

Arlington Land Realty, LLC 84 Sherman Street, 2nd Floor Cambridge, MA 02140

Contractor

To be determined

Environmental Consultant

BSC Group, Inc. 803 Summer Street Boston, MA 02127

Contact: Dominic Rinaldi, P.E.

Phone: (617) 896-4300

Email: drinaldi@bscgroup.com

Qualified SWPPP Inspectors

To Be Determined

3.1 Procedural Conditions of the Construction General Permit (CGP)

The following list outlines the Stormwater Responsibilities for all construction operators working on the Project. The operators below agree through a cooperative agreement to abide by the following conditions throughout the duration of the construction project, effective the date of signature of the required SWPPP. These conditions apply to all operators on the project site.

The project is subject to EPA's NPDES General Permit through the CGP. The goal of this permit is to prevent the discharge of pollutants associated with construction activity from entering the existing and proposed storm drain system or surface waters.

All contractors/operators involved in clearing, grading and excavation construction activities must sign the appropriate certification statement required, which will remain with the SWPPP. The owner must also sign a certification, which is to remain with the SWPPP in accordance with the signatory requirements of the SWPPP.



Once the SWPPP is finalized, a signed copy, plus supporting documents, must be held at the project site during construction. A copy must remain available to EPA, State and Local agencies, and other interested parties during normal business hours.

The following items associated with this SWPPP must be posted in a prominent place at the construction site until final stabilization has been achieved:

- The completed/submitted NOI form
- Location where the public can view the SWPPP during normal business hours
- A copy of the signed/submitted NOI, permit number issued by the EPA and a copy of the current CGP.

Project specific SWPPP documents are not submitted to the US EPA unless the agency specifically requests a copy for review. SWPPP documents requested by a permitting authority, the permitee(s) will submit it in a timely manner.

EPA inspectors will be allowed free and unrestricted access to the project site and all related documentation and records kept under the conditions of the permit.

The permitee is expected to keep all BMP's and Stormwater controls operating correctly and maintained regularly.

Any additions to the project which will significantly change the anticipated discharges of pollutants, must be reported to the EPA. The EPA should also be notified in advance of any anticipated events of noncompliance. The permitee must also orally inform the EPA of any discharge, which may endanger health or the environment within 24 hours, with a written report following within 5 days.

In maintaining the SWPPP, all records and supporting documents will be compiled together in an orderly fashion. Inspection reports and amendments to the SWPPP must remain with the document. Federal regulations require permitee(s) to keep their Project Specific SWPPP and all reports and documents for at least three (3) years after the project is complete.

3.2 Existing Site and Soil Conditions

The total project area is approximately 17.66 acres and is located off Dorothy Road. The project is bounded on the north by Dorothy Road, bounded on the east by residential properties, and bounded on the south and west by Concord Turnpike (Route 2).

The current site is comprised of forest and the primary soil classification identified by the NRCS Web Soil Survey is udorthents (655), which accounts for the majority of the property and all of the project area. On November 25, 2020, BSC Group conducted three test pits on the site, the locations of which are noted on the Grading and Drainage plan, and the test pit logs are attached in Appendix D. The test pits consisted of primarily fill material to a depth of 9-11 feet generally conforming with the soils mapping. Even though the material was fill, it all samples textured as sandy loam in test pits TP-1 and TP-2, closest to the proposed stormwater management systems. At the bottom of test pit TP-3, a layer of clay material was found. Based on the fill materials found, runoff calculations have been performed using curve numbers corresponding to Hydrologic Soil Group (HSG) C.

3.3 Project Description and Intended Construction Sequence

The site is currently comprised of woods. The proposed activities will include the following major components:

• The construction of one (1) multi-family housing building and six (6) duplex townhouses with associated parking, driveways, walkways, and retaining walls,



- The construction of stormwater management systems, and
- Site grading and compensatory flood storage creation, and
- Utility connections and installation.

The proposed project will disturb a total of approximately 131,000± S.F. (3.01± acres).

Soil disturbing activities will include site demolition, installing stabilized construction exits, installation of erosion and sedimentation controls, grading, storm drain inlets, stormwater management systems, utilities, building foundation, construction of site driveways and preparation for final landscaping. Please refer to Table 1 for the projects anticipated construction timetable. A description of BMP's associated with project timetable and construction-phasing elements is provided in this Erosion and Sediment Control Plan.

Table 1 – Anticipated Construction Timetable

Construction Phasing Activity	Anticipated Timetable
Grubbing and Stripping of Limits of	To be determined
Construction Phase	
Rough Site Grading and Site Utilities	To be determined
Utility Plan Construction	To be determined
Landscaping	To be determined

3.4 Potential Sources of Pollution

Any project site activities that have the potential to add pollutants to runoff are subject to the requirements of the SWPPP. Listed below are a description of potential sources of pollution from both sedimentation to Stormwater runoff, and pollutants from sources other than sedimentation.

Table 2 - Potential Sources of Sediment to Stormwater Runoff

Table 2 – Potential Sources of Sediment to Stormwater Runoff				
Potential Source	Activities/Comments			
Construction Site Entrance and	Vehicles leaving the site can track soils onto public			
Site Vehicles	roadways. Site Vehicles can readily transport exposed soils			
	throughout the site and off-site areas.			
Grading Operations	Exposed soils have the potential for erosion and discharge of			
	sediment to off-site areas.			
Material Excavation, Relocation,	Stockpiling of materials during excavation and relocation of			
and Stockpiling	soils can contribute to erosion and sedimentation. In			
	addition, fugitive dust from stockpiled material, vehicle			
	transport and site grading can be deposited in wetlands and			
	waterway.			
Landscaping Operations	Landscaping operations specifically associated with exposed			
	soils can contribute to erosion and sedimentation.			
	Hydroseeding, if not properly applied, can runoff to adjacent			
	wetlands and waterways.			

Table 3 - Potential Pollutants and Sources, other than Sediment to Stormwater Runoff

Potential Source	Activities/Comments
Staging Areas and Construction	Vehicle refueling, minor equipment maintenance, sanitary
Vehicles	facilities and hazardous waste storage
Materials Storage Area	General building materials, solvents, adhesives, paving
	materials, paints, aggregates, trash, etc.



Construction Activities	Construction, paving, curb/gutter installation, concrete
	pouring/mortar/stucco

3.5 Erosion and Sedimentation Control Best Management Practices

All construction activities will implement Best Management Practices (BMP's) in order to minimize overall site disturbance and impacts to the sites natural features. Please refer to the following sections for a detailed description of site specific BMP's. In addition, an Erosion and Sedimentation Control Plan is provided in the Site Plans.

3.6 Timetable and Construction Phasing

This section provides the Owner and Contractor with a suggested order of construction that shall minimize erosion and the transport of sediments. The individual objectives of the construction techniques described herein shall be considered an integral component of the project design intent of each project phase. The construction sequence is not intended to prescribe definitive construction methods and should not be interpreted as a construction specification document. However, the Contractor shall follow the general construction phase principles provided below:

- Protect and maintain existing vegetation wherever possible.
- Minimize the area of disturbance.
- To the extent possible, route unpolluted flows around disturbed areas.
- Install mitigation devices as early as possible.
- Minimize the time disturbed areas are left unstabilized.
- Maintain siltation control devices in proper condition.
- The contractor should use the suggested sequence and techniques as a general guide and modify
 the suggested methods and procedures as required to best suit seasonal, atmospheric, and site
 specific physical constraints for the purpose of minimizing the environmental impact of
 construction.

Demolition, Grubbing and Stripping of Limits of Construction Phase

- Install Temporary Erosion Control (TEC) devices as required to prevent sediment transport into resource areas.
- Place a ring of silt socks and/or haybales around stockpiles.
- Stabilize all exposed surfaces that will not be under immediate construction.
- Store and/or dispose all pavement and building demolition debris as indicated in accordance with all applicable local, state, and federal regulations.

Driveway Area Sub-Base Construction

- Install temporary culverts and diversion ditches and additional TEC devices as required by individual construction area constraints to direct potential runoff toward detention areas designated for the current construction phase.
- Compact gravel as work progresses to control erosion potential.
- Apply water to control air suspension of dust.
- Avoid creating an erosive condition due to over-watering.
- Install piped utility systems as required as work progresses, keeping all inlets sealed until all downstream drainage system components are functional.

Binder Construction

• Fine grade gravel base and install processed gravel to the design grades.



- Compact pavement base as work progresses.
- Install pavement binder coat starting from the downhill end of the site and work toward the top.

Finish Paving

- Repair and stabilize damaged side slopes.
- Clean inverts of drainage structures.
- Install final top coat of pavement.

Final Clean-up

- Clean inverts of culverts and catch basins.
- Remove sediment and debris from rip-rap outlet areas.
- Remove TEC devices only after permanent vegetation and erosion control has been fully established.

3.7 Site Stabilization

Grubbing Stripping and Grading

- Erosion control devices shall be in place as shown on the design plans before grading commences.
- Stripping shall be done in a manner, which will not concentrate runoff. If precipitation is expected, earthen berms shall be constructed around the area being stripped, with a silt sock, silt fence or haybale dike situated in an arc at the low point of the berm.
- If intense precipitation is anticipated, silt socks, haybales, dikes and /or silt fences shall be used as required to prevent erosion and sediment transport. The materials required shall be stored on site at all time.
- If water is required for soil compaction, it shall be added in a uniform manner that does not allow excess water to flow off the area being compacted.
- Dust shall be held at a minimum by sprinkling exposed soil with an appropriate amount of water.

Maintenance of Disturbed Surfaces

- Runoff shall be diverted from disturbed side slopes in both cut and fill.
- Mulching may be used for temporary stabilization.
- Silt sock, haybale or silt fences shall be set where required to trap products of erosion and shall be maintained on a continuing basis during the construction process.

Loaming and Seeding

- Loam shall not be placed unless it is to be seeded directly thereafter.
- All disturbed areas shall have a minimum of 4" of loam placed before seeded and mulched.
- Consideration shall be given to hydro-mulching, especially on slopes in excess of 3 to 1.
- Loamed and seeded slopes shall be protected from washout by mulching or other acceptable slope protection until vegetation begins to grow.

Stormwater Collection System Installation

- The Stormwater drainage system shall be installed from the downstream end up and in a manner which will not allow runoff from disturbed areas to enter pipes.
- Excavation for the drainage system shall not be left open when rainfall is expected overnight. If left open under other circumstances, pipe ends shall be closed by a staked board or by an equivalent method.



• All catch basin openings shall be covered by a silt bag between the grate and the frame or protected from sediment by silt fence surrounding the catch basin grate.

Completion of Paved Areas

- During the placement of sub-base and pavement, the entrance to the Stormwater drainage systems shall be sealed when rain is expected. When these entrances are closed, consideration must be given to the direction of run-off and measures shall be undertaken to minimize erosion and to provide for the collection of sediment.
- In some situations, it may be necessary to keep catch basins open.
- Appropriate arrangements shall be made downstream to remove all sediment deposition.

Stabilization of Surfaces

- Stabilization of surfaces includes the placement of pavement, rip-rap, wood bark mulch and the establishment of vegetated surfaces.
- Upon completion of construction, all surfaces shall be stabilized even though it is apparent that future construction efforts will cause their disturbance.
- Vegetated cover shall be established during the proper growing season and shall be enhanced by soil adjustment for proper pH, nutrients and moisture content.
- Surfaces that are disturbed by erosion processes or vandalism shall be stabilized as soon as possible.
- Areas where construction activities have permanently or temporarily ceased shall be stabilized within 14 days from the last construction activity, except when construction activity will resume within 21 days (e.g., the total time period that construction activity is temporarily ceased is less than 21 days).
- Hydro-mulching of grass surfaces is recommended, especially if seeding of the surfaces is required outside the normal growing season.
- Hay mulch is an effective method of temporarily stabilizing surfaces, but only if it is properly secured by branches, weighted snow fences or weighted chicken wire.

3.8 Temporary Structural Erosion Control Measures

Temporary erosion control measures serve to minimize construction-associated impacts to wetland resource and undisturbed areas. Please refer to the following sections for a description of temporary erosion control measures implemented as part of the project and this sample SWPPP.

3.8.1 Silt Socks, Havbales, and Silt Fencing

The siltation barriers will demarcate the limit of work, form a work envelope and provide additional assurance that construction equipment will not enter the adjacent wetlands or undisturbed portions of the site. All barriers will remain in place until disturbed areas are stabilized.

3.8.2 Temporary Stormwater Diversion Swale

A temporary diversion swale is an effective practice for temporarily diverting stormwater flows and to reduce stormwater runoff velocities during storm events. The swale channel can be installed before infrastructure construction begins at the site, or as needed throughout the construction process. The diversion swale should be routinely compacted or seeded to minimize the amount of exposed soil.

3.8.3 Dewatering Basins

Dewatering may be required during stormwater system, foundation construction and utility installation. Should the need for dewatering arise, groundwater will be pumped directly into a temporary settling basin, which will act as a sediment trap during construction. All temporary settling basins will be located within close proximity of daily work activities. Prior to discharge, all groundwater will be treated by means of the



settling basin or acceptable substitute. Discharges from sediment basins will be free of visible floating, suspended and settleable solids that would impair the functions of a wetland or degrade the chemical composition of the wetland resource area receiving ground or surface water flows and will be to the combined system.

3.8.4 Material Stockpiling Locations

Piping and trench excavate associated with the subsurface utility work will be contained with a single row of silt socks and/or haybales.

3.9 Permanent Structural Erosion Control Measures

Permanent erosion control measures serve to minimize post-construction impacts to wetland resource areas and undisturbed areas. Please refer to the Site Plans and Long-Term Operations and Maintenance Plan for a description of permanent erosion control measures implemented as part of the project and this SWPPP.

3.10 Good Housekeeping Best Management Practices

3.10.1 Street Sweeping

Dorothy Road in front of the project property shall be swept clean on a daily basis of any soils tracked onto it from the project site. All sweepings shall be disposed of off-site in accordance with all applicable laws and regulations.

3.10.2 Material Handling and Waste Management

Solid waste generation during the construction period will be primarily construction debris. The debris will include scrap lumber (used forming and shoring pallets and other shipping containers), waste packaging materials (plastic sheeting and cardboard), scrap cable and wire, roll-off containers (or dumpsters) and will be removed by a contract hauler to a properly licensed landfill. The roll-off containers will be covered with a properly secured tarp before the hauler exits the site. In addition to construction debris, the construction work force will generate some amount of household-type wastes (food packing, soft drink containers, and other paper). Trash containers for these wastes will be located around the site and will be emptied regularly so as to prevent wind-blown litter. This waste will also be removed by a contract hauler.

All hazardous waste material such as oil filters, petroleum products, paint and equipment maintenance fluids will be stored in structurally sound and sealed shipping containers in the hazardous-materials storage area and segregated from other non-waste materials. Secondary containment will be provided for all materials in the hazardous materials storage area and will consist of commercially available spill pallets. Additionally, all hazardous materials will be disposed of in accordance with federal, state and municipal regulations.

Two temporary sanitary facilities (portable toilets) will be provided at the site in the combined staging area. The toilets will be away from a concentrated flow path and traffic flow and will have collection pans underneath as secondary treatment. All sanitary waste will be collected from an approved party at a minimum of three times per week.

3.10.3 Building Material Staging Areas

Construction equipment and maintenance materials will be stored at the combined staging area and materials storage areas. Silt fence will be installed around the perimeter to designate the staging and materials storage area. A watertight shipping container will be used to store hand tools, small parts and other construction materials.

Non-hazardous building materials such as packaging material (wood, plastic and glass) and construction scrap material (brick, wood, steel, metal scraps, and pine cuttings) will be stored in a separate covered



storage facility adjacent to other stored materials. All hazardous-waste materials such as oil filters, petroleum products, paint and equipment maintenance fluids will be stored in structurally sound and sealed containers under cover within the hazardous materials storage area.

Large items such as framing materials and stockpiled lumber will be stored in the open storage area. Such materials will be elevated on wood blocks to minimize contact with runoff.

The combined storage areas are expected to remain clean, well-organized and equipped with ample cleaning supplies as appropriate for the materials being stored. Perimeter controls such as containment structures, covers and liners will be repaired or replaced as necessary to maintain proper function.

3.10.4 Designated Washout Areas

Designated temporary, below-ground concrete washout areas will be constructed, as required, to minimize the pollution potential associated with concrete, paint, stucco, mixers etc. Signs will, if required, be posted marking the location of the washout area to ensure that concrete equipment operators use the proper facility. Concrete pours will not be conducted during or before an anticipated precipitation event. All excess concrete and concrete washout slurries from the concrete mixer trucks and chutes will be discharged to the washout area or hauled off-site for disposal.

3.10.5 Equipment/Vehicle Maintenance and Fueling Areas

Several types of vehicles and equipment will be used on-site throughout the project including graders, scrapers, excavators, loaders, paving equipment, rollers, trucks and trailers, backhoes and forklifts. All major equipment/vehicle fueling and maintenance will be performed off-site. A small, 20-gallon pickup bed fuel tank will be kept on-site in the combined staging area. When vehicle fueling must occur on-site, the fueling activity will occur in the staging area. Only minor equipment maintenance will occur on-site. Vehicular refueling or maintenance shall not be allowed within the Adjacent Upland Resource Area (AURA) or in any protected wetland resource areas as defined by the Town of Arlington Regulations for Wetland Protection. All equipment fluids generated from maintenance activities will be disposed of into designated drums stored on spill pallets. Absorbent, spill-cleanup materials and spill kits will be available at the combined staging and materials storage area. Drip pans will be placed under all equipment receiving maintenance and vehicles and equipment parked overnight.

3.10.6 Equipment/Vehicle Wash down Area

All equipment and vehicle washing will be performed off-site.

3.10.7 Spill Prevention Plan

A spill containment kit will be kept on-site in the Contractor's trailer and/or the designated staging area throughout the duration of construction. Should there be an accidental release of petroleum product into a resource area, the appropriate agencies will be immediately notified.

3.10.8 Inspections

Maintenance of existing and proposed BMP's to address stormwater management facilities during construction is an on-going process. The purpose of the inspections is to observe all sources of stormwater or non-stormwater discharge as identified in the SWPPP as well as the status of the receiving waters and fulfill the requirements of the Order of Conditions. The following sections describe the appropriate inspection measures to adequately implement the project's SWPPP. A blank inspection form is provided at the end of this section. Completed inspection forms are to be maintained on site.



Inspection Personnel

The owner's appointed representative will be responsible for performing regular inspections of erosion controls and ordering repairs as necessary.

Inspection Frequency

Inspections will be performed by qualified personnel once every 7 days, in accordance with the CGP. The inspections must be documented on the inspection form provided at the end of this section, and completed forms will be provided to the on-site supervisor and maintained at the Owner's office throughout the entire duration of construction.

Inspection Reporting

Each inspection report will summarize the scope of the inspection, name(s) and qualifications of personnel making the inspection, and major observations relating to the implementation of the SWPPP, including compliance and non-compliance items. Completed inspection reports will remain with the completed SWPPP on site.

3.10.9 Amendment Requirements

The final SWPPP is intended to be a working document that is utilized regularly on the construction site, and provides guidance to the Contractor. It must reflect changes made to the originally proposed plan and will be updated to include project specific activities and ensure that they are in compliance with the NPDES General Permit and state and local laws and regulations. It should be amended whenever there is a change in design, construction, operation or maintenance that affects discharge of pollutants. The following items should be addressed should an amendment to the SWPPP occur:

- Dates of certain construction activities such as major grading activities, clearing and initiation of and completion of stabilization measures should be recorded.
- Future amendments to the SWPPP will be recorded as required. As this SWPPP is amended, all amendments will be kept on site and made part of the SWPPP.
- Upon completion of site stabilization (completed as designed and/or 70% background vegetative cover), it can be documented and marked on the plans. Inspections are no longer required at this time.
- Inspections often identify areas not included in the original SWPPP, which will require the SWPPP to be amended. These updates should be made within seven days of being recognized by the inspector.

3.11 SWPPP Inspection and Maintenance Report

The following form is an example to be used for SWPPP Inspection Reporting.



Stormwater Construction Site Inspection and Maintenance Report

TO BE COMPLETED AT LEAST EVERY 7 DAYS. AFTER SITE STABILIZATION, TO BE COMPLETED AT LEAST ONCE PER MONTH FOR THREE YEARS OR UNTIL A NOTICE OF TERMINATION IS FILED (IF APPLICABLE).

General Information						
Project Name	Thorndike I	Place				
NPDES Tracking No.		L	ocation	Dorothy Road		
(if applicable)				Arlington, MA		
Date of Inspection		S	tart/End Time			
Inspector's Name(s)						
Inspector's Title(s)						
Inspector's Contact Information						
Inspector's Qualifications						
Describe present phase of construction						
Type of Inspection: ☐ Regular ☐ Pre-storm event	☐ Durin	g storm event	☐ Post-storm e	vent		
		Weather Inform	nation			
Has there been a storm event since the last inspection? □Yes □No If yes, provide: Storm Start Date & Time: Storm Duration (hrs): Approximate Amount of Precipitation (in): Weather at time of this inspection? □ Clear □ Cloudy □ Rain □ Sleet □ Fog □ Snowing □ High Winds						
☐ Clear ☐ Cloudy ☐ Rain ☐ Sleet ☐ Fog ☐ Snowing ☐ High Winds ☐ Other: Temperature:						
Have any discharges occurred since the last inspection? □Yes □No If yes, describe:						
Are there any discharges at the time of inspection? Yes No If yes, describe:						
 many BMPs as necessary). Censure that you are inspecting. Describe corrective actions to Action Log. 	Carry a copy og 1g all required	f the numbered sit BMPs at your site	e map with you di e. ote the person that	your site map and list them below (add a uring your inspections. This list will tompleted the work in the Corrective		

	ВМР	BMP Installed?	BMP Maintenance Required?	Corrective Action Needed and Notes Action required by whom and when
1	Catch Basin Protection	□Yes □No	□Yes □No	

	ВМР	BMP Installed?	BMP Maintenance	Corrective Action Needed and Notes Action required by whom and when
2	Haybale & Silt Fencing	□Yes □No	Required? Yes No	
3	Straw Wattles	□Yes □No	□Yes □No	
4	Construction Entrance	□Yes □No	□Yes □No	
5	Sediment Basins	□Yes □No	□Yes □No	
6	Dewatering Pit	□Yes □No	□Yes □No	
7		□Yes □No	□Yes □No	

Overall Site Issues

Below are some general site issues that should be assessed during inspections. Customize this list as needed for conditions at your site.

	BMP/activity	Implemented?	Maintenance Required?	Corrective Action Needed and Notes Action required by whom and when
1	Are all slopes and disturbed areas not actively being worked properly stabilized?	□Yes □No	□Yes □No	
2	Are natural resource areas (e.g., streams, wetlands, mature trees, etc.) protected with barriers or similar BMPs?	□Yes □No	□Yes □No	
3	Are perimeter controls and sediment barriers adequately installed	□Yes □No	□Yes □No	

	BMP/activity	Implemented?	Maintenance Required?	Corrective Action Needed and Notes Action required by whom and when
	(keyed into substrate) and maintained?			
4	Are discharge points and receiving waters free of any sediment deposits?	□Yes □No	□Yes □No	
5	Are storm drain inlets properly protected?	□Yes □No	□Yes □No	
6	Is the construction exit preventing sediment from being tracked into the street?	□Yes □No	□Yes □No	
7	Is trash/litter from work areas collected and placed in covered dumpsters?	□Yes □No	□Yes □No	
8	Are washout facilities (e.g., paint, stucco, concrete) available, clearly marked, and maintained?	□Yes □No	□Yes □No	
9	Are vehicle and equipment fueling, cleaning, and maintenance areas free of spills, leaks, or any other deleterious material?	□Yes □No	□Yes □No	Vehicle Maintenance not allowed on site
10	Are materials that are potential stormwater contaminants stored inside or under cover?	□Yes □No	□Yes □No	
11	Are non-stormwater discharges (e.g., wash water, dewatering) properly controlled?	□Yes □No	□Yes □No	
12	(Other)	□Yes □No	□Yes □No	

Stormwater Report
Thorndike Place
Arlington, MA
Revised June 2021

Non-Compliance							
Describe any incidents of non-compliance not describe	ed above:						
CERTIF	TICATION STATEMENT						
accordance with a system designed to assure that qualifi Based on my inquiry of the person or persons who mana information, the information submitted is, to the best of	l attachments were prepared under my direction or supervision in ed personnel properly gathered and evaluated the information submitted. age the system, or those persons directly responsible for gathering the my knowledge and belief, true, accurate, and complete. I am aware that nation, including the possibility of fine and imprisonment for knowing						
Print name and title:							
(Qualified Person Performing the Inspection)							
Signature:	Date:						
Print name and title:							
(Contractor/Operator)							
Signatura	Data						
Signature:	Date:						

SECTION 4.0

LONG-TERM POLLUTION PREVENTION & OPERATION AND MAINTENANCE PLAN

4.0 Long-Term Pollution Prevention & Operation and Maintenance Plan

As required by Standard #4 of the Stormwater Management Policy, this Long-Term Pollution Prevention Plan has been developed for source control and pollution prevention at the site after construction.

MAINTENANCE RESPONSIBILITY

Ensuring that the provisions of the Long-Term Pollution Prevention Plan are followed will be the responsibility of The Applicant, Arlington Land Realty, LLC.

GOOD HOUSEKEEPING PRACTICES

The site to be kept clean of trash and debris at all times. Trash, junk, etc. is not to be left outside.

VEHICLE WASHING CONTROLS

The following BMP's, or equivalent measures, methods or practices are required if you are engaged in vehicle washing and/or steam cleaning:

It is allowable to rinse down the body or a vehicle, including the bed of a truck, with just water without doing any wash water control BMP's.

If you wash (with mild detergents) on an area that infiltrates water, such as gravel, grass, or loose soil, it is acceptable to let the wash water infiltrate as long as you only wash the body of vehicles.

However, if you wash on a paved area and use detergents or other cleansers, or if you wash/rinse the engine compartment or the underside of vehicles, you must take the vehicles to a commercial vehicle wash.

REQUIREMENTS FOR ROUTINE INSPECTIONS AND MAINTENANCE OF STORMWATER BMPS

All stormwater BMPs are to be inspected and maintain as follows;

Haybales, Silt Fence, and other temporary measures

The temporary erosion control measures will be installed up gradient of any wetland resource area where any disturbance or alteration might otherwise allow for erosion or sedimentation. They will be regularly inspected to ensure that they are functioning adequately. Additional supplies of these temporary measures will be stockpiled on site for any immediate needs or routine replacement.

Deep Sump Hooded Catch Basins

Regular maintenance is essential. Catch basins remain effective at removing pollutants only if they are cleaned out frequently. Inspect or clean basins at least four times per year and at the end of the foliage and snow removal seasons. Sediments must also be removed four times per year or whenever the depth of the deposits in the catch basin sump is greater than or equal to one half the depth from the bottom of the invert of the lowest pipe in the basin.

Water Quality Treatment Units

The water quality treatment structures require periodic inspection and cleaning to maintain operation and function. Owners should have these units inspected on a semi-annual basis and after periods of intense precipitation. Inspections can be done by using a clear Plexiglas tube ("sludge judge") to extract a water column sample. When sediment accumulation reaches 15% of storage capacity, cleaning of the unit is required.

These water quality structures must and will be checked and cleaned immediately after petroleum spills; contact appropriate regulatory agencies.

Maintenance of these units should be done by a vacuum truck that will remove the water, sediment, debris, floating hydrocarbons and other materials in unit. Proper cleaning and disposal of the removed materials and liquid must be followed.

Underground Infiltration System

Maintenance is required for the proper operation of the underground infiltration system. Infiltration systems are prone to failure due to clogging if the upstream water quality units are not maintained. The use of pretreatment BMPs will minimize failure and maintenance requirements.

After construction, the infiltration system shall be inspected after every major storm for the first few months to ensure proper stabilization and function. Water levels in the access ports shall be recorded over several days to check the drainage of the systems. It is recommended that a log book be maintained showing the depth of water in the detention/infiltration systems at each observation in order to determine the rate at which the system dewaters after runoff producing storm events. Once the performance characteristics of the detention/infiltration have been verified, the monitoring schedule can be reduced to an annual basis, unless the performance data suggests that a more frequent schedule is required.

Preventive maintenance on the infiltration system shall be performed at least twice a year, and sediment shall be removed from any and all pretreatment and collection structures. Sediment shall be removed when deposits approach within six inches of the invert heights of connecting pipes between unit rows, or in sumped inlet structures. Ponded water inside the systems (as visible from the access ports) that remains after several days most likely indicates that the bottom of the system is clogged and will require cleaning or replacement.

The system is designed with a defined top portal area at the "down-flow" end of the chamber that can be cut out to accept up to a 10-inch diameter riser pipe. The 10-inch riser can be used as an observation well and as access for a vacuum truck tube for use in removing sediment. The "down flow" ends of the units have end walls that are closed on the bottom. The closed bottom functions like a coffer dam, with most of the sediment depositing prior to flowing into the next chamber, facilitating its removal through the riser pipe, which is positioned directly above this area.

Pipe Outlet Protection

The outlet protection should be checked at least annually and after every major storm. If the rip-rap has been displaced, undermined or damaged, it should be repaired immediately. The channel immediately below the outlet should be checked to see that erosion is not occurring. The downstream channel should be kept clear of obstructions such as fallen trees, debris, and sediment that could change flow patterns and/or tailwater depths on the pipes. Repairs must be carried out immediately to avoid additional damage to the outlet protection apron.

PROVISIONS FOR MAINTENANCE OF LAWNS, GARDENS AND OTHER LANDSCAPE AREAS

Suggested Maintenance Operations

A. Trees and Shrubs

Disease and Pest Management - Prevention of disease or infestation is the first step of Pest Management. A plant that is in overall good health is far less susceptible to disease. Good general landscape maintenance can reduce problems from disease.

Inspections of plant materials for signs of disease or infestation are to be performed monthly by the Landscape Maintenance Contractor's Certified Arborist. This is a critical step for early diagnosis. Trees and Shrubs that have been diagnosed to have a plant disease or an infestation of insect pests are to be treated promptly with an appropriate material by a licensed applicator.

Fertilization - Trees and shrubs live outside their natural environment and should be given proper care to maintain health and vigor. Fertilizing trees and shrubs provides the plants with nutrients needed to resist insect attack, to resist drought and to grow thicker foliage. Fertilizing of new and old trees may be done in one of three ways, in either the early spring or the late fall.

• Systemic Injection of new and existing trees on trees 2 inches or greater in diameter. You must be licensed to apply this method.

- Soil Injection a liquid fertilizer with a product such as Arbor Green or Rapid Grow injected into the soil under the drip zone of a tree or shrub. Material must be used according to manufacturers' specifications to be effective. Outside contracting is recommended.
- Punch Bar Method a dry fertilizer such as 10-10-10, may be used by punched holes in the drip zone of the tree 12-18" deep, two feet apart around the circumference, to the edge of the drip line. Three pounds of fertilizer should be used per diameter inch for trees with trunks six inches or more in diameter.
- Fertilizer of shrubs use a fertilizer such as 10-10-10, broadcast over the planting area according to the manufacturers' rate and water in.
- All fertilization must be noted on daily maintenance log.

Watering - Trees and Shrubs will need supplemental watering to remain in vigorous health. All new plants need to be watered once a week in cool weather, twice a week during warm weather, and up to three times in a week during periods of extreme heat and drought. Trees and shrubs should be watered in such a manner as to totally saturate the soil in the root zone area. Over-watering or constant saturation of the soil must be avoided as this could lead to root rot and other disease problems. The use of a soil moisture meter can help you monitor the soil's water intake.

Plant Replacement - Unhealthy plants that may cause widespread infestation of other nearby plants shall be immediately removed from the site. Any vegetation removed from the site must be recorded and submitted with the daily maintenance log. The area shall be treated to prevent further infestation. The plant shall then be replaced with a healthy specimen of the same species and size. This work shall have a pre-established budget allowance for the year.

A spring inspection of all plant materials shall be performed to identify those plant materials that are not in vigorously healthy condition. Unhealthy plant materials shall be evaluated. If the problem is determined to be minor the plant material shall be given appropriate restorative care in accordance with this maintenance guideline until it is restored to a vigorously healthy condition. Unhealthy plant materials that do not respond to restorative care or are determined to be beyond saving shall be replaced with a healthy specimen of the same species and size. In the case of the necessity of replacing extremely large plant materials the Landscape Architect shall determine the size of the replacement plant.

Pruning - Proper pruning is the selective removal of branches without changing the plant's natural appearance, or habit of growth. All tree pruning is to be performed by a licensed Arborist. All branches that are dead, broken, scared or crossing should be removed. All cuts should be made at the collar and not cut flush with the base.

Pruning on the site shall be done for the following purposes;

- To maintain or reduce the size of a tree or shrub
- To remove dead, diseased or damaged branches
- To rejuvenate old shrubs and encourage new growth
- To stimulate future flower and fruit development
- To maximize the visibility of twig color
- To prevent damage and reduce hazards to people and properties

All shrubs are recommended to be pruned on an annual basis to prevent the shrub from becoming overgrown and eliminate the need for drastic pruning. There are several types of pruning for deciduous shrubs. Hand snips should be used to maintain a more natural look or hand shears can be used for a more formal appearance.

Winter Protection - All trees and shrubs are to be watered, fertilized, and mulched before the first frost. All stakes should be checked and ties adjusted. Damaged branches should be pruned.

Broadleaf and Coniferous Evergreen plant materials are to be sprayed with an anti-desiccant product to prevent winter burn. The application shall be repeated during a suitable mid-winter thaw.

Shrubs located in areas likely to be piled with snow during snow removal (but not designated as Snow Storage Areas) shall be marked by six-foot high poles with bright green banner flags. Stockpiles of snow are not to be located in these areas due to potential damage to the plant materials from both the weight of the snow and the snow melting chemicals.

At the fall landscape maintenance conference parameters will be discussed between the Landscape Maintenance Contractor and the snow removal contractor to assure minimal damage and loss of landscape amenities during the winter season.

Seasonal Clean Up - A thorough spring cleanup is to be performed. This includes the removal and replacement of dead or unhealthy plant materials and the cleanup of plant debris and any general debris that has accumulated over the winter season. Mulch is to be lightly raked to clean debris from the surface without removing any mulch. Twigs and debris are to be removed from the planting beds throughout the growing season.

Mulching - Planting beds shall be mulched with a treated shredded hardwood mulch free from dirt, debris, and insects. A sample of this mulch shall be given to the Owner for approval prior to installation.

Maintain a 2-3" maximum depth and keep free of weeds either by hand weeding or by the use of a pre-emergent weed control such as Treflan or Serfian. Seasonal re-mulching shall occur as necessary in the spring and the fall to maintain this minimum depth. When new mulch is added to the planting bed it shall be spread to create a total depth of no more than three inches. Edges should be maintained in a cleanly edged fashion.

Mulch shall not be placed directly against the trunk of any tree or shrub.

B. Groundcover and Perennials

Disease and Pest Management – Pesticides and herbicides should be applied only as problems occur, with the proper chemical applied only by a trained professional or in the case of pesticide, a Certified Pesticide Applicator. Plants should be monitored weekly and treated accordingly.

Fertilizer – The health of the plants can be maintained or improved, and their growth encouraged by an application of complete fertilizer. Apply a fertilizer such as 4-12-4 as growth becomes apparent and before mulching. Apply to all groundcover and perennial planting areas by hand and avoid letting the fertilizer come in contact with the foliage, or use a liquid fertilizer and apply by soaking the soil. Apply according to the manufacturers' specifications.

Fertilization shall stop at the end of July.

Water – Groundcovers and Perennials will need supplemental watering in order to become established, healthy plants. All new plants need to be watered once a week in cool weather, twice a week during warm weather, and up to three times in a week during periods of extreme heat and drought. Until established, groundcovers and perennials should be watered in such a manner as to totally saturate the soil in the root zone area, to a depth of 6 inches. Once established, perennials shall continue to be watered as necessary to maintain them in a vigorous healthy condition. Over-watering or constant saturation of the soil must be avoided as this could lead to root rot and other disease problems. The use of a soil moisture meter can help you monitor the soil's water intake.

On-site water shall be furnished by the Owner. Hose and other watering equipment shall be furnished by the Landscape Maintenance Contractor.

Replacement – Any unhealthy plant/s that may cause widespread infestation of other nearby plants shall be immediately removed from the site. Any vegetation removed from the site must be recorded and submitted with the landscape maintenance log. The area shall be treated to prevent further infestation. The plant/s shall then be replaced with healthy specimen/s of the same species and size. Old Forge shall have a pre-established budget allowance for this type of replacement, each year.

Plant material that is damaged as a result of other landscape maintenance activities, such as mowing, shall be replaced with healthy specimens of the same species and size, at no additional cost to the owner.

Deadheading – Perennials shall be checked on a weekly basis and dead-headed once flowers have faded or as necessary based on plant type and duration of flower. Spent flowers can be pinched off with the thumb and forefinger. Continue to remove all faded flowers until Fall. All associated debris shall be removed from site daily.

Staking – Upright-growing perennials need support especially when in flower. Use of bamboo stakes, galvanized wire hoops or mesh may be necessary for their support. Supports should be put in place before they have become too difficult to handle. The supports should not be taller than the mature height of the perennial plant.

Division of Perennials – Two or three-year-old perennials are easily divided in the spring if more plants are needed. To divide, cut out the entire section of plant to be divided, including roots. The larger divisions (those with three or more shoots), can be set out immediately in their permanent location, where they can be expected to bloom the same season. Smaller divisions are best planted in an out-of-the-way planting bed until the following autumn or spring, when they can be moved to their permanent location.

Weeding – All planting beds should be kept weed-free. Weed either by hand or with a pre-emergent herbicide such as Treflen used according to manufacturers' specifications. Manual weeding is to be used in combination with the use of spot applications of herbicides. Both live and dead weeds are to be pulled and removed from the site.

All herbicide applications shall be documented in the Landscape Maintenance Log. The actual product label or the manufacturer's product specification sheet for the specific product shall also be included in the Log.

Only personnel with appropriate applicator licenses shall supervise and/or perform the application of pesticide products requiring a license.

Winterizing – Perennial gardens should be cleaned-up when growth ceases in the fall. Remove foliage of plants that normally die down to the ground. Divide and replant over-grown clumps.

C. Lawn Areas - Turf Systems

Mowing – Proper mowing is an integral part of any good turf maintenance program. Without it, the finest in fertilization, watering and other vital maintenance practices would be completely ineffective. Proper mowing will help control dicot weeds; help the turf survive during periods of extreme heat, and gain strength and vigor to resist disease and other infestations.

Mowing height – The proper mowing height will vary somewhat according to the type of grass. The most common type of seed & sod lawns contain a mixture of bluegrass, fine fescue and perennial rye, which should be mowed at 2-3 inches.

Mowing frequency – The basic rule of thumb for mowing frequency is to never remove more than 1/3 of the grass blade in one mowing. Example: if you want to mow your turf at 2 inches, you should cut it when it reaches 3 inches. Removing more than 1/2 of the grass plant at a time can put the plant into shock, thus making it more susceptible to stress disease and weed infestation.

Mowing frequency will vary with the growing season and should be set by the plant height and not a set date. It will often be necessary to mow twice a week during periods of surge growth to help maintain plant health and color. Mowing should be cut back during periods of stress.

Grass clippings should be removed whenever they are thick enough to layer the turf. The return of clippings to the soil actually adds nutrients and helps retain moisture. Heavily clumped grass clippings are a sign of infrequent mowing, calling for an adjustment in the mowing schedule.

When mowing any area, try to alternate mowing patterns. This tends to keep grass blades more erect and assures an even cut. A dull mower will cause color loss due to tearing of the turf plant, and since mowing will ultimately determine the appearance of any turf area there is an absolute necessity for a clean sharp cut.

Weed & Pest Control and Fertilizing- In order to maintain turf grass health, vigor color, and nutrients, fertilizer must be added to the soil. Recommendations for fertilization of lawn areas are as follows; fertilize at the rate of one (1) pound of nitrogen per thousand square feet, per year is optimum. Fertilizer should be a balanced slow release, sulfur coated type fertilizer.

Weed Control - All turf areas will require some weed control, for both weed grasses and dicot weeds. Weeds should be treated at the appropriate time and with a material labeled for the target weed. Please refer to the fertilizer weed and pest schedule for timing.

Pest Control - All turf areas will require some pest control. Pests should be treated at the appropriate time with a material labeled for the target pest. Please refer to the fertilizer, weed and pest schedule for timing.

Lime - A common cause for an unhealthy lawn is acidic soil. When the pH is below the neutral range (between 6-7) vital plant nutrients become fixed in the soil and cannot be absorbed by the grass plant. Lime corrects an acid soil condition, supplies calcium for plant growth and improves air and water circulation. Limestone applied at the rate of 50 lbs. per thousand square feet will adjust the soil pH one point over a period of 6-9 months.

D. Fertilizer, Weed & Pest Control Schedule – Turf Systems

<u>Spring -</u> Fertilize one (1) pound of nitrogen per 1,000 square feet

(April) Pre-emergent weed grass control

Broadleaf weed control

<u>Late Spring</u> - Fertilize one (1) pound of nitrogen per 1,000 square feet

(June) Pre-emergent weed grass control

Broadleaf weed control Insect Control (if needed)

*Summer - Fertilize one (1) pound of nitrogen per 1,000 square feet

(August) Broadleaf weed control (if needed)

Insect Control (if needed)

<u>Fall</u> - Fertilize one (1) pound of nitrogen per 1,000 square feet

(September)

Lawn Maintenance Task Schedule

MARCH (Weather permitting)

- Clean up winter debris, sand, leaves, trash etc.
- Re-edge mulch beds, maintain at 2-3" maximum.
- Fertilize plants
- Aerate and thatch turf (conditions permitting)

APRIL

- Reseed or sod all areas needing attention.
- Fertilize and weed control
- Lime
- Start mowing when grass reaches 2-1/2", mow to 2"

MAY

- Mow turf to 2-2-1/2"
- Weed as necessary.
- Check for disease and pest problems in both turf and plants.

^{*}Omit if area is not to be irrigated

JUNE

- Mow turf to 2-1/2" 3"
- Fertilize and weed control.
- Weed
- Check for disease and pest problems in both turf and plants, treat as necessary.

PROVISIONS FOR SOLID WASTE MANAGEMENT (SITE TRASH)

Trash will be placed in on-site dumpsters and the Owner will make provisions for its regular and timely removal.

SNOW DISPOSAL AND PLOWING PLANS

The purpose of the snow and snowmelt management plan is to provide guidelines regarding snow disposal site selection, site preparation and maintenance that are acceptable to the Department of Environmental Protection. For the areas that require snow removal, snow storage onsite will largely be accomplished by using pervious areas along the shoulder of the roadway and development as windrowed by plows.

- Avoid dumping of snow into any water body, including rivers, ponds, or wetlands. In addition to water quality impacts and flooding, snow disposed of in open water can cause navigational hazards when it freezes into ice blocks.
- Avoid disposing of snow on top of storm drain catch basins or in stormwater basins. Snow combined with sand and debris may block a storm drainage system, causing localized flooding. A high volume of sand, sediment, and litter released from melting snow also may be quickly transported through the system into surface water.
- In significant storm events, the melting or off-site trucking of snow may be implemented. These activities shall be conducted in accordance with all local, state and federal regulations.

WINTER ROAD SALT AND/OR SAND USE AND STORAGE RESTRICTIONS

The applicant will be responsible for sanding and salting the site. No storage on site.

STREET SWEEPING SCHEDULES

There are three types of sweepers: Mechanical, Regenerative Air, and Vacuum Filter.

- 1) Mechanical: Mechanical sweepers use brooms or rotary brushes to scour the pavement.
- 2) Regenerative Air: These sweepers blow air onto the road or parking lot surface, causing fines to rise where they are vacuumed.
- 3) Vacuum filter: These sweepers remove fines along roads. Two general types of vacuum filter sweepers are available wet and dry. The dry type uses a broom in combination with the vacuum. The wet type uses water for dust suppression

Regardless of the type chosen, the efficiency of street sweeping is increased when sweepers are operated in tandem.

This project has not included street sweeping as part of the TSS removal calculations. However, it is recommended that street sweeping of the parking areas occur four times a year, including once after the spring snow melt.

Reuse and Disposal of Street Sweepings

Once removed from paved surfaces, the sweepings must be handled and disposed of properly. Mass DEP's Bureau of Waste Prevention has issued a written policy regarding the reuse and disposal of street sweepings. These sweepings are regulated as a solid waste, and can be used in three ways:

• In one of the ways already approved by Mass DEP (e.g., daily cover in a landfill, additive to compost, fill in a public way)

- If approved under a Beneficial Use Determination
- Disposed in a landfill

TRAINING OF STAFF OR PERSONNEL INVOLVED WITH IMPLEMENTING LONG-TERM POLLUTION PREVENTION PLAN

The Long-Term Pollution Prevention Plan is to be implemented by property owner of the site. Trained and, if required, licensed Professionals are to be hired by the owner as applicable to implement the Long-Term Pollution Prevention Plan.

LIST OF EMERGENCY CONTACTS FOR IMPLEMENTING LONG-TERM POLLUTION PREVENTION PLAN

The applicant will be required to implement the Long-Term Pollution Prevention Plan and will create and maintain a list of emergency contacts.

POST CONSTRUCTION PHASE INSPECTION SCHEDULE AND EVALUATION CHECKLIST

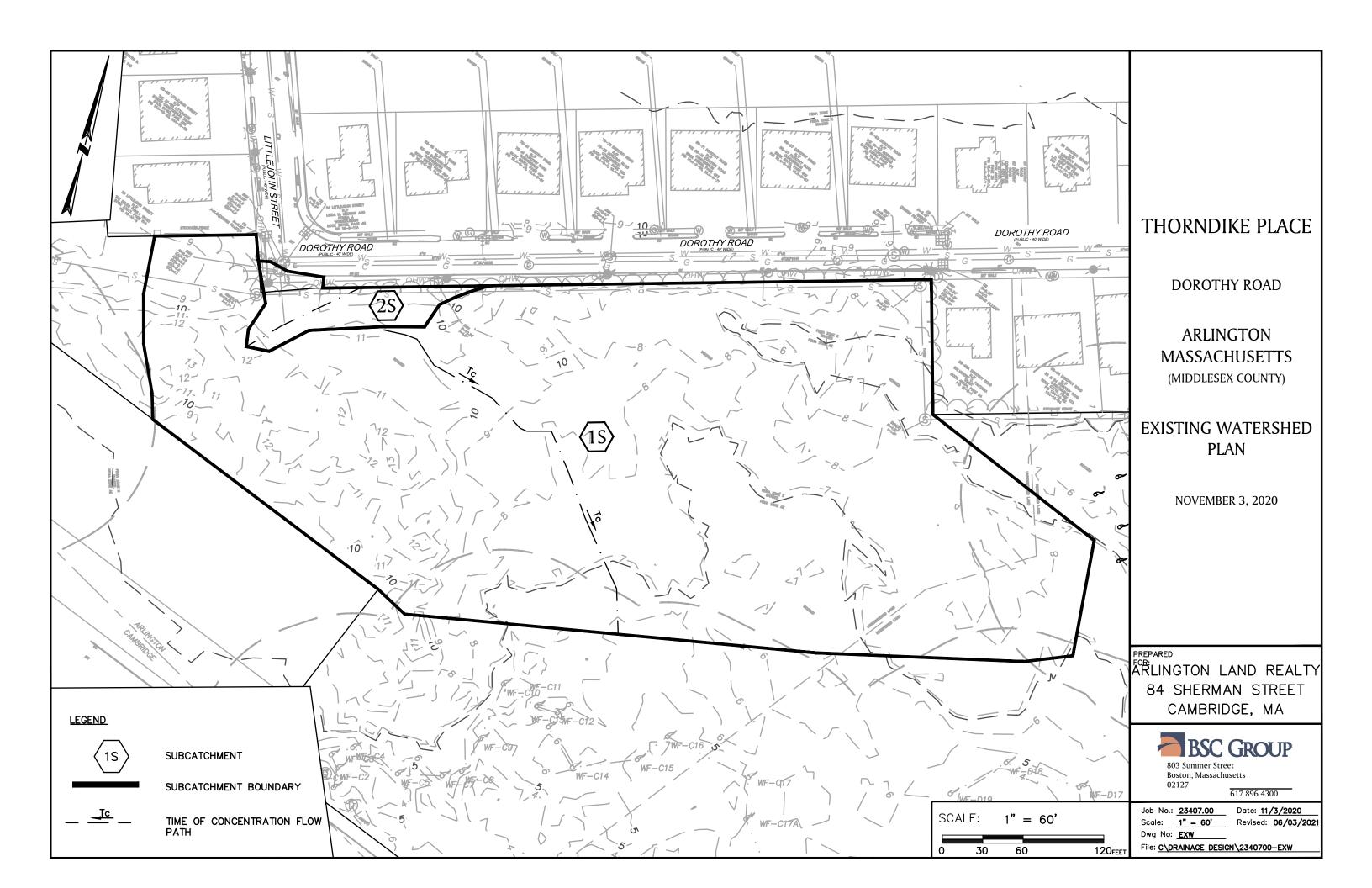
Inspection Date	Inspector	BMP Inspected	Inspection Frequency Requirement s	Comments	Recommendation	Follow-up Inspection Required (yes/no)
		Catch Basin	Four times a year			
		Water Quality Units	Four times a year			
		Infiltration System	Twice a year			
		Pipe Outlet Protection	Once a year			

- 1. Refer to the Massachusetts Stormwater Handbook Volume Two: Stormwater Technical Handbook (February 2008) for recommendations regarding frequency for inspections and maintenance of specific BMP's
- 2. Inspections to be conducted by a qualified professional such as an environmental scientist or civil engineer.
- 3. Limited or no use of sodium chloride salts, fertilizers or pesticides recommended.
- 4. <u>Other Notes</u>: (Include deviations from Conservation Commission Approvals, Planning Board Approvals and Approved Plans)

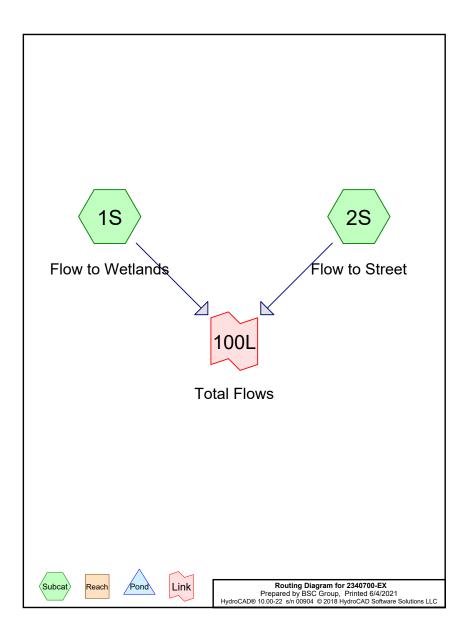
SECTION 5.0

HYDROLOGY CALCULATIONS

5.01 EXISTING WATERSHED PLAN



5.02 EXISTING HYDROLOGY CALCULATIONS (HYDROCADTM PRINTOUTS)



Thorndike Place-Existing Conditions

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Area Listing (all nodes)

Area	CN	Description
(acres)		(subcatchment-numbers)
0.021	98	Paved parking, HSG C (2S)
3.534	70	Woods, Good, HSG C (1S, 2S)
3.555	70	TOTAL AREA

Thorndike Place-Existing Conditions

2340700-EX

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Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
0.000	HSG B	
3.555	HSG C	1S, 2S
0.000	HSG D	
0.000	Other	
3.555		TOTAL AREA

Thorndike Place-Existing Conditions

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Ground Covers (all nodes)

 HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.000	0.000	0.021	0.000	0.000	0.021	Paved parking	2S
0.000	0.000	3.534	0.000	0.000	3.534	Woods, Good	1S, 2S
0.000	0.000	3.555	0.000	0.000	3.555	TOTAL AREA	

Thorndike Place-Existing Conditions
Type III 24-hr 2-Year Rainfall=3.64"
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Time span=0.00-24.00 hrs, dt=0.01 hrs, 2401 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1S: Flow to Wetlands

Runoff Area=147,900 sf 0.00% Impervious Runoff Depth>1.09" Flow Length=310' Tc=17.5 min CN=70 Runoff=2.9 cfs 0.308 af

Subcatchment 2S: Flow to Street

Runoff Area=6,954 sf 13.30% Impervious Runoff Depth>1.34" Flow Length=95' Tc=6.0 min CN=74 Runoff=0.2 cfs 0.018 af

Link 100L: Total Flows

Inflow=3.0 cfs 0.326 af Primary=3.0 cfs 0.326 af

Total Runoff Area = 3.555 ac Runoff Volume = 0.326 af Average Runoff Depth = 1.10" 99.40% Pervious = 3.534 ac 0.60% Impervious = 0.021 ac 2340700-EX

Thorndike Place-Existing Conditions

Type III 24-hr 2-Year Rainfall=3.64"

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Summary for Subcatchment 1S: Flow to Wetlands

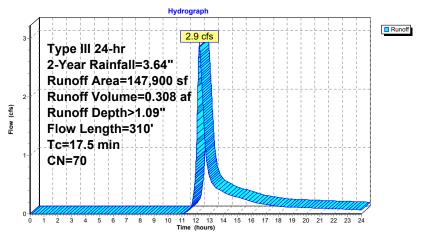
Runoff = 2.9 cfs @ 12.27 hrs, Volume= 0

0.308 af, Depth> 1.09"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2-Year Rainfall=3.64"

A	rea (sf)	CN D	escription		
147,900 70 Woods, Good, HSG C				od, HSG C	
1	147,900 100.00% Pervious Area			ervious Are	a
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
11.4	50	0.0240	0.07		Sheet Flow, A to B Woods: Light underbrush n= 0.400 P2= 3.23"
6.1	260	0.0200	0.71		Shallow Concentrated Flow, B to C Woodland Kv= 5.0 fps
17.5	310	Total			<u> </u>

Subcatchment 1S: Flow to Wetlands



Thorndike Place-Existing Conditions Type III 24-hr 2-Year Rainfall=3.64" Printed 6/4/2021

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Summary for Subcatchment 2S: Flow to Street

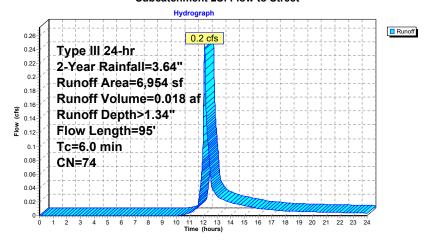
0.2 cfs @ 12.09 hrs, Volume= 0.018 af, Depth> 1.34" Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2-Year Rainfall=3.64"

A	rea (sf)	CN I	Description						
	6,029	70	Noods, Go	od, HSG C					
	925	98 I	Paved park	ing, HSG C	,				
	6,954	74	74 Weighted Average						
	6,029		36.70% Pei	rvious Area					
	925		13.30% Impervious Area						
Tc	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)		(cfs)	Description				
3.5	20	0.0750	0.10		Sheet Flow, A to B				
					Woods: Light underbrush n= 0.400 P2= 3.23"				
1.8	75	0.0200	0.71		Shallow Concentrated Flow, B to C				
					Woodland Kv= 5.0 fps				

5.3 95 Total, Increased to minimum Tc = 6.0 min

Subcatchment 2S: Flow to Street



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Thorndike Place-Existing Conditions Type III 24-hr 2-Year Rainfall=3.64" Printed 6/4/2021

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Summary for Link 100L: Total Flows

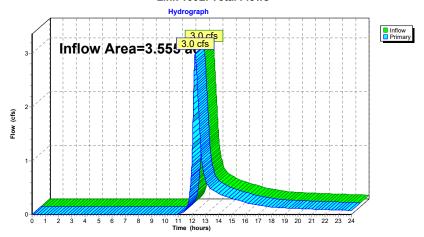
3.555 ac, 0.60% Impervious, Inflow Depth > 1.10" for 2-Year event 3.0 cfs @ 12.26 hrs, Volume= 0.326 af Inflow Area =

Inflow

Primary = 3.0 cfs @ 12.26 hrs, Volume= 0.326 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Link 100L: Total Flows



Thorndike Place-Existing Conditions Type III 24-hr 10-Year Rainfall=5.79" Printed 6/4/2021

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Time span=0.00-24.00 hrs, dt=0.01 hrs, 2401 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Runoff Area=147,900 sf 0.00% Impervious Runoff Depth>2.63" Flow Length=310' Tc=17.5 min CN=70 Runoff=7.4 cfs 0.744 af

Subcatchment 2S: Flow to Street

Subcatchment 1S: Flow to Wetlands

Runoff Area=6,954 sf 13.30% Impervious Runoff Depth>3.01" Flow Length=95' Tc=6.0 min CN=74 Runoff=0.6 cfs 0.040 af

Link 100L: Total Flows

Inflow=7.7 cfs 0.784 af Primary=7.7 cfs 0.784 af

Total Runoff Area = 3.555 ac Runoff Volume = 0.784 af Average Runoff Depth = 2.65" 99.40% Pervious = 3.534 ac 0.60% Impervious = 0.021 ac 2340700-EX

Thorndike Place-Existing Conditions
Type III 24-hr 10-Year Rainfall=5.79"
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Summary for Subcatchment 1S: Flow to Wetlands

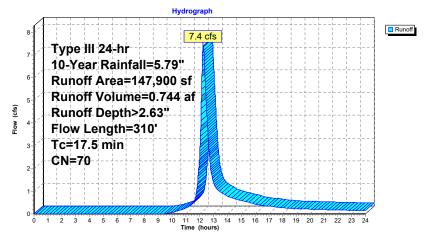
Runoff = 7.4 cfs @ 12.25 hrs, Volume=

0.744 af, Depth> 2.63"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.79"

A	rea (sf)	CN D	escription		
147,900 70 Woods, Good, HSG C					
1	147,900 100.00% Pervious Area			ervious Are	a
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
11.4	50	0.0240	0.07		Sheet Flow, A to B Woods: Light underbrush n= 0.400 P2= 3.23"
6.1	260	0.0200	0.71		Shallow Concentrated Flow, B to C Woodland Kv= 5.0 fps
17.5	310	Total			

Subcatchment 1S: Flow to Wetlands



Thorndike Place-Existing Conditions Type III 24-hr 10-Year Rainfall=5.79" Printed 6/4/2021

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Summary for Subcatchment 2S: Flow to Street

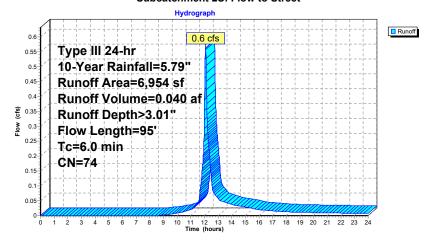
0.6 cfs @ 12.09 hrs, Volume= 0.040 af, Depth> 3.01" Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.79"

A	rea (sf)	CN [Description						
	6,029	70 V	Woods, Good, HSG C						
	925	98 F	Paved park	ing, HSG C)				
	6,954	74 V	Veighted A	verage					
	6,029	8	86.70% Per	vious Area					
	925	1	3.30% Imp	ervious Ar	ea				
т.	1	01	M-1it-	0:	Description				
Tc	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
3.5	20	0.0750	0.10		Sheet Flow, A to B				
					Woods: Light underbrush n= 0.400 P2= 3.23"				
1.8	75	0.0200	0.71		Shallow Concentrated Flow, B to C				
					Woodland Kv= 5.0 fps				

5.3 95 Total, Increased to minimum Tc = 6.0 min

Subcatchment 2S: Flow to Street



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Type III 24-hr 10-Year Rainfall=5.79" Prepared by BSC Group Printed 6/4/2021 HydroCAD® 10.00-22 s/n 00904 © 2018 HydroCAD Software Solutions LLC Page 12

Thorndike Place-Existing Conditions

Summary for Link 100L: Total Flows

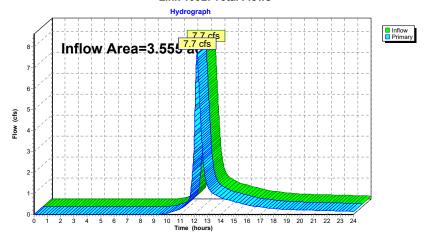
3.555 ac, $\,$ 0.60% Impervious, Inflow Depth > $\,$ 2.65" $\,$ for 10-Year event 7.7 cfs @ 12.24 hrs, Volume= $\,$ 0.784 af Inflow Area =

Inflow

Primary = 7.7 cfs @ 12.24 hrs, Volume= 0.784 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Link 100L: Total Flows



Thorndike Place-Existing Conditions Type III 24-hr 25-Year Rainfall=7.49"

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Time span=0.00-24.00 hrs, dt=0.01 hrs, 2401 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1S: Flow to Wetlands

Runoff Area=147,900 sf 0.00% Impervious Runoff Depth>4.01" Flow Length=310' Tc=17.5 min CN=70 Runoff=11.4 cfs 1.136 af

Subcatchment 2S: Flow to Street

Runoff Area=6,954 sf 13.30% Impervious Runoff Depth>4.47" Flow Length=95' Tc=6.0 min CN=74 Runoff=0.8 cfs 0.059 af

Link 100L: Total Flows

Inflow=11.8 cfs 1.195 af Primary=11.8 cfs 1.195 af

Total Runoff Area = 3.555 ac Runoff Volume = 1.195 af Average Runoff Depth = 4.04" 99.40% Pervious = 3.534 ac 0.60% Impervious = 0.021 ac 2340700-EX

Thorndike Place-Existing Conditions
Type III 24-hr 25-Year Rainfall=7.49"
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Summary for Subcatchment 1S: Flow to Wetlands

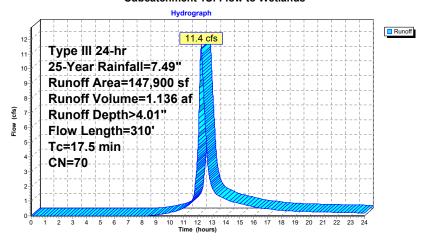
Runoff = 11.4 cfs @ 12.24 hrs, Volume= 1.136 a

1.136 af, Depth> 4.01"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=7.49"

A	rea (sf)	CN D	escription		
147,900 70 Woods, Good,			Voods, Go	od, HSG C	
147,900		100.00% Pervious Area			a
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
11.4	50	0.0240	0.07		Sheet Flow, A to B
6.1	260	0.0200	0.71		Woods: Light underbrush n= 0.400 P2= 3.23" Shallow Concentrated Flow, B to C Woodland Kv= 5.0 fps
17.5	310	Total			

Subcatchment 1S: Flow to Wetlands



Thorndike Place-Existing Conditions Type III 24-hr 25-Year Rainfall=7.49" Printed 6/4/2021

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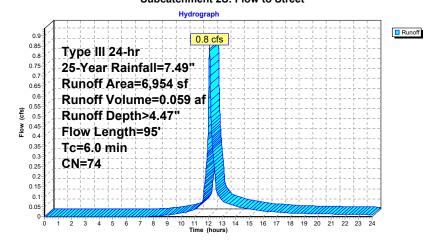
Summary for Subcatchment 2S: Flow to Street

0.8 cfs @ 12.09 hrs, Volume= 0.059 af, Depth> 4.47" Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=7.49"

	Area (sf)	CN E	Description					
	6,029	70 V	Voods, Go	od, HSG C				
	925	98 F	Paved parking, HSG C					
	6,954	74 V	Veighted A	verage				
	6,029	8	86.70% Pervious Area					
	925	1	3.30% Imp	pervious Are	ea			
Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
3.5	20	0.0750	0.10		Sheet Flow, A to B			
					Woods: Light underbrush n= 0.400 P2= 3.23"			
1.8	75	0.0200	0.71		Shallow Concentrated Flow, B to C			
					Woodland Kv= 5.0 fps			
5.3	95	Total, I	ncreased t	o minimum	Tc = 6.0 min			

Subcatchment 2S: Flow to Street



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Thorndike Place-Existing Conditions Type III 24-hr 25-Year Rainfall=7.49" Printed 6/4/2021

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Summary for Link 100L: Total Flows

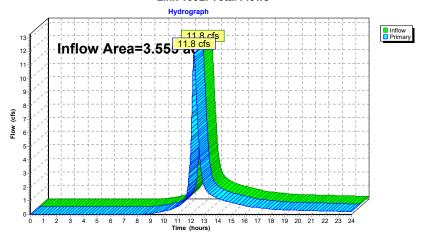
3.555 ac, $\,$ 0.60% Impervious, Inflow Depth > 4.04" $\,$ for 25-Year event 11.8 cfs @ 12.23 hrs, Volume= $\,$ 1.195 af Inflow Area =

Inflow

Primary = 11.8 cfs @ 12.23 hrs, Volume= 1.195 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Link 100L: Total Flows



Thorndike Place-Existing Conditions
Type III 24-hr 50-Year Rainfall=8.72"

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Time span=0.00-24.00 hrs, dt=0.01 hrs, 2401 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1S: Flow to Wetlands

Runoff Area=147,900 sf 0.00% Impervious Runoff Depth>5.07" Flow Length=310' Tc=17.5 min CN=70 Runoff=14.4 cfs 1.435 af

Subcatchment 2S: Flow to Street

Runoff Area=6,954 sf 13.30% Impervious Runoff Depth>5.57" Flow Length=95' Tc=6.0 min CN=74 Runoff=1.0 cfs 0.074 af

Link 100L: Total Flows

Inflow=15.0 cfs 1.509 af Primary=15.0 cfs 1.509 af

Total Runoff Area = 3.555 ac Runoff Volume = 1.509 af Average Runoff Depth = 5.09" 99.40% Pervious = 3.534 ac 0.60% Impervious = 0.021 ac 2340700-EX

Thorndike Place-Existing Conditions Type III 24-hr 50-Year Rainfall=8.72" Printed 6/4/2021

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Summary for Subcatchment 1S: Flow to Wetlands

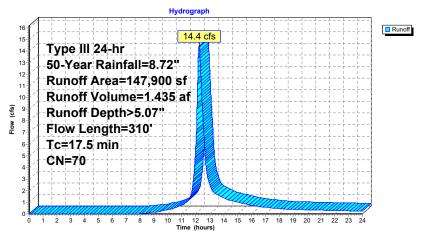
Runoff = 14.4 cfs @ 12.23 hrs, Volume=

1.435 af, Depth> 5.07"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 50-Year Rainfall=8.72"

	Α	rea (sf)	CN I	Description						
147,900 70 Woods, Good, HSG C					od, HSG C					
	1	47,900		100.00% Pe	ervious Are	a				
	Tc (min)	Length (feet)	Slope (ft/ft)	,	Capacity (cfs)	Description				
	11.4	50	0.0240	0.07	· · · · · ·	Sheet Flow, A to B				
	6.1	260	0.0200	0.71		Woods: Light underbrush n= 0.400 P2= 3.23" Shallow Concentrated Flow, B to C Woodland Kv= 5.0 fps				
	17.5	310	Total							

Subcatchment 1S: Flow to Wetlands



Thorndike Place-Existing Conditions Type III 24-hr 50-Year Rainfall=8.72" Printed 6/4/2021

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Summary for Subcatchment 2S: Flow to Street

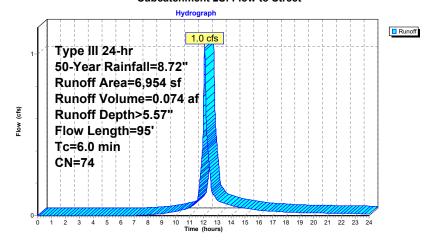
1.0 cfs @ 12.09 hrs, Volume= Runoff 0.074 af, Depth> 5.57"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 50-Year Rainfall=8.72"

	Area (sf)	CN E	Description					
	6,029	70 V	70 Woods, Good, HSG C					
	925	98 F	Paved parking, HSG C					
	6,954	74 V	Weighted Average					
	6,029	8	86.70% Pervious Area					
	925	1	3.30% Imp	pervious Are	ea			
Т	c Length	Slope	Velocity	Capacity	Description			
(mir	n) (feet)	(ft/ft)	(ft/sec)	(cfs)				
3.	5 20	0.0750	0.10		Sheet Flow, A to B			
					Woods: Light underbrush n= 0.400 P2= 3.23"			
1.	8 75	0.0200	0.71		Shallow Concentrated Flow, B to C			
					Woodland Kv= 5.0 fps			
5.	3 95	Total, I	ncreased t	o minimum	Tc = 6.0 min			

95 Total, Increased to minimum Tc = 6.0 min

Subcatchment 2S: Flow to Street



2340700-EX

Thorndike Place-Existing Conditions Type III 24-hr 50-Year Rainfall=8.72" Printed 6/4/2021

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Summary for Link 100L: Total Flows

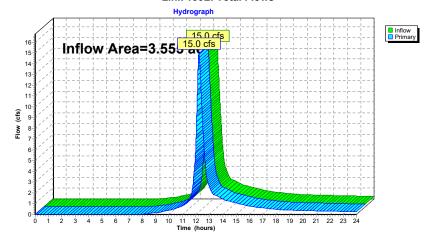
3.555 ac, $\,$ 0.60% Impervious, Inflow Depth > $\,$ 5.09" $\,$ for 50-Year event Inflow Area =

Inflow 15.0 cfs @ 12.23 hrs, Volume= 1.509 af

Primary = 15.0 cfs @ 12.23 hrs, Volume= 1.509 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Link 100L: Total Flows



Thorndike Place-Existing Conditions Type III 24-hr 100-Year Rainfall=10.35"

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Time span=0.00-24.00 hrs, dt=0.01 hrs, 2401 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1S: Flow to Wetlands

Runoff Area=147.900 sf 0.00% Impervious Runoff Depth>6.52" Flow Length=310' Tc=17.5 min CN=70 Runoff=18.5 cfs 1.844 af

Subcatchment 2S: Flow to Street

Runoff Area=6.954 sf 13.30% Impervious Runoff Depth>7.06" Flow Length=95' Tc=6.0 min CN=74 Runoff=1.3 cfs 0.094 af

Link 100L: Total Flows

Inflow=19.2 cfs 1.938 af Primary=19.2 cfs 1.938 af

Total Runoff Area = 3.555 ac Runoff Volume = 1.938 af Average Runoff Depth = 6.54" 99.40% Pervious = 3.534 ac 0.60% Impervious = 0.021 ac

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Thorndike Place-Existing Conditions Type III 24-hr 100-Year Rainfall=10.35" Printed 6/4/2021

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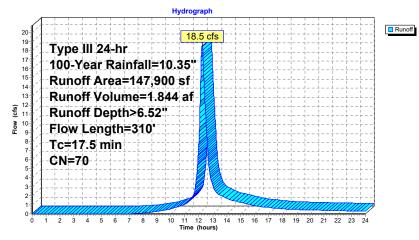
Summary for Subcatchment 1S: Flow to Wetlands

18.5 cfs @ 12.23 hrs, Volume= Runoff 1.844 af, Depth> 6.52"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100-Year Rainfall=10.35"

A	rea (sf)	CN D	CN Description							
147,900 70 Woods, Good, HSG C				od, HSG C						
1	147,900 100.00% Pervious Area			ervious Are	a					
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description					
11.4	50	0.0240	0.07		Sheet Flow, A to B Woods: Light underbrush n= 0.400 P2= 3.23"					
6.1	260	0.0200	0.71		Shallow Concentrated Flow, B to C Woodland Kv= 5.0 fps					
17.5	310	Total			·					

Subcatchment 1S: Flow to Wetlands



Thorndike Place-Existing Conditions Type III 24-hr 100-Year Rainfall=10.35" Printed 6/4/2021

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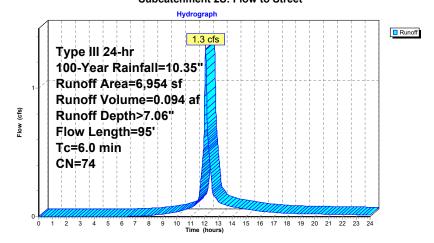
Summary for Subcatchment 2S: Flow to Street

0.094 af, Depth> 7.06" Runoff 1.3 cfs @ 12.09 hrs, Volume=

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100-Year Rainfall=10.35"

A	rea (sf)	CN E	escription		
	6,029	70 V	Voods, Go	od, HSG C	
	925	98 F	aved park	ing, HSG C	
	6,954	74 V	Veighted A	verage	
	6,029	8	6.70% Per	vious Area	
	925	1	3.30% Imp	pervious Are	ea
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
3.5	20	0.0750	0.10		Sheet Flow, A to B
					Woods: Light underbrush n= 0.400 P2= 3.23"
1.8	75	0.0200	0.71		Shallow Concentrated Flow, B to C
					Woodland Kv= 5.0 fps
5.3	95	Total, I	ncreased t	o minimum	Tc = 6.0 min

Subcatchment 2S: Flow to Street



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Summary for Link 100L: Total Flows

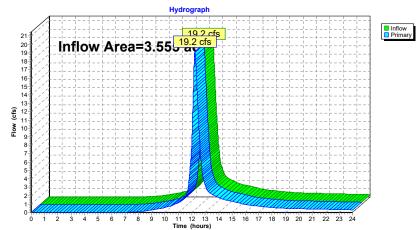
3.555 ac, $\,$ 0.60% Impervious, Inflow Depth > 6.54" $\,$ for 100-Year event 19.2 cfs @ 12.23 hrs, Volume= $\,$ 1.938 af Inflow Area =

Inflow

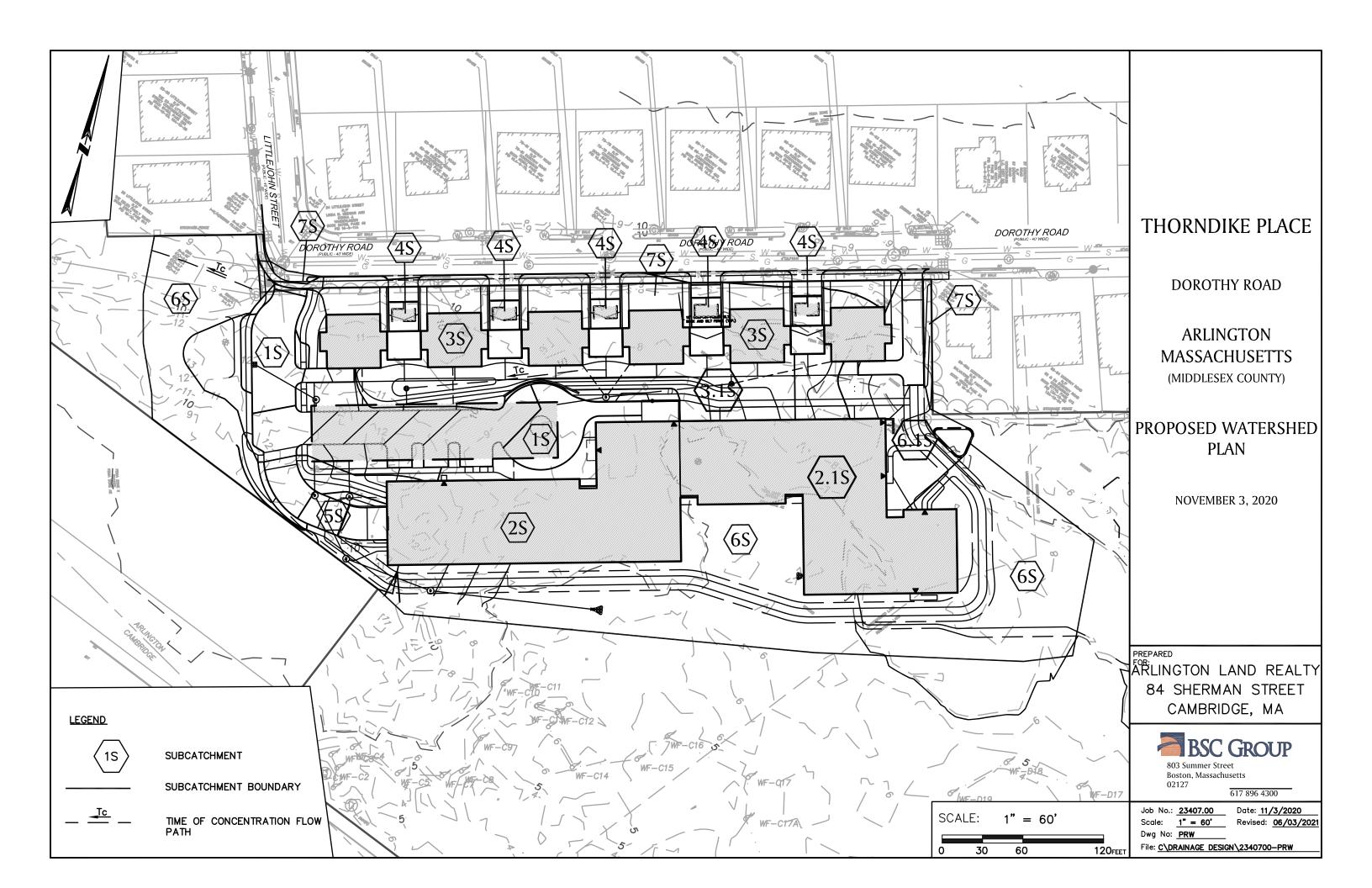
Primary = 19.2 cfs @ 12.23 hrs, Volume= 1.938 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

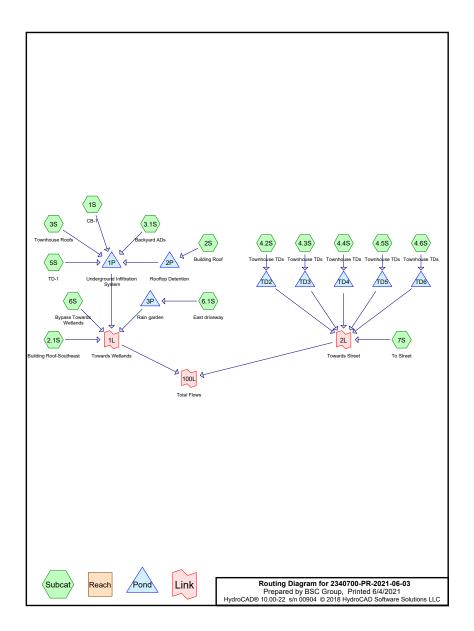
Link 100L: Total Flows



5.03 PROPOSED WATERSHED PLAN



5.04 PROPOSED HYDROLOGY CALCULATIONS (HYDROCAD $^{\text{TM}}$ PRINTOUTS)



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Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
1.544	74	>75% Grass cover, Good, HSG C (1S, 3.1S, 5S, 6.1S, 6S, 7S)
0.580	98	Paved parking, HSG C (1S, 4.2S, 4.3S, 4.4S, 4.5S, 4.6S, 5S, 7S
0.041	98	Paved roads w/curbs & sewers, HSG C (6.1S)
1.054	98	Roofs, HSG C (2.1S, 2S, 3S, 6S)
0.027	98	Unconnected pavement, HSG C (3.1S)
0.310	70	Woods, Good, HSG C (6S)
3.555	85	TOTAL AREA

Thorndike Place - Proposed Conditions

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Soil Listing (all nodes)

	Area	Soil	Subcatchment
(;	acres)	Group	Numbers
	0.000	HSG A	
	0.000	HSG B	
	3.555	HSG C	1S, 2.1S, 2S, 3.1S, 3S, 4.2S, 4.3S, 4.4S, 4.5S, 4.6S, 5S, 6.1S, 6S, 7S
	0.000	HSG D	
	0.000	Other	
	3.555		TOTAL AREA

Thorndike Place - Proposed Conditions

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Ground Covers (all nodes)

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.000	0.000	1.544	0.000	0.000	1.544	>75% Grass cover, Good	1S, 3.1S
							, 5S, 6.1S
							, 6S, 7S
0.000	0.000	0.580	0.000	0.000	0.580	Paved parking	1S, 4.2S
							, 4.3S
							, 4.4S
							, 4.5S
							, 4.6S
							, 5S, 7S
0.000 0.000	0.000	0.041 1.054	0.000	0.000	0.041 1.054	Paved roads w/curbs & sewers Roofs	6.1S 2.1S
0.000	0.000	1.054	0.000	0.000	1.054	Roois	2S, 3S, 6S
0.000	0.000	0.027	0.000	0.000	0.027	Unconnected pavement	3.1S
0.000 0.000	0.000 0.000	0.310 3.555	0.000 0.000	0.000 0.000	0.310 3.555	Woods, Good TOTAL AREA	6S

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Pond 2P: Rooftop Detention

Thorndike Place - Proposed Conditions Type III 24-hr 2-Year Rainfall=3.64" Printed 6/4/2021

Peak Elev=57.26' Storage=1,934 cf Inflow=1.3 cfs 0.104 af

Outflow=0.2 cfs 0.104 af

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Time span=0.00-72.00 hrs, dt=0.01 hrs, 7201 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Reach routing by Stor-Ind+11	ans method - Pond routing by Stor-Ind method
Subcatchment 1S: CB-1	Runoff Area=22,742 sf 72.16% Impervious Runoff Depth=2.67" Tc=6.0 min CN=91 Runoff=1.6 cfs 0.116 af
Subcatchment 2.1S: Building	Runoff Area=16,789 sf 100.00% Impervious Runoff Depth=3.41" Tc=6.0 min CN=98 Runoff=1.4 cfs 0.109 af
Subcatchment 2S: Building Roof	Runoff Area=15,928 sf 100.00% Impervious Runoff Depth=3.41" Tc=6.0 min CN=98 Runoff=1.3 cfs 0.104 af
Subcatchment 3.1S: Backyard ADs Flow Length	Runoff Area=13,693 sf 8.51% Impervious Runoff Depth=1.40" h=147' Tc=10.3 min UI Adjusted CN=75 Runoff=0.4 cfs 0.037 af
Subcatchment 3S: Townhouse Roofs	Runoff Area=13,067 sf 100.00% Impervious Runoff Depth=3.41" Tc=6.0 min CN=98 Runoff=1.1 cfs 0.085 af
Subcatchment 4.2S: Townhouse TDs	Runoff Area=485 sf 100.00% Impervious Runoff Depth=3.41" Tc=6.0 min CN=98 Runoff=0.0 cfs 0.003 af
Subcatchment 4.3S: Townhouse TDs	Runoff Area=485 sf 100.00% Impervious Runoff Depth=3.41" Tc=6.0 min CN=98 Runoff=0.0 cfs 0.003 af
Subcatchment 4.4S: Townhouse TDs	Runoff Area=485 sf 100.00% Impervious Runoff Depth=3.41" Tc=6.0 min CN=98 Runoff=0.0 cfs 0.003 af
Subcatchment 4.5S: Townhouse TDs	Runoff Area=485 sf 100.00% Impervious Runoff Depth=3.41" Tc=6.0 min CN=98 Runoff=0.0 cfs 0.003 af
Subcatchment 4.6S: Townhouse TDs	Runoff Area=485 sf 100.00% Impervious Runoff Depth=3.41" Tc=6.0 min CN=98 Runoff=0.0 cfs 0.003 af
Subcatchment 5S: TD-1	Runoff Area=5,851 sf 51.63% Impervious Runoff Depth=2.22" Tc=6.0 min CN=86 Runoff=0.3 cfs 0.025 af
Subcatchment 6.1S: East driveway	Runoff Area=6,850 sf 25.93% Impervious Runoff Depth=1.75" Tc=6.0 min CN=80 Runoff=0.3 cfs 0.023 af
Subcatchment 6S: Bypass Towards Flow Length=80	Runoff Area=48,647 sf 0.22% Impervious Runoff Depth=1.27" 'Slope=0.0133'/' Tc=15.4 min CN=73 Runoff=1.2 cfs 0.119 af
Subcatchment 7S: To Street	Runoff Area=8,882 sf 38.49% Impervious Runoff Depth=1.98" Tc=6.0 min CN=83 Runoff=0.5 cfs 0.034 af
Pond 1P: Underground Infiltration System Discarded=0.	Peak Elev=7.58' Storage=10,244 cf Inflow=3.5 cfs 0.367 af 1 cfs 0.348 af Primary=0.1 cfs 0.019 af Outflow=0.1 cfs 0.367 af

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 Type III 24-hr 2-Year Rainfall=3.64"

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Peak Elev=6.33' Storage=179 cf Inflow=0.3 cfs 0.023 af

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Pond 3P: Rain garden

Discarded=0.0 cfs 0.009 af Primary=0.3 cfs 0.014 af Outflow=0.3 cfs 0.023 af

Pond TD2:

Peak Elev=7.35' Storage=66 cf Inflow=0.0 cfs 0.003 af
Discarded=0.0 cfs 0.003 af Primary=0.0 cfs 0.000 af Outflow=0.0 cfs 0.003 af

Pond TD3: Peak Elev=7.35' Storage=66 cf Inflow=0.0 cfs 0.003 af

Discarded=0.0 cfs 0.003 af Primary=0.0 cfs 0.000 af Outflow=0.0 cfs 0.003 af

Pond TD4:

Peak Elev=7.35' Storage=66 cf Inflow=0.0 cfs 0.003 af Discarded=0.0 cfs 0.003 af Primary=0.0 cfs 0.000 af Outflow=0.0 cfs 0.003 af Primary=0.0 cfs 0.000 af Outflow=0.0 cfs 0.003 af

Pond TD5:

Peak Elev=7.35' Storage=66 cf Inflow=0.0 cfs 0.003 af Discarded=0.0 cfs 0.003 af Primary=0.0 cfs 0.000 af Outflow=0.0 cfs 0.003 af Outflow=0.0 cfs 0.003 af Discarded=0.0 cf

Pond TD6:

Peak Elev=7.35' Storage=66 cf Inflow=0.0 cfs 0.003 af
Discarded=0.0 cfs 0.003 af Primary=0.0 cfs 0.000 af Outflow=0.0 cfs 0.003 af

Link 1L: Towards Wetlands Inflow=2.4 cfs 0.260 af

Link 2L: Towards Street Inflow=0.5 cfs 0.034 af

Primary=0.5 cfs 0.034 af

Primary=2.4 cfs 0.260 af

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Link 100L: Total Flows Inflow=2.9 cfs 0.294 af

Primary=2.9 cfs 0.294 af

Total Runoff Area = 3.555 ac Runoff Volume = 0.667 af Average Runoff Depth = 2.25" 52.15% Pervious = 1.854 ac 47.85% Impervious = 1.701 ac

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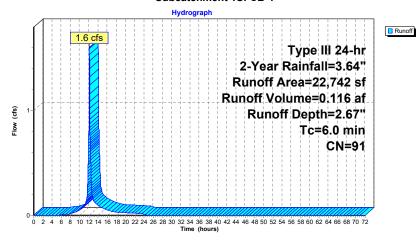
Summary for Subcatchment 1S: CB-1

Runoff = 1.6 cfs @ 12.09 hrs, Volume= 0.116 af, Depth= 2.67"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 2-Year Rainfall=3.64"

	Ar	ea (sf)	CN I	Description							
	•	16,410	98	Paved parking, HSG C							
		6,332	74	>75% Grass cover, Good, HSG C							
	2	22,742	91	1 Weighted Average							
		6,332	:	27.84% Per	vious Area	a					
	•	16,410		72.16% Imp	ervious Ar	rea					
	Тс	Length	Slope	Velocity	Capacity	Description					
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		_				
	6.0					Direct Entry, Min. Tc					

Subcatchment 1S: CB-1



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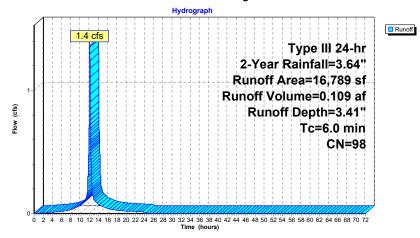
Summary for Subcatchment 2.1S: Building Roof-Southeast

Runoff = 1.4 cfs @ 12.08 hrs, Volume= 0.109 af, Depth= 3.41"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 2-Year Rainfall=3.64"

	Α	rea (sf)	CN I	Description		
ľ		16,789	98 I	Roofs, HSC	G C	
		16,789		100.00% In	npervious A	Area
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	6.0					Direct Entry, Min. Tc

Subcatchment 2.1S: Building Roof-Southeast



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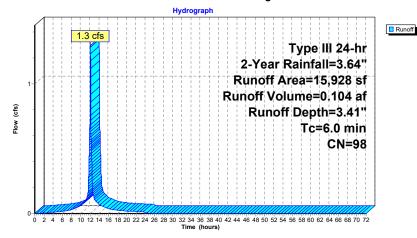
Summary for Subcatchment 2S: Building Roof

Runoff = 1.3 cfs @ 12.08 hrs, Volume= 0.104 af, Depth= 3.41"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 2-Year Rainfall=3.64"

A	rea (sf)	CN E	Description		
	15,928	98 F	Roofs, HSG	C C	
	15,928	1	00.00% In	npervious A	Area
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Min. Tc

Subcatchment 2S: Building Roof



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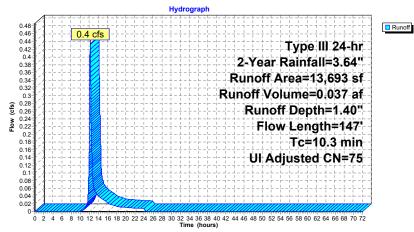
Summary for Subcatchment 3.1S: Backyard ADs

Runoff = 0.4 cfs @ 12.15 hrs, Volume= 0.037 af, Depth= 1.40"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 2-Year Rainfall=3.64"

Α	rea (sf)	CN	Adj Desc	Description						
	1,165	98	Unco	Unconnected pavement, HSG C						
	12,528	74	>75%	√ Grass co	ver, Good, HSG C					
	13,693	76	75 Weig	hted Avera	ge, UI Adjusted					
	12,528		91.4	9% Perviou	s Area					
	1,165		8.51	% Impervio	us Area					
	1,165		100.	00% Uncon	nected					
_					5					
Tc	Length	Slope		Capacity	Description					
(min)	(feet)	(ft/ft)		(cfs)		_				
9.4	50	0.0142	0.09		Sheet Flow,					
					Grass: Dense n= 0.240 P2= 3.23"					
0.9	97	0.0154	1.86		Shallow Concentrated Flow,					
					Grassed Waterway Kv= 15.0 fps					
10.3	147	Total								

Subcatchment 3.1S: Backyard ADs



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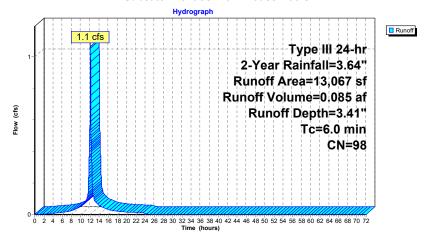
Summary for Subcatchment 3S: Townhouse Roofs

Runoff = 1.1 cfs @ 12.08 hrs, Volume= 0.085 af, Depth= 3.41"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 2-Year Rainfall=3.64"

Area (s	f) CN	Description		
13,06	7 98	Roofs, HSC	G C	
13,06	7	100.00% In	npervious A	Area
Tc Leng			Capacity (cfs)	Description
6.0			-	Direct Entry, Min. Tc

Subcatchment 3S: Townhouse Roofs



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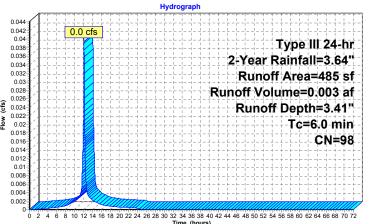
Summary for Subcatchment 4.2S: Townhouse TDs

Runoff = 0.0 cfs @ 12.08 hrs, Volume= 0.003 af, Depth= 3.41"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 2-Year Rainfall=3.64"

Α	rea (sf)	CN I	Description					
	485	98 I	Paved parking, HSG C					
	485		100.00% Impervious Area					
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
6.0					Direct Entry, Min. Tc			

Subcatchment 4.2S: Townhouse TDs





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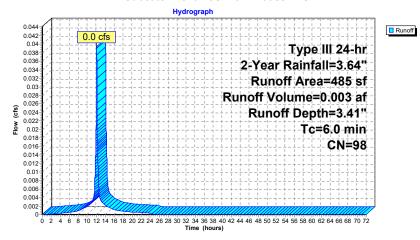
Summary for Subcatchment 4.3S: Townhouse TDs

Runoff = 0.0 cfs @ 12.08 hrs, Volume= 0.003 af, Depth= 3.41"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 2-Year Rainfall=3.64"

	Α	rea (sf)	CN [Description Paved parking, HSG C 00.00% Impervious Area Velocity Capacity Description						
		485	98 F	1 0,						
Ī		485	•	100.00% In	npervious A	rea				
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
	6.0				. ,	Direct Entry Min To				

Subcatchment 4.3S: Townhouse TDs



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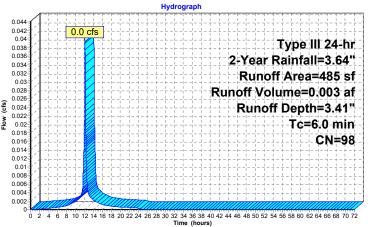
Summary for Subcatchment 4.4S: Townhouse TDs

Runoff = 0.0 cfs @ 12.08 hrs, Volume= 0.003 af, Depth= 3.41"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 2-Year Rainfall=3.64"

	rea (sf)	CN D	escription		
	485	98 F	aved park	ing, HSG C	
	485	1	00.00% In	pervious A	Area
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Min. Tc

Subcatchment 4.4S: Townhouse TDs



Runoff

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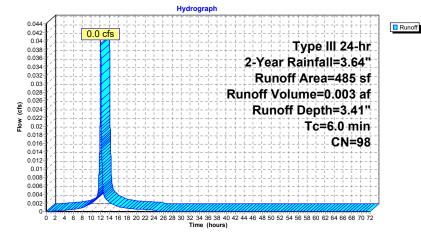
Summary for Subcatchment 4.5S: Townhouse TDs

Runoff = 0.0 cfs @ 12.08 hrs, Volume= 0.003 af, Depth= 3.41"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 2-Year Rainfall=3.64"

Α	rea (sf)	CN E	Description			
	485	98 F	aved park	ing, HSG C		
	485 100.00% Impervious Area					
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
6.0					Direct Entry, Min. Tc	

Subcatchment 4.5S: Townhouse TDs



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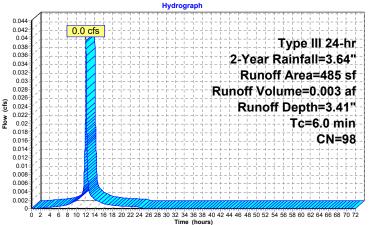
Summary for Subcatchment 4.6S: Townhouse TDs

Runoff = 0.0 cfs @ 12.08 hrs, Volume= 0.003 af, Depth= 3.41"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 2-Year Rainfall=3.64"

Α	rea (sf)	CN I	Description		
	485	98 I	Paved park	ing, HSG C	,
	485		100.00% In	pervious A	rea
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description
6.0					Direct Entry Min To

Subcatchment 4.6S: Townhouse TDs





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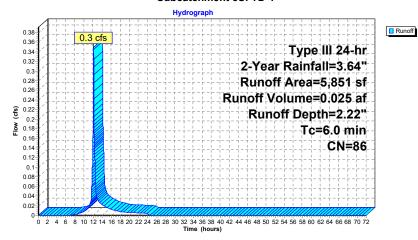
Summary for Subcatchment 5S: TD-1

Runoff = 0.3 cfs @ 12.09 hrs, Volume= 0.025 af, Depth= 2.22"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 2-Year Rainfall=3.64"

	Α	rea (sf)	CN	Description						
		3,021	98	Paved parking, HSG C						
		2,830	74	>75% Grass cover, Good, HSG C						
		5,851	86	Weighted A	verage					
		2,830		48.37% Pei	rvious Area	a				
		3,021		51.63% Imp	pervious Are	rea				
	Τ.	1	01	M-1!6.	0	Description				
,	Tc	Length		Slope Velocity Capacity Description						
<u>(r</u>	nin)	(feet)	(ft/ft	t) (ft/sec) (cfs)						
	6.0					Direct Entry, Min. To				

Subcatchment 5S: TD-1



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Thorndike Place - Proposed Conditions

Type III 24-hr 2-Year Rainfall=3.64"

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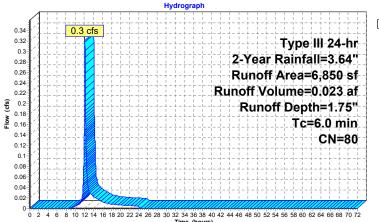
Summary for Subcatchment 6.1S: East driveway

Runoff = 0.3 cfs @ 12.09 hrs, Volume= 0.023 af, Depth= 1.75"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 2-Year Rainfall=3.64"

_	Α	rea (sf)	CN	Description							
		5,074	74	>75% Grass cover, Good, HSG C							
		1,776	98	Paved road	Paved roads w/curbs & sewers, HSG C						
		6,850	80	Weighted A	verage						
		5,074		74.07% Pe	rvious Area	a e e e e e e e e e e e e e e e e e e e					
		1,776		25.93% Imp	pervious Are	rea					
	Tc (min)	Length (feet)	Slop (ft/fi	,	Capacity (cfs)	Description					
	6.0					Direct Entry,					

Subcatchment 6.1S: East driveway



Runoff

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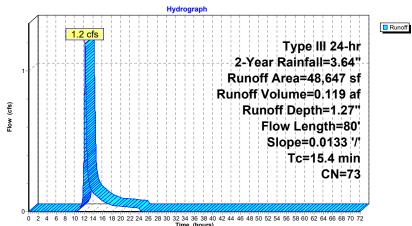
Summary for Subcatchment 6S: Bypass Towards Wetlands

Runoff = 1.2 cfs @ 12.23 hrs, Volume= 0.119 af, Depth= 1.27"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 2-Year Rainfall=3.64"

	Δ	rea (sf)	CN	Description					
-		13.497	_						
		35.043							
		107		tt) (ft/sec) (cfs) 3 0.06 Sheet Flow, Woods: Light underbrush n= 0.400 P2= 3.23"					
-		48.647	73	Weighted A	verage				
		48,540							
		107		0.22% Impe	ervious Are	a			
	Tc	Length	Slope	Velocity	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	14.5	50	0.0133	0.06		Sheet Flow,			
						Woods: Light underbrush n= 0.400 P2= 3.23"			
	0.9	30	0.0133	0.58					
_						Woodland Kv= 5.0 fps			
	15 4	80	Total						

Subcatchment 6S: Bypass Towards Wetlands



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Runoff

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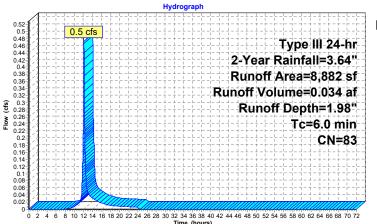
Summary for Subcatchment 7S: To Street

= 0.5 cfs @ 12.09 hrs, Volume= 0.034 af, Depth= 1.98"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 2-Year Rainfall=3.64"

_	Α	rea (sf)	CN	Description	Description Payed partiag USC C					
		3,419	98	Paved parking, HSG C						
		5,463	74	>75% Grass cover, Good, HSG C						
		8,882	83	Weighted A	Weighted Average					
		5,463		61.51% Pe	rvious Area	a e e e e e e e e e e e e e e e e e e e				
		3,419		38.49% Imp	pervious Are	rea				
	Tc (min)	Length (feet)	Slop (ft/ft		Capacity (cfs)	Description				
-	6.0			, , , , ,		Direct Entry, Min. Tc				

Subcatchment 7S: To Street



Runoff

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Primary =

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Summary for Pond 1P: Underground Infiltration System

 Inflow Area = Inflow = Inflow = Uniform = Inflow = In

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 7.58' @ 17.23 hrs Surf.Area= 7,556 sf Storage= 10,244 cf

0.1 cfs @ 17.23 hrs, Volume=

Plug-Flow detention time= 968.4 min calculated for 0.367 af (100% of inflow) Center-of-Mass det. time= 968.2 min (1,793.4 - 825.1)

Volume	Invert	Avail.Storage	Storage Description
#1	6.00'	19,495 cf	6.89'W x 14.06'L x 3.00'H StormTrap ST-1 Units (Irregular Shape)x 78
			22,668 cf Overall x 86.0% Voids

0.019 af

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.00'	0.520 in/hr Exfiltration over Surface area
#2	Primary	7.45'	15.0" Round Culvert
			L= 260.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 7.45' / 6.15' S= 0.0050 '/' Cc= 0.900
			n= 0.013, Flow Area= 1.23 sf

Discarded OutFlow Max=0.1 cfs @ 9.49 hrs HW=6.03' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.1 cfs)

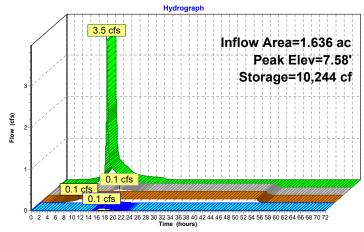
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Pond 1P: Underground Infiltration System





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Summary for Pond 2P: Rooftop Detention

0.366 ac,100.00% Impervious, Inflow Depth = 3.41" for 2-Year event Inflow Area =

0.104 af Inflow 1.3 cfs @ 12.08 hrs, Volume=

Outflow 0.2 cfs @ 12.55 hrs, Volume= 0.104 af, Atten= 84%, Lag= 27.9 min

Primary = 0.2 cfs @ 12.55 hrs, Volume= 0.104 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 57.26' @ 12.55 hrs Surf.Area= 7,500 sf Storage= 1,934 cf

Plug-Flow detention time= 151.5 min calculated for 0.104 af (100% of inflow)

Center-of-Mass det. time= 151.8 min (905.6 - 753.8)

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Volume	Inve	ert Avail.Stora	ige Storage D	escription	
#1	57.0	7,500	of Rooftop D	Detention (Prism	atic)Listed below (Recalc)
Elevation (fee		Surf.Area (sq-ft) (Inc.Store cubic-feet)	Cum.Store (cubic-feet)	
57.0	00	7,500	0	0	
58.0	00	7,500	7,500	7,500	
Device	Routing	Invert	Outlet Devices		
#1	Primary	8.02'	12.0" Round F	Roof Drain	
		I	L= 16.0' CPP,	mitered to confor	m to fill, Ke= 0.700
			Inlet / Outlet Inv	ert= 8.02' / 7.70'	S= 0.0200 '/' Cc= 0.900
		1	n= 0.013, Flow	Area= 0.79 sf	
#2	Device 1	57.00'	4.0" Horiz. Orif	ice/Grate C= 0.	600
		ĺ	Limited to weir f	low at low heads	

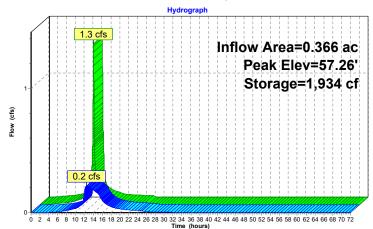
Primary OutFlow Max=0.2 cfs @ 12.55 hrs HW=57.26' (Free Discharge)
1=Roof Drain (Passes 0.2 cfs of 23.3 cfs potential flow)
2=Orifice/Grate (Orifice Controls 0.2 cfs @ 2.44 fps)

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Pond 2P: Rooftop Detention





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Summary for Pond 3P: Rain garden

Inflow Area = 0.157 ac, 25.93% Impervious, Inflow Depth = 1.75" for 2-Year event

Inflow = 0.3 cfs @ 12.09 hrs, Volume= 0.023 af

Outflow = 0.3 cfs @ 12.10 hrs, Volume= 0.023 af, Atten= 1%, Lag= 0.5 min

Discarded = 0.0 cfs @ 12.02 hrs, Volume= 0.009 af Primary = 0.3 cfs @ 12.10 hrs, Volume= 0.014 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 6.33' @ 12.10 hrs Surf.Area= 425 sf Storage= 179 cf

Plug-Flow detention time= 173.6 min calculated for 0.023 af (100% of inflow)

Center-of-Mass det. time= 173.7 min (1,010.0 - 836.3)

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Volume	Invert	Avail.S	Storage	Storage Descripti	on	
#1	5.60	'	463 cf	Custom Stage D	ata (Irregular)List	ed below (Recalc)
Elevation	on S	urf.Area	Perim.	Inc.Store	Cum.Store	Wet.Area
(fee	et)	(sq-ft)	(feet)	(cubic-feet)	(cubic-feet)	(sq-ft)
5.6	30	2	2.0	0	0	2
6.0	00	346	75.8	50	50	459
6.3	30	425	82.0	115	165	541
7.0	00	425	82.0	298	463	598
Device	Routing	Inve	rt Outle	et Devices		
#1	Discarded	5.6	0' 0.52	0 in/hr Exfiltration	over Surface ar	ea
#2 Primary 6.30		0' 22.0	long x 5.0' brea	dth Broad-Creste	d Rectangular Weir	
,		Head	d (feet) 0.20 0.40	0.60 0.80 1.00	1.20 1.40 1.60 1.80 2.00	
			2.50	3.00 3.50 4.00	4.50 5.00 5.50	
			Coef	(English) 2.34 2	.50 2.70 2.68 2.	68 2.66 2.65 2.65 2.65
				2.67 2.66 2.68		

Discarded OutFlow Max=0.0 cfs @ 12.02 hrs HW=6.31' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.0 cfs)

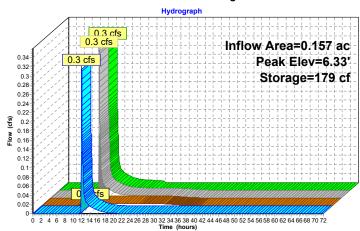
Primary OutFlow Max=0.3 cfs @ 12.10 hrs HW=6.33' (Free Discharge) —2=Broad-Crested Rectangular Weir (Weir Controls 0.3 cfs @ 0.43 fps)

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Pond 3P: Rain garden





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Type III 24-hr 2-Year Rainfall=3.64"
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Summary for Pond TD2:

Inflow Area	1 =	0.011 ac,100	0.00% Imperviou	s, Inflow [Depth = 3.4	1" for 2	2-Year event	
Inflow	=	0.0 cfs @	12.08 hrs, Volu	me=	0.003 af			
Outflow	=	0.0 cfs @	10.30 hrs, Volu	me=	0.003 af,	Atten= 9	5%, Lag= 0.0 m	iin
Discarded	=	0.0 cfs @	10.30 hrs, Volu	me=	0.003 af		-	
Primary	=	0.0 cfs @	0.00 hrs, Volu	me=	0.000 af			

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 7.35' @ 14.45 hrs Surf.Area= 152 sf Storage= 66 cf Flood Elev= 10.60' Surf.Area= 152 sf Storage= 300 cf

Plug-Flow detention time= 311.3 min calculated for 0.003 af (100% of inflow) Center-of-Mass det. time= 311.2 min (1,065.0 - 753.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	6.50'	91 cf	8.90'W x 17.06'L x 3.67'H Field A
			557 cf Overall - 329 cf Embedded = 228 cf x 40.0% Voids
#2A	7.00'	209 cf	StormTrap ST1 SingleTrap 2-6 Inside #1
			Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf
			Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf
			6.90' x 14.06' Core + 0.00' x 0.50' Border = 6.90' x 15.06' System
		300 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.50'	0.520 in/hr Exfiltration over Surface area
#2	Primary	10.60'	6.0" x 240.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Discarded OutFlow Max=0.0 cfs @ 10.30 hrs HW=6.54' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=6.50' (Free Discharge) 2=Orifice/Grate (Controls 0.0 cfs)

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Pond TD2: - Chamber Wizard Field A

Chamber Model = StormTrap ST1 SingleTrap 2-6 (StormTrap ST1 SingleTrap® Type VI)

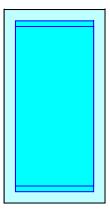
Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf

- 1 Chambers/Row x 14.06' Long = 14.06' Row Length +6.0" Border x 2 +12.0" End Stone x 2 = 17.06' Base Length
- 1 Rows x 82.7" Wide + 12.0" Side Stone x 2 = 8.90' Base Width 6.0" Base + 38.0" Chamber Height = 3.67' Field Height
- 1 Chambers x 208.5 cf = 208.5 cf Chamber Storage
- 1 Chambers x 307.1 cf + 21.8 cf Border = 328.9 cf Displacement

556.5 cf Field - 328.9 cf Chambers = 227.6 cf Stone x 40.0% Voids = 91.1 cf Stone Storage

Chamber Storage + Stone Storage = 299.6 cf = 0.007 af Overall Storage Efficiency = 53.8% Overall System Size = 17.06' x 8.90' x 3.67'

1 Chambers (plus border) 20.6 cy Field 8.4 cy Stone



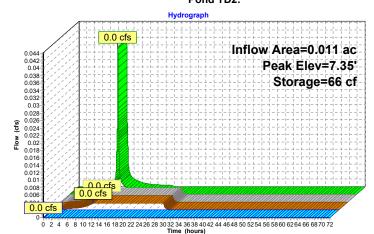


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Pond TD2:





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Summary for Pond TD3:

Inflow Area = 0.011 ac,100.00% Impervious, Inflow Depth = 3.41" for 2-Year event Inflow = 0.00 cfs @ 12.08 hrs, Volume= 0.003 af

Outflow = 0.0 cfs @ 10.30 hrs, Volume= 0.003 af, Atten= 95%, Lag= 0.0 min

Discarded = 0.0 cfs @ 10.30 hrs, Volume= 0.003 af Primary = 0.0 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 7.35' @ 14.45 hrs Surf.Area= 152 sf Storage= 66 cf Flood Elev= 10.60' Surf.Area= 152 sf Storage= 300 cf

Plug-Flow detention time= 311.3 min calculated for 0.003 af (100% of inflow) Center-of-Mass det. time= 311.2 min (1,065.0 - 753.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	6.50'	91 cf	8.90'W x 17.06'L x 3.67'H Field A
			557 cf Overall - 329 cf Embedded = 228 cf x 40.0% Voids
#2A	7.00'	209 cf	StormTrap ST1 SingleTrap 2-6 Inside #1
			Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf
			Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf
			6.90' x 14.06' Core + 0.00' x 0.50' Border = 6.90' x 15.06' System
		300 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.50'	0.520 in/hr Exfiltration over Surface area
#2	Primary	10.60'	6.0" x 240.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Discarded OutFlow Max=0.0 cfs @ 10.30 hrs HW=6.54' (Free Discharge) 1-Exfiltration (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=6.50' (Free Discharge) 2=Orifice/Grate (Controls 0.0 cfs)

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Pond TD3: - Chamber Wizard Field A

Chamber Model = StormTrap ST1 SingleTrap 2-6 (StormTrap ST1 SingleTrap® Type VI)

Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf

1 Chambers/Row x 14.06' Long = 14.06' Row Length +6.0" Border x 2 +12.0" End Stone x 2 = 17.06' Base Length

1 Rows x 82.7" Wide + 12.0" Side Stone x 2 = 8.90' Base Width 6.0" Base + 38.0" Chamber Height = 3.67' Field Height

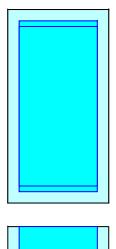
1 Chambers x 208.5 cf = 208.5 cf Chamber Storage

1 Chambers x 307.1 cf + 21.8 cf Border = 328.9 cf Displacement

556.5 cf Field - 328.9 cf Chambers = 227.6 cf Stone x 40.0% Voids = 91.1 cf Stone Storage

Chamber Storage + Stone Storage = 299.6 cf = 0.007 af Overall Storage Efficiency = 53.8% Overall System Size = 17.06' x 8.90' x 3.67'

1 Chambers (plus border) 20.6 cy Field 8.4 cy Stone

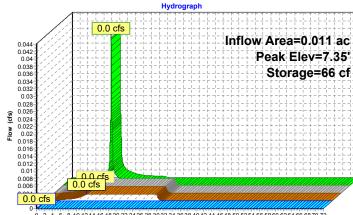


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Pond TD3:



0 2 4 6 8 10 1214 16 1820 22 2426 28 30 32 34 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70 72 Time (hours)



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Thorndike Place - Proposed Conditions

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Summary for Pond TD4:

Inflow Area	1 =	0.011 ac,100	0.00% Imperv	ious, Inflow I	Depth = $3.$.41" for	2-Year event
Inflow	=	0.0 cfs @	12.08 hrs, V	'olume=	0.003 af	f	
Outflow	=	0.0 cfs @	10.30 hrs, V	'olume=	0.003 af	f, Atten= 9	95%, Lag= 0.0 min
Discarded	=	0.0 cfs @	10.30 hrs, V	'olume=	0.003 af	f	=
Primary	=	0.0 cfs @	0.00 hrs, V	'olume=	0.000 af	f	

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 7.35' @ 14.45 hrs Surf.Area= 152 sf Storage= 66 cf Flood Elev= 10.60' Surf.Area= 152 sf Storage= 300 cf

Plug-Flow detention time= 311.3 min calculated for 0.003 af (100% of inflow) Center-of-Mass det. time= 311.2 min (1,065.0 - 753.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	6.50'	91 cf	8.90'W x 17.06'L x 3.67'H Field A
			557 cf Overall - 329 cf Embedded = 228 cf x 40.0% Voids
#2A	7.00'	209 cf	StormTrap ST1 SingleTrap 2-6 Inside #1
			Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf
			Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf
			6.90' x 14.06' Core + 0.00' x 0.50' Border = 6.90' x 15.06' System
		300 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.50'	0.520 in/hr Exfiltration over Surface area
#2	Primary	10.60'	6.0" x 240.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Discarded OutFlow Max=0.0 cfs @ 10.30 hrs HW=6.54' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=6.50' (Free Discharge) 2=Orifice/Grate (Controls 0.0 cfs)

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Thorndike Place - Proposed Conditions
Type III 24-hr 2-Year Rainfall=3.64"
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Pond TD4: - Chamber Wizard Field A

Chamber Model = StormTrap ST1 SingleTrap 2-6 (StormTrap ST1 SingleTrap® Type VI)

Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf

1 Chambers/Row x 14.06' Long = 14.06' Row Length +6.0" Border x 2 +12.0" End Stone x 2 = 17.06' Base Length

1 Rows x 82.7" Wide + 12.0" Side Stone x 2 = 8.90' Base Width 6.0" Base + 38.0" Chamber Height = 3.67' Field Height

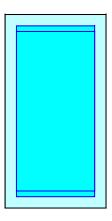
1 Chambers x 208.5 cf = 208.5 cf Chamber Storage

1 Chambers x 307.1 cf + 21.8 cf Border = 328.9 cf Displacement

556.5 cf Field - 328.9 cf Chambers = 227.6 cf Stone x 40.0% Voids = 91.1 cf Stone Storage

Chamber Storage + Stone Storage = 299.6 cf = 0.007 af Overall Storage Efficiency = 53.8% Overall System Size = 17.06' x 8.90' x 3.67'

1 Chambers (plus border) 20.6 cy Field 8.4 cy Stone





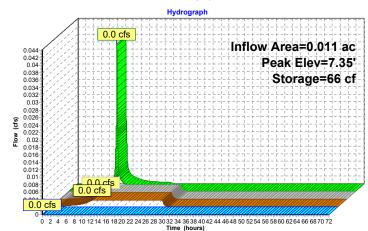
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Pond TD4:





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Summary for Pond TD5:

Inflow Area = 0.011 ac,100.00% Impervious, Inflow Depth = 3.41" for 2-Year event Inflow = 0.00 cfs @ 12.08 hrs, Volume= 0.003 af

Outflow = 0.0 cfs @ 10.30 hrs, Volume= 0.003 af, Atten= 95%, Lag= 0.0 min

Discarded = 0.0 cfs @ 10.30 hrs, Volume= 0.003 af Primary = 0.0 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 7.35' @ 14.45 hrs Surf.Area= 152 sf Storage= 66 cf Flood Elev= 10.60' Surf.Area= 152 sf Storage= 300 cf

Plug-Flow detention time= 311.3 min calculated for 0.003 af (100% of inflow) Center-of-Mass det. time= 311.2 min (1,065.0 - 753.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	6.50'	91 cf	8.90'W x 17.06'L x 3.67'H Field A
			557 cf Overall - 329 cf Embedded = 228 cf x 40.0% Voids
#2A	7.00'	209 cf	StormTrap ST1 SingleTrap 2-6 Inside #1
			Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf
			Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf
			6.90' x 14.06' Core + 0.00' x 0.50' Border = 6.90' x 15.06' System
		300 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.50'	0.520 in/hr Exfiltration over Surface area
#2	Primary	10.60'	6.0" x 240.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Discarded OutFlow Max=0.0 cfs @ 10.30 hrs HW=6.54' (Free Discharge) 1-Exfiltration (Exfiltration Controls 0.0 cfs)

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Pond TD5: - Chamber Wizard Field A

Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf

1 Chambers/Row x 14.06' Long = 14.06' Row Length +6.0" Border x 2 +12.0" End Stone x 2 = 17.06' Base Length

1 Rows x 82.7" Wide + 12.0" Side Stone x 2 = 8.90' Base Width 6.0" Base + 38.0" Chamber Height = 3.67' Field Height

1 Chambers x 208.5 cf = 208.5 cf Chamber Storage

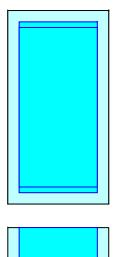
1 Chambers x 307.1 cf + 21.8 cf Border = 328.9 cf Displacement

556.5 cf Field - 328.9 cf Chambers = 227.6 cf Stone x 40.0% Voids = 91.1 cf Stone Storage

Chamber Storage + Stone Storage = 299.6 cf = 0.007 af Overall Storage Efficiency = 53.8% Overall System Size = 17.06' x 8.90' x 3.67'

1 Chambers (plus border) 20.6 cy Field 8.4 cy Stone

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Thorndike Place - Proposed Conditions

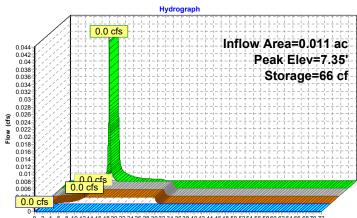
Type III 24-hr 2-Year Rainfall=3.64"

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Inflow
Outflow
Discarded

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Pond TD5:



0 2 4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 34 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70 72 Time (hours)

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Thorndike Place - Proposed Conditions
Type III 24-hr 2-Year Rainfall=3.64"
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Summary for Pond TD6:

Inflow Area	a =	0.011 ac,100	0.00% Imperv	ious, Inflow D	Depth = 3.41"	for 2-Year event	
Inflow	=	0.0 cfs @	12.08 hrs, V	olume=	0.003 af		
Outflow	=	0.0 cfs @	10.30 hrs, V	olume=	0.003 af, At	tten= 95%, Lag= 0.0 mir	n
Discarded	=	0.0 cfs @	10.30 hrs, V	olume=	0.003 af		
Drimon	_	വ വ ക്കേത്	0.00 brc \/	olumo-	0.000 of		

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 7.35' @ 14.45 hrs Surf.Area= 152 sf Storage= 66 cf Flood Elev= 10.60' Surf.Area= 152 sf Storage= 300 cf

Plug-Flow detention time= 311.3 min calculated for 0.003 af (100% of inflow) Center-of-Mass det. time= 311.2 min (1,065.0 - 753.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	6.50'	91 cf	8.90'W x 17.06'L x 3.67'H Field A
			557 cf Overall - 329 cf Embedded = 228 cf x 40.0% Voids
#2A	7.00'	209 cf	StormTrap ST1 SingleTrap 2-6 Inside #1
			Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf
			Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf
			6.90' x 14.06' Core + 0.00' x 0.50' Border = 6.90' x 15.06' System
		300 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.50'	0.520 in/hr Exfiltration over Surface area
#2	Primary	10.60'	6.0" x 240.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Discarded OutFlow Max=0.0 cfs @ 10.30 hrs HW=6.54' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=6.50' (Free Discharge) 2=Orifice/Grate (Controls 0.0 cfs)

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Thorndike Place - Proposed Conditions
Type III 24-hr 2-Year Rainfall=3.64"
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Pond TD6: - Chamber Wizard Field A

Chamber Model = StormTrap ST1 SingleTrap 2-6 (StormTrap ST1 SingleTrap® Type VI)

Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf

1 Chambers/Row x 14.06' Long = 14.06' Row Length +6.0" Border x 2 +12.0" End Stone x 2 = 17.06' Base Length

1 Rows x 82.7" Wide + 12.0" Side Stone x 2 = 8.90' Base Width 6.0" Base + 38.0" Chamber Height = 3.67' Field Height

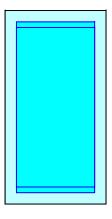
1 Chambers x 208.5 cf = 208.5 cf Chamber Storage

1 Chambers x 307.1 cf + 21.8 cf Border = 328.9 cf Displacement

556.5 cf Field - 328.9 cf Chambers = 227.6 cf Stone x 40.0% Voids = 91.1 cf Stone Storage

Chamber Storage + Stone Storage = 299.6 cf = 0.007 af Overall Storage Efficiency = 53.8% Overall System Size = 17.06' x 8.90' x 3.67'

1 Chambers (plus border) 20.6 cy Field 8.4 cy Stone

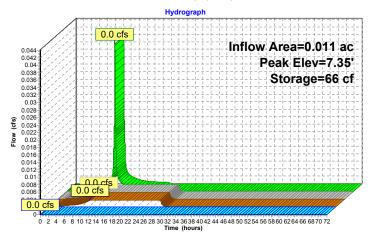




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Pond TD6:



Inflow
Outflow
Discarded
Primary

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Summary for Link 1L: Towards Wetlands

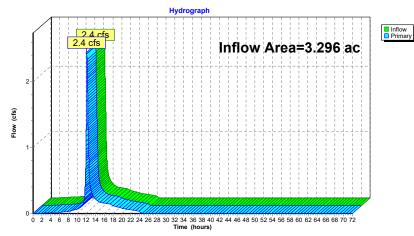
3.296 ac, 47.55% Impervious, Inflow Depth = 0.95" for 2-Year event 2.4 cfs @ 12.11 hrs, Volume= 0.260 af 2.4 cfs @ 12.11 hrs, Volume= 0.260 af, Atten= 0%, Lag= 0.0 Inflow Area =

Inflow

Primary = 0.260 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Link 1L: Towards Wetlands



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Summary for Link 2L: Towards Street

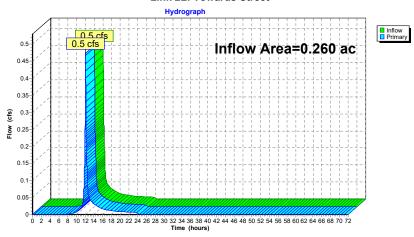
0.260 ac, 51.68% Impervious, Inflow Depth = 1.55" for 2-Year event Inflow Area =

0.5 cfs @ 12.09 hrs, Volume= 0.034 af Inflow

Primary = 0.5 cfs @ 12.09 hrs, Volume= 0.034 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Link 2L: Towards Street



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Thorndike Place - Proposed Conditions Type III 24-hr 2-Year Rainfall=3.64" Printed 6/4/2021

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Summary for Link 100L: Total Flows

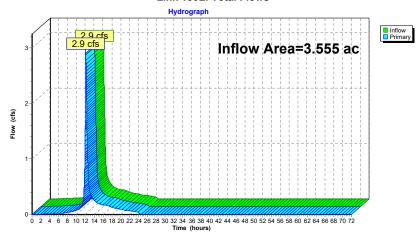
3.555 ac, 47.85% Impervious, Inflow Depth = 0.99" for 2-Year event 2.9 cfs @ 12.10 hrs, Volume= 0.294 af Inflow Area =

Inflow Primary = 2.9 cfs @ 12.10 hrs, Volume=

0.294 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Link 100L: Total Flows



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Thorndike Place - Proposed Conditions Type III 24-hr 10-Year Rainfall=5.79"

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Time span=0.00-72.00 hrs, dt=0.01 hrs, 7201 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1S: CB-1 Runoff Area=22,742 sf 72.16% Impervious Runoff Depth=4.75"
Tc=6.0 min CN=91 Runoff=2.8 cfs 0.207 af

Subcatchment 2.1S: Building

Runoff Area=16,789 sf 100.00% Impervious Runoff Depth=5.55"

Tc=6.0 min CN=98 Runoff=2.2 cfs 0.178 af

Tc=6.0 min CN=98 Runoff=2.2 cfs 0.178 at

Subcatchment 2S: Building Roof Runoff Area=15,928 sf 100.00% Impervious Runoff Depth=5.55"
Tc=6.0 min CN=98 Runoff=2.1 cfs 0.169 af

Subcatchment 3.1S: Backyard ADs Runoff Area=13,693 sf 8.51% Impervious Runoff Depth=3.10"

Flow Length=147' Tc=10.3 min UI Adjusted CN=75 Runoff=1.0 cfs 0.081 af

Subcatchment 3S: Townhouse Roofs Runoff Area=13,067 sf 100.00% Impervious Runoff Depth=5.55" Tc=6.0 min CN=98 Runoff=1.7 cfs 0.139 af

Subcatchment 4.2S: Townhouse TDs Runoff Area=485 sf 100.00% Impervious Runoff Depth=5.55"

Tc=6.0 min CN=98 Runoff=0.1 cfs 0.005 af

Subcatchment 4.3S: Townhouse TDs

Runoff Area=485 sf 100.00% Impervious Runoff Depth=5.55"

Tc=6.0 min CN=98 Runoff=0.1 cfs 0.005 af

Subcatchment 4.4S: Townhouse TDs Runoff Area=485 sf 100.00% Impervious Runoff Depth=5.55"

Tc=6.0 min CN=98 Runoff=0.1 cfs 0.005 af

Subcatchment 4.5S: Townhouse TDs Runoff Area=485 sf 100.00% Impervious Runoff Depth=5.55"

Tc=6.0 min CN=98 Runoff=0.1 cfs 0.005 af

Subcatchment 4.6S: Townhouse TDs Runoff Area=485 sf 100.00% Impervious Runoff Depth=5.55"

Tc=6.0 min CN=98 Runoff=0.1 cfs 0.005 af

Subcatchment 5S: TD-1 Runoff Area=5.851 sf 51.63% Impervious Runoff Depth=4.21"

Tc=6.0 min CN=86 Runoff=0.6 cfs 0.047 af

Subcatchment 6.1S: East driveway Runoff Area=6,850 sf 25.93% Impervious Runoff Depth=3.59"

Tc=6.0 min CN=80 Runoff=0.7 cfs 0.047 af

Subcatchment 6S: Bypass Towards Runoff Area=48,647 sf 0.22% Impervious Runoff Depth=2.92"

Flow Length=80' Slope=0.0133 '/' Tc=15.4 min CN=73 Runoff=2.8 cfs 0.271 af

Subcatchment 7S: To Street Runoff Area=8,882 sf 38.49% Impervious Runoff Depth=3.90"

Tc=6.0 min CN=83 Runoff=0.9 cfs 0.066 af

Pond 1P: Underground Infiltration System Peak Elev=7.92' Storage=12,466 cf Inflow=6.2 cfs 0.643 af

Discarded=0.1 cfs 0.375 af Primary=0.8 cfs 0.268 af Outflow=0.9 cfs 0.643 af

Pond 2P: Rooftop Detention Peak Elev=57.42' Storage=3,176 cf Inflow=2.1 cfs 0.169 af

Outflow=0.3 cfs 0.169 af

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Thorndike Place - Proposed Conditions Type III 24-hr 10-Year Rainfall=5.79"

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Pond 3P: Rain garden

Peak Elev=6.35' Storage=188 cf Inflow=0.7 cfs 0.047 af

Discarded=0.0 cfs 0.010 af Primary=0.7 cfs 0.037 af Outflow=0.7 cfs 0.047 af

Pond TD2: Peak Elev=7.96' Storage=129 cf Inflow=0.1 cfs 0.005 af

Discarded=0.0 cfs 0.005 af Primary=0.0 cfs 0.000 af Outflow=0.0 cfs 0.005 af

Pond TD3: Peak Elev=7.96' Storage=129 cf Inflow=0.1 cfs 0.005 af

Discarded=0.0 cfs 0.005 af Primary=0.0 cfs 0.000 af Outflow=0.0 cfs 0.005 af

Pond TD4: Peak Elev=7.96' Storage=129 cf Inflow=0.1 cfs 0.005 af Discarded=0.0 cfs 0.005 af Primary=0.0 cfs 0.000 af Outflow=0.0 cfs 0.005 af

Pond TD5: Peak Elev=7.96' Storage=129 cf Inflow=0.1 cfs 0.005 af Discarded=0.0 cfs 0.005 af Primary=0.0 cfs 0.000 af Outflow=0.0 cfs 0.005 af

Biodalada did did didda i Tilliany did did didda ii Ganiow did didda ii

Pond TD6: Peak Elev=7.96' Storage=129 cf Inflow=0.1 cfs 0.005 af Discarded=0.0 cfs 0.005 af Primary=0.0 cfs 0.000 af Outflow=0.0 cfs 0.005 af

Link 1L: Towards Wetlands Inflow=4.9 cfs 0.755 af

Primary=4.9 cfs 0.755 af

Link 2L: Towards Street Inflow=0.9 cfs 0.066 af

Primary=0.9 cfs 0.066 af

Link 100L: Total Flows Inflow=5.7 cfs 0.821 af

Primary=5.7 cfs 0.821 af

Total Runoff Area = 3.555 ac Runoff Volume = 1.232 af Average Runoff Depth = 4.16" 52.15% Pervious = 1.854 ac 47.85% Impervious = 1.701 ac

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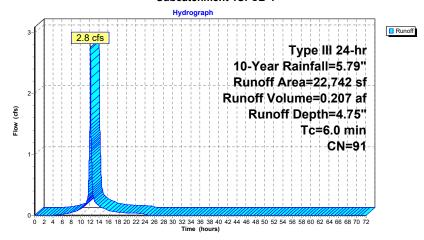
Summary for Subcatchment 1S: CB-1

Runoff = 2.8 cfs @ 12.08 hrs, Volume= 0.207 af, Depth= 4.75"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.79"

	Area (sf)	CN	Description						
	16,410	98	Paved park	ing, HSG C					
	6,332	74	>75% Gras	s cover, Go	ood, HSG C				
	22,742	91	Weighted A	Veighted Average					
	6,332		27.84% Per	rvious Area	l				
	16,410		72.16% lmp	pervious Are	rea				
(mi	Γc Length n) (feet)	Slope (ft/ft	,	Capacity (cfs)	Description				
6	.0				Direct Entry, Min. Tc				

Subcatchment 1S: CB-1



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Thorndike Place - Proposed Conditions

Type III 24-hr 10-Year Rainfall=5.79"

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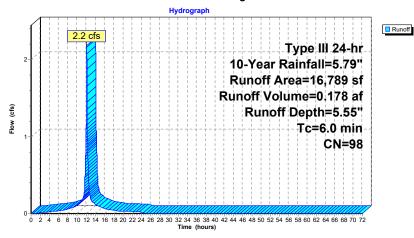
Summary for Subcatchment 2.1S: Building Roof-Southeast

Runoff = 2.2 cfs @ 12.08 hrs, Volume= 0.178 af, Depth= 5.55"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.79"

_	Α	rea (sf)	CN	Description	ı		
		16,789	98	Roofs, HSG C			
		16,789		100.00% In	npervious A	ırea	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
_	6.0				-	Direct Entry, Min. Tc	

Subcatchment 2.1S: Building Roof-Southeast



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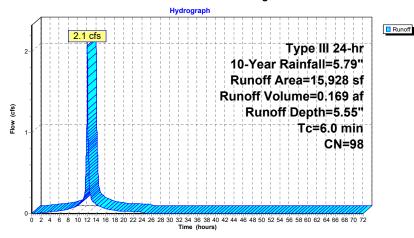
Summary for Subcatchment 2S: Building Roof

0.169 af, Depth= 5.55" Runoff 2.1 cfs @ 12.08 hrs, Volume=

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.79"

Ar	ea (sf)	CN E	Description		
	15,928	98 F	Roofs, HSC	C	
	15,928	1	00.00% In	npervious A	Area
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Min. Tc

Subcatchment 2S: Building Roof



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Thorndike Place - Proposed Conditions Type III 24-hr 10-Year Rainfall=5.79" Printed 6/4/2021

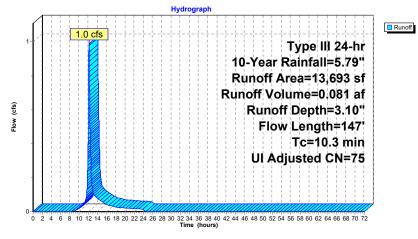
Summary for Subcatchment 3.1S: Backyard ADs

Runoff 1.0 cfs @ 12.14 hrs, Volume= 0.081 af, Depth= 3.10"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.79"

	Α	rea (sf)	CN	Adj Desc	Description					
		1,165	98	Unco	onnected pa	avement, HSG C				
		12,528	74	>75%	% Grass co	ver, Good, HSG C				
		13,693	76	75 Weig	hted Avera	ige, UI Adjusted				
		12,528		91.4	9% Perviou	is Area				
		1,165		8.51	% Impervio	us Area				
		1,165		100.	00% Uncor	nected				
	т.	1	01	\	0	Description				
	Tc	Length	Slope		Capacity	Description				
-	(min)	(feet)	(ft/ft)		(cfs)		_			
	9.4	50	0.0142	0.09		Sheet Flow,				
						Grass: Dense n= 0.240 P2= 3.23"				
	0.9	97	0.0154	1.86		Shallow Concentrated Flow,				
_						Grassed Waterway Kv= 15.0 fps				
	10.3	147	Total							

Subcatchment 3.1S: Backyard ADs



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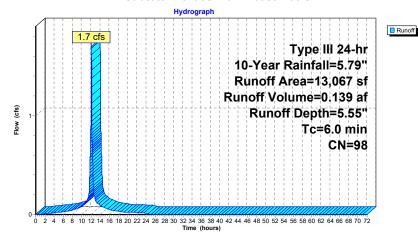
Summary for Subcatchment 3S: Townhouse Roofs

Runoff = 1.7 cfs @ 12.08 hrs, Volume= 0.139 af, Depth= 5.55"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.79"

A	rea (sf)	CN I	Description				
	13,067	98 I	Roofs, HSG C				
	13,067		100.00% Impervious Area				
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
6.0					Direct Entry, Min. Tc		

Subcatchment 3S: Townhouse Roofs



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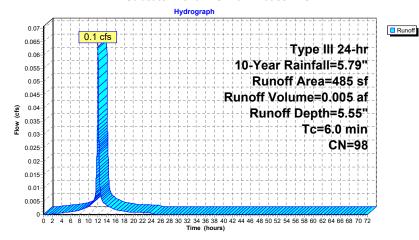
Summary for Subcatchment 4.2S: Townhouse TDs

Runoff = 0.1 cfs @ 12.08 hrs, Volume= 0.005 af, Depth= 5.55"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.79"

A	rea (sf)	CN [Description				
	485	98 F	Paved parking, HSG C				
	485	1	00.00% Impervious Area				
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
6.0					Direct Entry, Min. Tc		

Subcatchment 4.2S: Townhouse TDs



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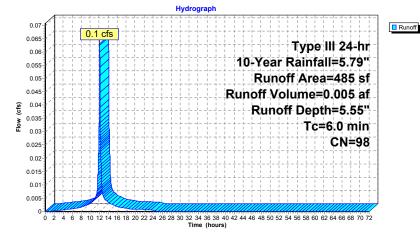
Summary for Subcatchment 4.3S: Townhouse TDs

Runoff = 0.1 cfs @ 12.08 hrs, Volume= 0.005 af, Depth= 5.55"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.79"

	Α	rea (sf)	CN [Description							
		485	98 F	Paved parking, HSG C							
Ī		485	•	100.00% Impervious Area							
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description					
	6.0				. ,	Direct Entry Min To					

Subcatchment 4.3S: Townhouse TDs



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Type III 24-hr 10-Year Rainfall=5.79"

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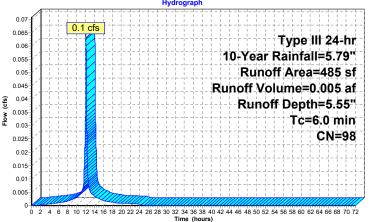
Summary for Subcatchment 4.4S: Townhouse TDs

Runoff = 0.1 cfs @ 12.08 hrs, Volume= 0.005 af, Depth= 5.55"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.79"

Α	rea (sf)	CN [Description						
	485	98 F	Paved parking, HSG C						
	485	1	00.00% Impervious Area						
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
6.0					Direct Entry Min To				

Subcatchment 4.4S: Townhouse TDs





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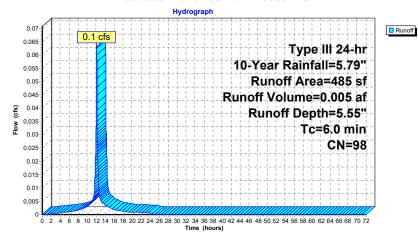
Summary for Subcatchment 4.5S: Townhouse TDs

Runoff = 0.1 cfs @ 12.08 hrs, Volume= 0.005 af, Depth= 5.55"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.79"

A	rea (sf)	CN [Description					
	485	98 F	Paved parking, HSG C					
	485	1	100.00% Impervious Area					
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
6.0					Direct Entry, Min. Tc			

Subcatchment 4.5S: Townhouse TDs



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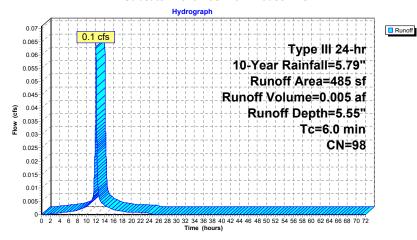
Summary for Subcatchment 4.6S: Townhouse TDs

Runoff = 0.1 cfs @ 12.08 hrs, Volume= 0.005 af, Depth= 5.55"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.79"

	rea (sf)	CN D	escription				
	485	98 F	Paved parking, HSG C				
	485	1	00.00% In	pervious A	Area		
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
6.0					Direct Entry, Min. Tc		

Subcatchment 4.6S: Townhouse TDs



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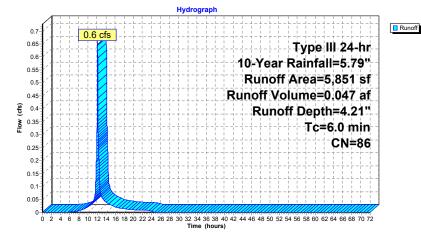
Summary for Subcatchment 5S: TD-1

Runoff = 0.6 cfs @ 12.09 hrs, Volume= 0.047 af, Depth= 4.21"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.79"

	Α	rea (sf)	CN I	Description				
		3,021	98 I	Paved park	ing, HSG C	С		
		2,830	74	>75% Ġras	s cover, Go	Good, HSG C		
		5,851	86 \	Weighted Average				
		2,830	4	48.37% Pervious Area				
		3,021		51.63% Impervious Area				
		Length	Slope	,	Capacity			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
	6.0					Direct Entry Min To		

Subcatchment 5S: TD-1



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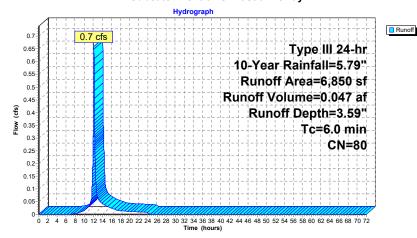
Summary for Subcatchment 6.1S: East driveway

Runoff = 0.7 cfs @ 12.09 hrs, Volume= 0.047 af, Depth= 3.59"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.79"

Α	rea (sf)	CN	Description	Description				
	5,074	74	>75% Gras	s cover, Go	ood, HSG C			
	1,776	98	Paved road	Paved roads w/curbs & sewers, HSG C				
	6,850	80	80 Weighted Average					
	5,074		74.07% Pervious Area					
	1,776		25.93% Impervious Area					
Tc (min)	Length (feet)	Slop (ft/f	,	Capacity (cfs)	Description			
6.0					Direct Entry,			

Subcatchment 6.1S: East driveway



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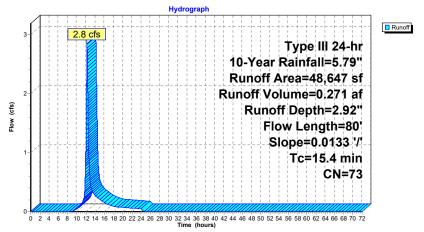
Summary for Subcatchment 6S: Bypass Towards Wetlands

Runoff = 2.8 cfs @ 12.21 hrs, Volume= 0.271 af, Depth= 2.92"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.79"

	A (-£)	ON	D					
	Area (sf)	CN	CN Description					
	13,497	70	Woods, Go	od, HSG C				
	35,043	74	>75% Gras	s cover, Go	ood, HSG C			
	107	98	Roofs, HSC	G C	<u> </u>			
	48,647	73	Weighted A	verage				
	48,540	!	99.78% Pei	rvious Area				
	107	(0.22% Impe	ervious Are	a			
			-					
To	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)		(cfs)	•			
14.5	50	0.0133	0.06		Sheet Flow,			
					Woods: Light underbrush n= 0.400 P2= 3.23"			
0.9	30	0.0133	0.58		Shallow Concentrated Flow,			
					Woodland Kv= 5.0 fps			
15.4	. 80	Total			·			

Subcatchment 6S: Bypass Towards Wetlands



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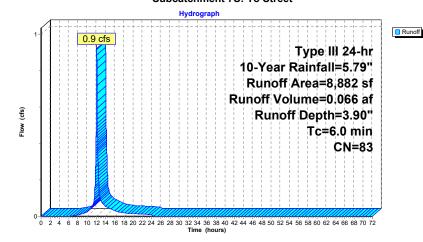
Summary for Subcatchment 7S: To Street

Runoff = 0.9 cfs @ 12.09 hrs, Volume= 0.066 af, Depth= 3.90"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.79"

A	rea (sf)	CN	Description					
	3,419	98	Paved park	Paved parking, HSG C				
	5,463	74	>75% Gras	>75% Grass cover, Good, HSG C				
·	8,882	83	Weighted A	Weighted Average				
	5,463		61.51% Pervious Area					
	3,419		38.49% Imp	38.49% Impervious Area				
Tc (min)	Length (feet)	Slop (ft/fi		Capacity (cfs)	Description			
6.0					Direct Entry, Min. Tc			

Subcatchment 7S: To Street



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Summary for Pond 1P: Underground Infiltration System

Primary = 0.8 cfs @ 12.96 hrs, Volume= 0.268 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 7.92' @ 12.96 hrs Surf.Area= 7,556 sf Storage= 12,466 cf

Plug-Flow detention time= 637.6 min calculated for 0.643 af (100% of inflow) Center-of-Mass det. time= 637.6 min (1,452.0-814.3)

Volume	Invert	Avail.Storage	Storage Description
#1	6.00'	19,495 cf	6.89'W x 14.06'L x 3.00'H StormTrap ST-1 Units (Irregular Shape)x 78
			22,668 cf Overall x 86.0% Voids

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.00'	0.520 in/hr Exfiltration over Surface area
#2	Primary	7.45'	15.0" Round Culvert
			L= 260.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 7.45' / 6.15' S= 0.0050 '/' Cc= 0.900
			n= 0.013, Flow Area= 1.23 sf

Discarded OutFlow Max=0.1 cfs @ 7.73 hrs HW=6.03' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.1 cfs)

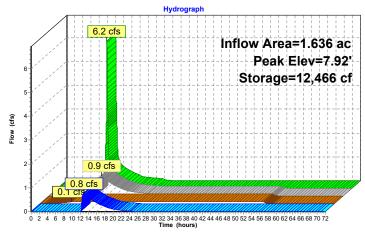
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Pond 1P: Underground Infiltration System





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Summary for Pond 2P: Rooftop Detention

0.366 ac,100.00% Impervious, Inflow Depth = 5.55" for 10-Year event Inflow Area =

2.1 cfs @ 12.08 hrs, Volume= 0.169 af Inflow

Outflow 0.3 cfs @ 12.60 hrs, Volume= 0.169 af, Atten= 87%, Lag= 31.2 min

Primary = 0.3 cfs @ 12.60 hrs, Volume= 0.169 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 57.42' @ 12.60 hrs Surf.Area= 7,500 sf Storage= 3,176 cf

Plug-Flow detention time= 159.8 min calculated for 0.169 af (100% of inflow)

Center-of-Mass det. time= 160.0 min (905.7 - 745.7)

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Volume	Inv	ert Avail.Stora	ge Storage D	escription	
#1	57.0	00' 7,500	cf Rooftop I	Detention (Prisn	natic)Listed below (Recalc)
Elevation (fee		Surf.Area (sq-ft) (c	Inc.Store cubic-feet)	Cum.Store (cubic-feet)	
57.0	00	7,500	0	0	
58.0	00	7,500	7,500	7,500	
Device	Routing	Invert (Outlet Devices		
#1	Primary	8.02' 1	2.0" Round F	Roof Drain	
	•	L	.= 16.0' CPP,	mitered to confo	rm to fill, Ke= 0.700
		I	nlet / Outlet Inv	ert= 8.02' / 7.70'	' S= 0.0200 '/' Cc= 0.900
		r	n= 0.013, Flow	Area= 0.79 sf	
#2	Device 1	57.00' 4	I.0" Horiz. Orif	fice/Grate C= 0	0.600
		L	imited to weir	flow at low heads	3

Primary OutFlow Max=0.3 cfs @ 12.60 hrs HW=57.42' (Free Discharge)
1=Roof Drain (Passes 0.3 cfs of 23.3 cfs potential flow)
2=Orifice/Grate (Orifice Controls 0.3 cfs @ 3.13 fps)

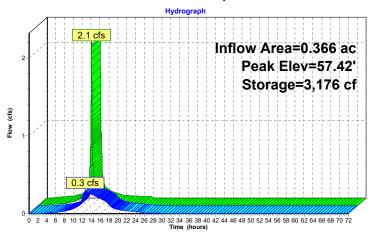
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Pond 2P: Rooftop Detention





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Summary for Pond 3P: Rain garden

Inflow Area = 0.157 ac, 25.93% Impervious, Inflow Depth = 3.59" for 10-Year event

Inflow = 0.7 cfs @ 12.09 hrs, Volume= 0.047 af

Outflow = 0.7 cfs @ 12.09 hrs, Volume= 0.047 af, Atten= 0%, Lag= 0.4 min

Discarded = 0.0 cfs @ 11.47 hrs, Volume= 0.010 af Primary = 0.7 cfs @ 12.09 hrs, Volume= 0.037 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 6.35' @ 12.09 hrs Surf.Area= 425 sf Storage= 188 cf

Plug-Flow detention time= 91.8 min calculated for 0.047 af (100% of inflow) Center-of-Mass det. time= 92.0 min (907.6 - 815.6)

Volume	Inve	rt Avail.	Storage	Storage Description	n		
#1	5.6	0'	463 cf	Custom Stage Da	ata (Irregular)Liste	ed below (Recalc)	
Elevatio		Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
5.6	60	2	2.0	0	0	2	
6.0	00	346	75.8	50	50	459	
6.3	30	425	82.0	115	165	541	
7.0	00	425	82.0	298	463	598	
Device	Routing	Inve	ert Outle	et Devices			
#1	Discarde	d 5.6	60' 0.52	0 in/hr Exfiltration	over Surface are	a	
#2	Primary	6.3	30' 22.0 '	long x 5.0' bread	th Broad-Crested	l Rectangular Weir	
	•		Head	d (feet) 0.20 0.40	0.60 0.80 1.00 1	1.20 1.40 1.60 1.80	2.00
			Coef	3.00 3.50 4.00 4 (English) 2.34 2. 2.67 2.66 2.68 2	50 2.70 2.68 2.6	68 2.66 2.65 2.65 2. 88	65

Discarded OutFlow Max=0.0 cfs @ 11.47 hrs HW=6.30' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.0 cfs)

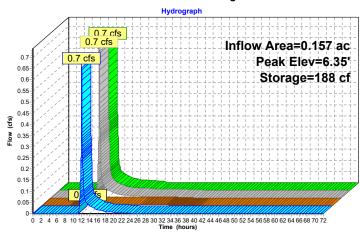
Primary OutFlow Max=0.6 cfs @ 12.09 hrs HW=6.35' (Free Discharge) —2=Broad-Crested Rectangular Weir (Weir Controls 0.6 cfs @ 0.54 fps)

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Pond 3P: Rain garden





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Summary for Pond TD2:

Inflow Area	1 =	0.011 ac,100	0.00% Impervious, Inflow	Depth = 5.55" for 10-Year event	
Inflow	=	0.1 cfs @	12.08 hrs, Volume=	0.005 af	
Outflow	=	0.0 cfs @	8.76 hrs, Volume=	0.005 af, Atten= 97%, Lag= 0.0 min	
Discarded	=	0.0 cfs @	8.76 hrs, Volume=	0.005 af	
Primary	=	0.0 cfs @	0.00 hrs Volume=	0 000 af	

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 7.96' @ 15.91 hrs Surf.Area= 152 sf Storage= 129 cf Flood Elev= 10.60' Surf.Area= 152 sf Storage= 300 cf

Plug-Flow detention time= 608.9 min calculated for 0.005 af (100% of inflow) Center-of-Mass det. time= 608.9 min (1,354.6 - 745.7)

Volume	Invert	Avail.Storage	Storage Description
#1A	6.50'	91 cf	8.90'W x 17.06'L x 3.67'H Field A
			557 cf Overall - 329 cf Embedded = 228 cf x 40.0% Voids
#2A	7.00'	209 cf	StormTrap ST1 SingleTrap 2-6 Inside #1
			Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf
			Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf
			6.90' x 14.06' Core + 0.00' x 0.50' Border = 6.90' x 15.06' System
		300 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.50'	0.520 in/hr Exfiltration over Surface area
#2	Primary	10.60'	6.0" x 240.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Discarded OutFlow Max=0.0 cfs @ 8.76 hrs HW=6.54' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=6.50' (Free Discharge) 2=Orifice/Grate (Controls 0.0 cfs)

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Pond TD2: - Chamber Wizard Field A

Chamber Model = StormTrap ST1 SingleTrap 2-6 (StormTrap ST1 SingleTrap® Type VI)

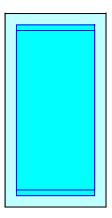
Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf

- 1 Chambers/Row x 14.06' Long = 14.06' Row Length +6.0" Border x 2 + 12.0" End Stone x 2 = 17.06' Base Length
- 1 Rows x 82.7" Wide + 12.0" Side Stone x 2 = 8.90' Base Width 6.0" Base + 38.0" Chamber Height = 3.67' Field Height
- 1 Chambers x 208.5 cf = 208.5 cf Chamber Storage
- 1 Chambers x 307.1 cf + 21.8 cf Border = 328.9 cf Displacement

556.5 cf Field - 328.9 cf Chambers = 227.6 cf Stone x 40.0% Voids = 91.1 cf Stone Storage

Chamber Storage + Stone Storage = 299.6 cf = 0.007 af Overall Storage Efficiency = 53.8% Overall System Size = 17.06' x 8.90' x 3.67'

1 Chambers (plus border) 20.6 cy Field 8.4 cy Stone





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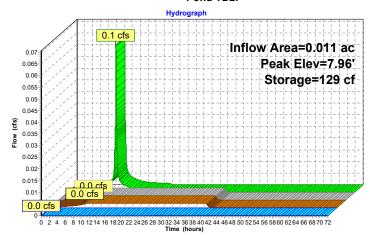
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Pond TD2:



☐ Inflow☐ Outflow☐ Discarded☐ Primary

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Summary for Pond TD3:

 Inflow Area = Inflow = O.011 ac,100.00% Impervious, Inflow Depth = 5.55" for 10-Year event

 Inflow = O.005 af
 0.1 cfs @ 12.08 hrs, Volume= 0.005 af

 Outflow = O.0 cfs @ 8.76 hrs, Volume= 0.005 af, Atten= 97%, Lag= 0.0 min

 Discarded = Primary = 0.0 cfs @ 0.00 fs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 7.96' @ 15.91 hrs Surf.Area= 152 sf Storage= 129 cf Flood Elev= 10.60' Surf.Area= 152 sf Storage= 300 cf

Plug-Flow detention time= 608.9 min calculated for 0.005 af (100% of inflow) Center-of-Mass det. time= 608.9 min (1,354.6 - 745.7)

Volume	Invert	Avail.Storage	Storage Description
#1A	6.50'	91 cf	8.90'W x 17.06'L x 3.67'H Field A
			557 cf Overall - 329 cf Embedded = 228 cf x 40.0% Voids
#2A	7.00'	209 cf	StormTrap ST1 SingleTrap 2-6 Inside #1
			Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf
			Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf
			6.90' x 14.06' Core + 0.00' x 0.50' Border = 6.90' x 15.06' System
		300 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.50'	0.520 in/hr Exfiltration over Surface area
#2	Primary	10.60'	6.0" x 240.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Discarded OutFlow Max=0.0 cfs @ 8.76 hrs HW=6.54' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=6.50' (Free Discharge)
2=Orifice/Grate (Controls 0.0 cfs)

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Pond TD3: - Chamber Wizard Field A

Chamber Model = StormTrap ST1 SingleTrap 2-6 (StormTrap ST1 SingleTrap® Type VI)

Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf

1 Chambers/Row x 14.06' Long = 14.06' Row Length +6.0" Border x 2 +12.0" End Stone x 2 = 17.06' Base Length

1 Rows x 82.7" Wide + 12.0" Side Stone x 2 = 8.90' Base Width 6.0" Base + 38.0" Chamber Height = 3.67' Field Height

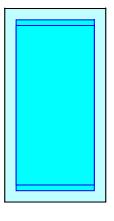
1 Chambers x 208.5 cf = 208.5 cf Chamber Storage

1 Chambers x 307.1 cf + 21.8 cf Border = 328.9 cf Displacement

556.5 cf Field - 328.9 cf Chambers = 227.6 cf Stone x 40.0% Voids = 91.1 cf Stone Storage

Chamber Storage + Stone Storage = 299.6 cf = 0.007 af Overall Storage Efficiency = 53.8% Overall System Size = 17.06' x 8.90' x 3.67'

1 Chambers (plus border) 20.6 cv Field 8.4 cy Stone





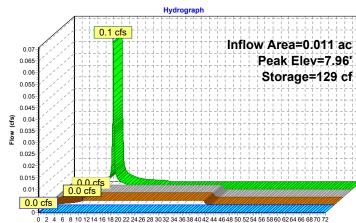
2340700-PR-2021-06-03

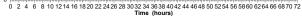
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Thorndike Place - Proposed Conditions Type III 24-hr 10-Year Rainfall=5.79" Printed 6/4/2021

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Pond TD3:





Inflow
Outflow
Discarded

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Thorndike Place - Proposed Conditions

Type III 24-hr 10-Year Rainfall=5.79"

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Summary for Pond TD4:

Inflow Area	a =	0.011 ac,100	0.00% Impervious, Inflow D	Depth = 5.55" for 10-Year event	
Inflow	=	0.1 cfs @	12.08 hrs, Volume=	0.005 af	
Outflow	=	0.0 cfs @	8.76 hrs, Volume=	0.005 af, Atten= 97%, Lag= 0.0 min	
Discarded	=	0.0 cfs @	8.76 hrs, Volume=	0.005 af	
Primary	=	0.0 cfs @	0.00 hrs Volume=	0.000 af	

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 7.96' @ 15.91 hrs Surf.Area= 152 sf Storage= 129 cf Flood Elev= 10.60' Surf.Area= 152 sf Storage= 300 cf

Plug-Flow detention time= 608.9 min calculated for 0.005 af (100% of inflow) Center-of-Mass det. time= 608.9 min (1,354.6 - 745.7)

Volume	Invert	Avail.Storage	Storage Description
#1A	6.50'	91 cf	8.90'W x 17.06'L x 3.67'H Field A
			557 cf Overall - 329 cf Embedded = 228 cf x 40.0% Voids
#2A	7.00'	209 cf	StormTrap ST1 SingleTrap 2-6 Inside #1
			Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf
			Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf
			6.90' x 14.06' Core + 0.00' x 0.50' Border = 6.90' x 15.06' System
		300 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.50'	0.520 in/hr Exfiltration over Surface area
#2	Primary	10.60'	6.0" x 240.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Discarded OutFlow Max=0.0 cfs @ 8.76 hrs HW=6.54' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=6.50' (Free Discharge) 2=Orifice/Grate (Controls 0.0 cfs)

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Thorndike Place - Proposed Conditions
Type III 24-hr 10-Year Rainfall=5.79"
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Pond TD4: - Chamber Wizard Field A

Chamber Model = StormTrap ST1 SingleTrap 2-6 (StormTrap ST1 SingleTrap® Type VI)

Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf

1 Chambers/Row x 14.06' Long = 14.06' Row Length +6.0" Border x 2 +12.0" End Stone x 2 = 17.06' Base Length

1 Rows x 82.7" Wide + 12.0" Side Stone x 2 = 8.90' Base Width 6.0" Base + 38.0" Chamber Height = 3.67' Field Height

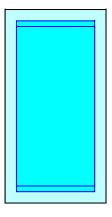
1 Chambers x 208.5 cf = 208.5 cf Chamber Storage

1 Chambers x 307.1 cf + 21.8 cf Border = 328.9 cf Displacement

556.5 cf Field - 328.9 cf Chambers = 227.6 cf Stone x 40.0% Voids = 91.1 cf Stone Storage

Chamber Storage + Stone Storage = 299.6 cf = 0.007 af Overall Storage Efficiency = 53.8% Overall System Size = 17.06' x 8.90' x 3.67'

1 Chambers (plus border) 20.6 cy Field 8.4 cy Stone





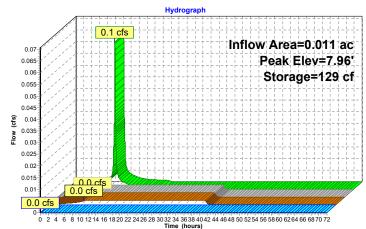
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Pond TD4:





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Summary for Pond TD5:

0.011 ac,100.00% Impervious, Inflow Depth = 5.55" for 10-Year event Inflow Area = 0.1 cfs @ 12.08 hrs, Volume= Inflow 0.005 af Outflow = 0.0 cfs @ 8.76 hrs, Volume= 0.005 af, Atten= 97%, Lag= 0.0 min Discarded = 0.0 cfs @ 8.76 hrs, Volume= 0.005 af 0.0 cfs @ 0.00 hrs, Volume= 0.000 af Primary =

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 7.96' @ 15.91 hrs Surf.Area= 152 sf Storage= 129 cf Flood Elev= 10.60' Surf.Area= 152 sf Storage= 300 cf

Plug-Flow detention time= 608.9 min calculated for 0.005 af (100% of inflow) Center-of-Mass det. time= 608.9 min (1,354.6 - 745.7)

Volume	Invert	Avail.Storage	Storage Description
#1A	6.50'	91 cf	8.90'W x 17.06'L x 3.67'H Field A
			557 cf Overall - 329 cf Embedded = 228 cf x 40.0% Voids
#2A	7.00'	209 cf	StormTrap ST1 SingleTrap 2-6 Inside #1
			Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf
			Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf
			6.90' x 14.06' Core + 0.00' x 0.50' Border = 6.90' x 15.06' System
		300 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.50'	0.520 in/hr Exfiltration over Surface area
#2	Primary	10.60'	6.0" x 240.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Discarded OutFlow Max=0.0 cfs @ 8.76 hrs HW=6.54' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=6.50' (Free Discharge) 2=Orifice/Grate (Controls 0.0 cfs)

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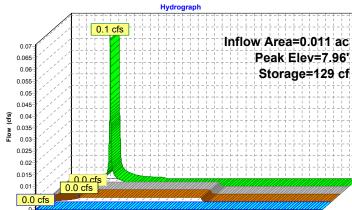
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Thorndike Place - Proposed Conditions
Type III 24-hr 10-Year Rainfall=5.79"
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Inflow
Outflow
Discarded

Pond TD5:





Pond TD5: - Chamber Wizard Field A

Chamber Model = StormTrap ST1 SingleTrap 2-6 (StormTrap ST1 SingleTrap® Type VI)

Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf

1 Chambers/Row x 14.06' Long = 14.06' Row Length +6.0" Border x 2 +12.0" End Stone x 2 = 17.06' Base Length

1 Rows x 82.7" Wide + 12.0" Side Stone x 2 = 8.90' Base Width 6.0" Base + 38.0" Chamber Height = 3.67' Field Height

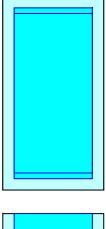
1 Chambers x 208.5 cf = 208.5 cf Chamber Storage

1 Chambers x 307.1 cf + 21.8 cf Border = 328.9 cf Displacement

556.5 cf Field - 328.9 cf Chambers = 227.6 cf Stone x 40.0% Voids = 91.1 cf Stone Storage

Chamber Storage + Stone Storage = 299.6 cf = 0.007 af Overall Storage Efficiency = 53.8% Overall System Size = 17.06' x 8.90' x 3.67'

1 Chambers (plus border) 20.6 cy Field 8.4 cy Stone





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Thorndike Place - Proposed Conditions

Type III 24-hr 10-Year Rainfall=5.79"

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Summary for Pond TD6:

Inflow Area	a =	0.011 ac,100	.00% Imperviou	us, Inflow De	pth = 5.55"	for 10-Ye	ar event
Inflow	=	0.1 cfs @	12.08 hrs, Volu	ıme=	0.005 af		
Outflow	=	0.0 cfs @	8.76 hrs, Volu	ıme=	0.005 af, At	ten= 97%, I	Lag= 0.0 min
Discarded	=	0.0 cfs @	8.76 hrs, Volu	ıme=	0.005 af		-
Drimary	_	∩ ∩ cfc @	0.00 hre Volu	ıma-	0.000 of		

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 7.96' @ 15.91 hrs Surf.Area= 152 sf Storage= 129 cf Flood Elev= 10.60' Surf.Area= 152 sf Storage= 300 cf

Plug-Flow detention time= 608.9 min calculated for 0.005 af (100% of inflow) Center-of-Mass det. time= 608.9 min (1,354.6-745.7)

Volume	Invert	Avail.Storage	Storage Description
#1A	6.50'	91 cf	8.90'W x 17.06'L x 3.67'H Field A
			557 cf Overall - 329 cf Embedded = 228 cf x 40.0% Voids
#2A	7.00'	209 cf	StormTrap ST1 SingleTrap 2-6 Inside #1
			Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf
			Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf
			6.90' x 14.06' Core + 0.00' x 0.50' Border = 6.90' x 15.06' System
		300 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.50'	0.520 in/hr Exfiltration over Surface area
#2	Primary	10.60'	6.0" x 240.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Discarded OutFlow Max=0.0 cfs @ 8.76 hrs HW=6.54' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=6.50' (Free Discharge) 2=Orifice/Grate (Controls 0.0 cfs)

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Thorndike Place - Proposed Conditions

Type III 24-hr 10-Year Rainfall=5.79"

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Pond TD6: - Chamber Wizard Field A

Chamber Model = StormTrap ST1 SingleTrap 2-6 (StormTrap ST1 SingleTrap® Type VI)

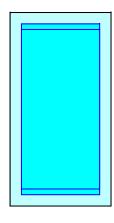
Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf

- 1 Chambers/Row x 14.06' Long = 14.06' Row Length +6.0" Border x 2 + 12.0" End Stone x 2 = 17.06' Base Length
- 1 Rows x 82.7" Wide + 12.0" Side Stone x 2 = 8.90' Base Width 6.0" Base + 38.0" Chamber Height = 3.67' Field Height
- 1 Chambers x 208.5 cf = 208.5 cf Chamber Storage
- 1 Chambers x 307.1 cf + 21.8 cf Border = 328.9 cf Displacement

556.5 cf Field - 328.9 cf Chambers = 227.6 cf Stone x 40.0% Voids = 91.1 cf Stone Storage

Chamber Storage + Stone Storage = 299.6 cf = 0.007 af Overall Storage Efficiency = 53.8% Overall System Size = 17.06' x 8.90' x 3.67'

1 Chambers (plus border) 20.6 cy Field 8.4 cy Stone





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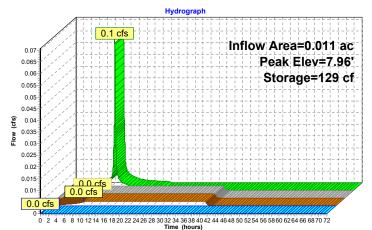
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Pond TD6:



Inflow
Outflow
Discarded
Primary

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Summary for Link 1L: Towards Wetlands

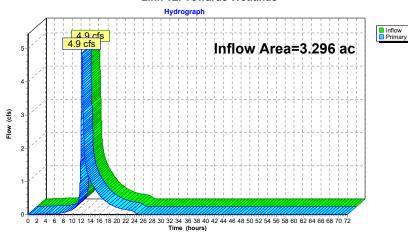
3.296 ac, 47.55% Impervious, Inflow Depth = 2.75" for 10-Year event 4.9 cfs @ 12.12 hrs, Volume= 0.755 af 4.9 cfs @ 12.12 hrs, Volume= 0.755 af, Atten= 0%, Lag= 0.0 n Inflow Area =

Inflow

Primary = 0.755 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Link 1L: Towards Wetlands



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Summary for Link 2L: Towards Street

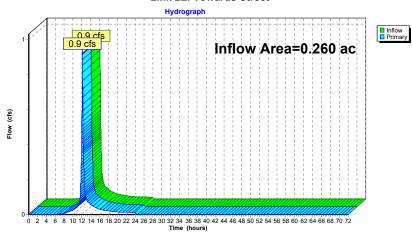
Inflow Area = 0.260 ac, 51.68% Impervious, Inflow Depth = 3.06" for 10-Year event

Inflow = 0.9 cfs @ 12.09 hrs, Volume= 0.066 af

Primary = 0.9 cfs @ 12.09 hrs, Volume= 0.066 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Link 2L: Towards Street



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Summary for Link 100L: Total Flows

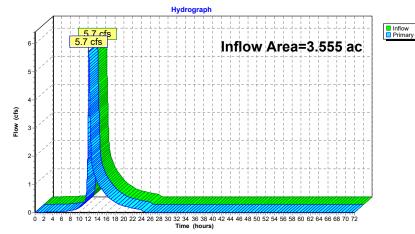
Inflow Area = 3.555 ac, 47.85% Impervious, Inflow Depth = 2.77" for 10-Year event

Inflow = 5.7 cfs @ 12.11 hrs, Volume= 0.821 af

Primary = 5.7 cfs @ 12.11 hrs, Volume= 0.821 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Link 100L: Total Flows



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Pond 2P: Rooftop Detention

Thorndike Place - Proposed Conditions Type III 24-hr 25-Year Rainfall=7.49"

Peak Elev=57.56' Storage=4,196 cf Inflow=2.7 cfs 0.221 af

Outflow=0.3 cfs 0.221 af

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Time span=0.00-72.00 hrs, dt=0.01 hrs, 7201 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Reach routing by Stor-ind+1	rans method - Pond routing by Stor-Ind method
Subcatchment 1S: CB-1	Runoff Area=22,742 sf 72.16% Impervious Runoff Depth=6.42" Tc=6.0 min CN=91 Runoff=3.7 cfs 0.279 af
Subcatchment 2.1S: Building	Runoff Area=16,789 sf 100.00% Impervious Runoff Depth=7.25" Tc=6.0 min CN=98 Runoff=2.8 cfs 0.233 af
Subcatchment 2S: Building Roof	Runoff Area=15,928 sf 100.00% Impervious Runoff Depth=7.25" Tc=6.0 min CN=98 Runoff=2.7 cfs 0.221 af
Subcatchment 3.1S: Backyard ADs Flow Length	Runoff Area=13,693 sf 8.51% Impervious Runoff Depth=4.58" th=147' Tc=10.3 min UI Adjusted CN=75 Runoff=1.5 cfs 0.120 af
Subcatchment 3S: Townhouse Roofs	Runoff Area=13,067 sf 100.00% Impervious Runoff Depth=7.25" Tc=6.0 min CN=98 Runoff=2.2 cfs 0.181 af
Subcatchment 4.2S: Townhouse TDs	Runoff Area=485 sf 100.00% Impervious Runoff Depth=7.25" Tc=6.0 min CN=98 Runoff=0.1 cfs 0.007 af
Subcatchment 4.3S: Townhouse TDs	Runoff Area=485 sf 100.00% Impervious Runoff Depth=7.25" Tc=6.0 min CN=98 Runoff=0.1 cfs 0.007 af
Subcatchment 4.4S: Townhouse TDs	Runoff Area=485 sf 100.00% Impervious Runoff Depth=7.25" Tc=6.0 min CN=98 Runoff=0.1 cfs 0.007 af
Subcatchment 4.5S: Townhouse TDs	Runoff Area=485 sf 100.00% Impervious Runoff Depth=7.25" Tc=6.0 min CN=98 Runoff=0.1 cfs 0.007 af
Subcatchment 4.6S: Townhouse TDs	Runoff Area=485 sf 100.00% Impervious Runoff Depth=7.25" Tc=6.0 min CN=98 Runoff=0.1 cfs 0.007 af
Subcatchment 5S: TD-1	Runoff Area=5,851 sf 51.63% Impervious Runoff Depth=5.84" Tc=6.0 min CN=86 Runoff=0.9 cfs 0.065 af
Subcatchment 6.1S: East driveway	Runoff Area=6,850 sf 25.93% Impervious Runoff Depth=5.15" Tc=6.0 min CN=80 Runoff=0.9 cfs 0.067 af
Subcatchment 6S: Bypass Towards Flow Length=80	Runoff Area=48,647 sf 0.22% Impervious Runoff Depth=4.36" 0' Slope=0.0133 '/' Tc=15.4 min CN=73 Runoff=4.3 cfs 0.406 af
Subcatchment 7S: To Street	Runoff Area=8,882 sf 38.49% Impervious Runoff Depth=5.49" Tc=6.0 min CN=83 Runoff=1.3 cfs 0.093 af
Pond 1P: Underground Infiltration Syster Discarded=0.	n Peak Elev=8.30' Storage=14,959 cf Inflow=8.3 cfs 0.867 af .1 cfs 0.388 af Primary=2.3 cfs 0.479 af Outflow=2.4 cfs 0.867 af

Thorndike Place - Proposed Conditions 2340700-PR-2021-06-03 Type III 24-hr 25-Year Rainfall=7.49" Printed 6/4/2021

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Pond 3P: Rain garden Peak Elev=6.37' Storage=195 cf Inflow=0.9 cfs 0.067 af Discarded=0.0 cfs 0.010 af Primary=0.9 cfs 0.057 af Outflow=0.9 cfs 0.067 af

Pond TD2: Peak Elev=8.49' Storage=183 cf Inflow=0.1 cfs 0.007 af Discarded=0.0 cfs 0.007 af Primary=0.0 cfs 0.000 af Outflow=0.0 cfs 0.007 af

Pond TD3:

Peak Elev=8.49' Storage=183 cf Inflow=0.1 cfs 0.007 af Discarded=0.0 cfs 0.007 af Primary=0.0 cfs 0.000 af Outflow=0.0 cfs 0.007 af

Pond TD4: Peak Elev=8.49' Storage=183 cf Inflow=0.1 cfs 0.007 af

Discarded=0.0 cfs 0.007 af Primary=0.0 cfs 0.000 af Outflow=0.0 cfs 0.007 af

Peak Elev=8.49' Storage=183 cf $\,$ Inflow=0.1 cfs $\,$ 0.007 af $\,$ Discarded=0.0 cfs $\,$ 0.007 af $\,$ Primary=0.0 cfs $\,$ 0.000 af $\,$ Outflow=0.0 cfs $\,$ 0.007 af Pond TD5:

Peak Elev=8.49' Storage=183 cf Inflow=0.1 cfs 0.007 af Pond TD6: Discarded=0.0 cfs 0.007 af Primary=0.0 cfs 0.000 af Outflow=0.0 cfs 0.007 af

Inflow=7.7 cfs 1.175 af Link 1L: Towards Wetlands Primary=7.7 cfs 1.175 af

Link 2L: Towards Street Inflow=1.3 cfs 0.093 af

Primary=1.3 cfs 0.093 af

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Inflow=8.6 cfs 1.268 af Link 100L: Total Flows

Primary=8.6 cfs 1.268 af

Total Runoff Area = 3.555 ac Runoff Volume = 1.700 af Average Runoff Depth = 5.74" 52.15% Pervious = 1.854 ac 47.85% Impervious = 1.701 ac

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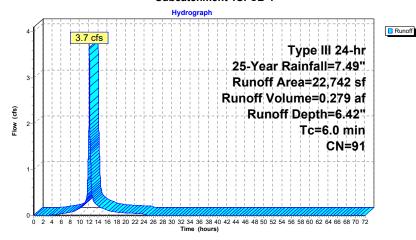
Summary for Subcatchment 1S: CB-1

Runoff = 3.7 cfs @ 12.08 hrs, Volume= 0.279 af, Depth= 6.42"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=7.49"

	Area (sf)	CN	Description						
	16,410	98	Paved parking, HSG C						
	6,332	74	>75% Gras	s cover, Go	ood, HSG C				
	22,742	91	Weighted A	Weighted Average					
	6,332		27.84% Per	vious Area	a				
	16,410		72.16% Imp	ervious Ar	rea				
Tc	Length	Slope	e Velocity	Capacity	Description				
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)					
6.0					Direct Entry, Min. Tc				

Subcatchment 1S: CB-1



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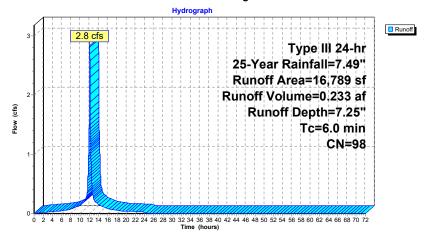
Summary for Subcatchment 2.1S: Building Roof-Southeast

Runoff = 2.8 cfs @ 12.08 hrs, Volume= 0.233 af, Depth= 7.25"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=7.49"

A	rea (sf)	CN	Description						
	16,789	98	Roofs, HSG C						
	16,789		100.00% Impervious Area						
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description				
6.0					Direct Entry Min To				

Subcatchment 2.1S: Building Roof-Southeast



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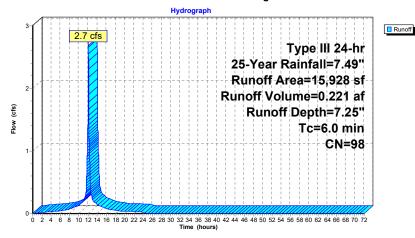
Summary for Subcatchment 2S: Building Roof

Runoff = 2.7 cfs @ 12.08 hrs, Volume= 0.221 af, Depth= 7.25"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=7.49"

Ar	ea (sf)	CN D	escription		
•	15,928	98 F	Roofs, HSG	C	
	15,928	1	00.00% In	pervious A	Area
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Min. Tc

Subcatchment 2S: Building Roof



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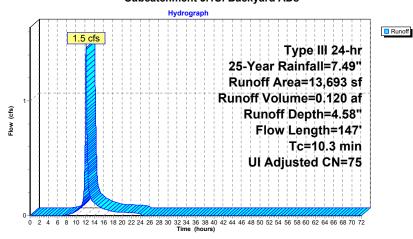
Summary for Subcatchment 3.1S: Backyard ADs

Runoff = 1.5 cfs @ 12.14 hrs, Volume= 0.120 af, Depth= 4.58"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=7.49"

Α	rea (sf)	CN	Adj Desc	Description					
	1,165	98	Unco	onnected pa	avement, HSG C				
	12,528	74	>759	% Grass co	ver, Good, HSG C				
	13,693	76	75 Weig	hted Avera	ige, UI Adjusted				
	12,528		91.4	9% Perviou	is Area				
	1,165		8.51	% Impervio	us Area				
	1,165		100.	00% Uncor	nected				
т.	1	01	\	0	Description				
Tc	Length	Slope		Capacity	Description				
(min)	(feet)	(ft/ft)		(cfs)					
9.4	50	0.0142	0.09		Sheet Flow,				
					Grass: Dense n= 0.240 P2= 3.23"				
0.9	97	0.0154	1.86		Shallow Concentrated Flow,				
					Grassed Waterway Kv= 15.0 fps				
10.3	147	Total							

Subcatchment 3.1S: Backyard ADs



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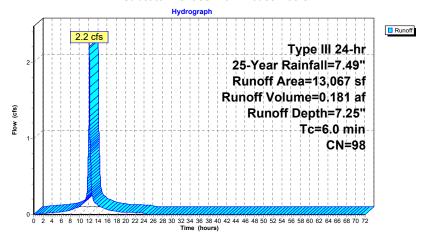
Summary for Subcatchment 3S: Townhouse Roofs

Runoff = 2.2 cfs @ 12.08 hrs, Volume= 0.181 af, Depth= 7.25"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=7.49"

Area	(sf) CN	Description						
13	067 98	Roofs, HSC	Roofs, HSG C					
13	,067	100.00% In	npervious A	Area				
Tc Le		pe Velocity (ft) (ft/sec)	Capacity (cfs)	Description				
6.0				Direct Entry, Min. Tc				

Subcatchment 3S: Townhouse Roofs



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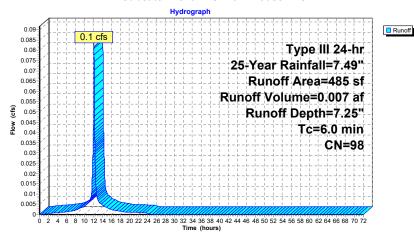
Summary for Subcatchment 4.2S: Townhouse TDs

Runoff = 0.1 cfs @ 12.08 hrs, Volume= 0.007 af, Depth= 7.25"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=7.49"

A	rea (sf)	CN [Description					
	485	98 F	Paved parking, HSG C					
	485	1	100.00% Impervious Area					
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
6.0					Direct Entry, Min. Tc			

Subcatchment 4.2S: Townhouse TDs



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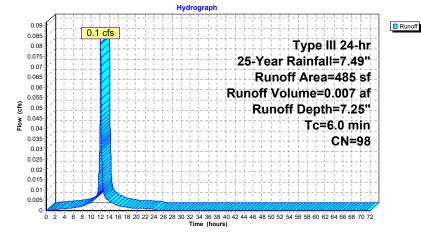
Summary for Subcatchment 4.3S: Townhouse TDs

Runoff = 0.1 cfs @ 12.08 hrs, Volume= 0.007 af, Depth= 7.25"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=7.49"

	Α	rea (sf)	CN [Description							
		485	98 F	Paved parking, HSG C							
Ī		485	•	100.00% Impervious Area							
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description					
	6.0				. ,	Direct Entry Min To					

Subcatchment 4.3S: Townhouse TDs



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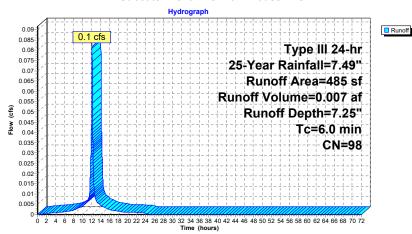
Summary for Subcatchment 4.4S: Townhouse TDs

Runoff = 0.1 cfs @ 12.08 hrs, Volume= 0.007 af, Depth= 7.25"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=7.49"

	rea (sf)	CN D	escription					
	485	98 F	Paved parking, HSG C					
	485	1	100.00% Impervious Area					
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
6.0					Direct Entry, Min. Tc			

Subcatchment 4.4S: Townhouse TDs



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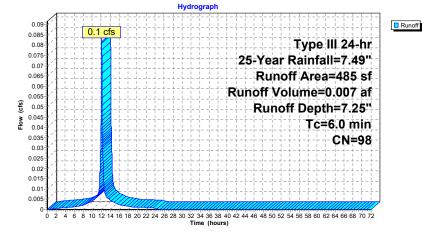
Summary for Subcatchment 4.5S: Townhouse TDs

Runoff = 0.1 cfs @ 12.08 hrs, Volume= 0.007 af, Depth= 7.25"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=7.49"

A	rea (sf)	CN [Description					
	485	98 F	Paved parking, HSG C					
	485	1	100.00% Impervious Area					
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
6.0					Direct Entry, Min. Tc			

Subcatchment 4.5S: Townhouse TDs



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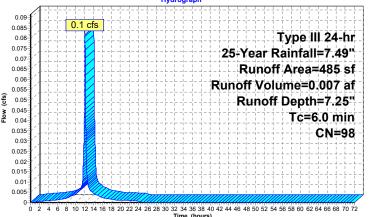
Summary for Subcatchment 4.6S: Townhouse TDs

Runoff = 0.1 cfs @ 12.08 hrs, Volume= 0.007 af, Depth= 7.25"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=7.49"

	rea (sf)	CN D	escription					
	485	98 F	Paved parking, HSG C					
	485	1	100.00% Impervious Area					
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
6.0					Direct Entry, Min. Tc			

Subcatchment 4.6S: Townhouse TDs



Runoff

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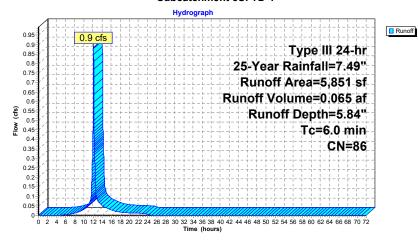
Summary for Subcatchment 5S: TD-1

Runoff = 0.9 cfs @ 12.09 hrs, Volume= 0.065 af, Depth= 5.84"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=7.49"

A	rea (sf)	CN	Description						
	3,021	98	Paved parking, HSG C						
	2,830	74	>75% Grass cover, Good, HSG C						
	5,851	86	Weighted Average						
	2,830		48.37% Pervious Area						
	3,021		51.63% lmp	ervious Ar	rea				
_		٥.			-				
Tc	Length	Slope	,	Capacity	Description				
(min)	(feet)	(ft/ft	(ft/sec)	(cfs)					
6.0					Direct Entry, Min. Tc				

Subcatchment 5S: TD-1



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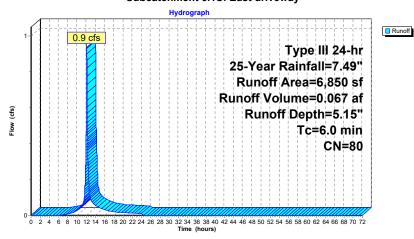
Summary for Subcatchment 6.1S: East driveway

Runoff = 0.9 cfs @ 12.09 hrs, Volume= 0.067 af, Depth= 5.15"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=7.49"

A	rea (sf)	CN	Description							
	5,074	74	>75% Gras	>75% Grass cover, Good, HSG C						
	1,776	98	Paved road	s w/curbs &	& sewers, HSG C					
	6,850	80	Weighted A	Weighted Average						
	5,074		74.07% Per	rvious Area	a					
	1,776		25.93% Imp	pervious Are	rea					
Tc (min)	Length (feet)	Slop (ft/f	,	Capacity (cfs)						
6.0					Direct Entry,					

Subcatchment 6.1S: East driveway



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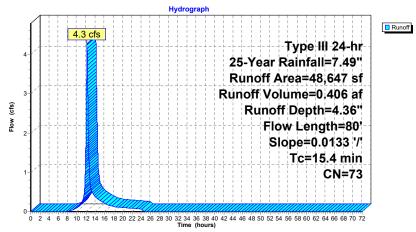
Summary for Subcatchment 6S: Bypass Towards Wetlands

Runoff = 4.3 cfs @ 12.21 hrs, Volume= 0.406 af, Depth= 4.36"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=7.49"

	Α	rea (sf)	CN	Description		
		13,497	70	Woods, Go	od, HSG C	
		35,043	74	>75% Gras	s cover, Go	ood, HSG C
		107	98	Roofs, HSC	S C	
		48,647	73	Weighted A	verage	
		48,540		99.78% Pei	rvious Area	
		107		0.22% Impe	ervious Are	a
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	14.5	50	0.0133	0.06		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 3.23"
	0.9	30	0.0133	0.58		Shallow Concentrated Flow,
_						Woodland Kv= 5.0 fps
	15.4	80	Total			

Subcatchment 6S: Bypass Towards Wetlands



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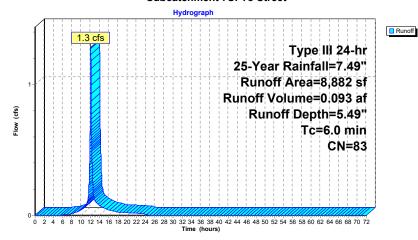
Summary for Subcatchment 7S: To Street

Runoff = 1.3 cfs @ 12.09 hrs, Volume= 0.093 af, Depth= 5.49"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=7.49"

	Area (sf)	CN	Description						
	3,419	98	Paved park	Paved parking, HSG C					
	5,463	74	>75% Gras	>75% Grass cover, Good, HSG C					
	8,882	83	Weighted A	Weighted Average					
	5,463		61.51% Pervious Area						
	3,419		38.49% Impervious Area						
т.	Lananth	Class	- Valasitu	Canasitu	Description				
Tc	J	Slop	,	Capacity	Description				
(min)	(feet)	(ft/f	t) (ft/sec)	(cfs)					
6.0					Direct Entry, Min. Tc				

Subcatchment 7S: To Street



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Summary for Pond 1P: Underground Infiltration System

Inflow Area = 1.636 ac, 69.57% Impervious, Inflow Depth = 6.36" for 25-Year event Inflow = 8.3 cfs @ 12.09 hrs, Volume= 0.867 af

Outflow = 2.4 cfs @ 12.48 hrs, Volume= 0.867 af, Atten= 71%, Lag= 23.5 min

Discarded = 0.1 cfs @ 6.59 hrs, Volume= 0.388 af Primary = 2.3 cfs @ 12.48 hrs, Volume= 0.479 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 8.30' @ 12.48 hrs Surf.Area= 7,556 sf Storage= 14,959 cf

Plug-Flow detention time= 501.4 min calculated for 0.867 af (100% of inflow) Center-of-Mass det. time= 501.5 min (1,312.0 - 810.5)

Volume	Invert	Avail.Storage	Storage Description
#1	6.00'	19,495 cf	6.89'W x 14.06'L x 3.00'H StormTrap ST-1 Units (Irregular Shape)x 78
			22,668 cf Overall x 86.0% Voids

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.00'	0.520 in/hr Exfiltration over Surface area
#2	Primary	7.45'	15.0" Round Culvert
			L= 260.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 7.45' / 6.15' S= 0.0050 '/' Cc= 0.900
			n= 0.013. Flow Area= 1.23 sf

Discarded OutFlow Max=0.1 cfs @ 6.59 hrs HW=6.03' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.1 cfs)

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Thorndike Place - Proposed Conditions

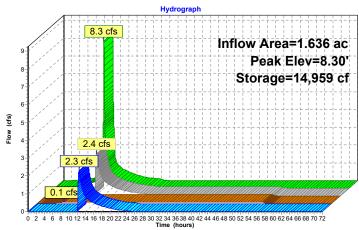
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Pond 1P: Underground Infiltration System





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Summary for Pond 2P: Rooftop Detention

Inflow Area = 0.366 ac,100.00% Impervious, Inflow Depth = 7.25" for 25-Year event

2.7 cfs @ 12.08 hrs, Volume= 0.221 af Inflow

Outflow 0.3 cfs @ 12.67 hrs, Volume= 0.221 af, Atten= 88%, Lag= 35.1 min

Primary = 0.3 cfs @ 12.67 hrs, Volume= 0.221 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 57.56' @ 12.67 hrs Surf.Area= 7,500 sf Storage= 4,196 cf

Plug-Flow detention time= 170.6 min calculated for 0.221 af (100% of inflow)

Center-of-Mass det. time= 170.8 min (912.9 - 742.1)

Volume	Inve	ert Avail.Stor	rage Storage D	escription	
#1	57.0	00' 7,50	00 cf Rooftop D	Detention (Prism	atic)Listed below (Recalc)
Elevation (fee		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
57.0	00	7,500	0	0	
58.0	00	7,500	7,500	7,500	
Device	Routing	Invert	Outlet Devices		
#1	Primary	8.02'	12.0" Round R	Roof Drain	
	•		L= 16.0' CPP,	mitered to confor	m to fill, Ke= 0.700
			Inlet / Outlet Inv	ert= 8.02' / 7.70'	S= 0.0200 '/' Cc= 0.900
			n= 0.013, Flow	Area= 0.79 sf	
#2	Device 1	57.00'	4.0" Horiz. Orif	ice/Grate C= 0.	600
			Limited to weir f	low at low heads	

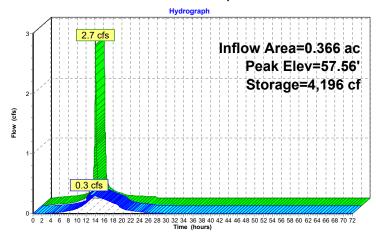
Primary OutFlow Max=0.3 cfs @ 12.67 hrs HW=57.56' (Free Discharge)
1=Roof Drain (Passes 0.3 cfs of 23.4 cfs potential flow)
2=Orifice/Grate (Orifice Controls 0.3 cfs @ 3.60 fps)

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Pond 2P: Rooftop Detention





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Summary for Pond 3P: Rain garden

Inflow Area = 0.157 ac, 25.93% Impervious, Inflow Depth = 5.15" for 25-Year event

Inflow = 0.9 cfs @ 12.09 hrs, Volume= 0.067 af

Outflow = 0.9 cfs @ 12.09 hrs, Volume= 0.067 af, Atten= 0%, Lag= 0.4 min

Discarded = 0.0 cfs @ 10.67 hrs, Volume= 0.010 af Primary = 0.9 cfs @ 12.09 hrs, Volume= 0.057 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 6.37' @ 12.09 hrs Surf.Area= 425 sf Storage= 195 cf

Plug-Flow detention time= 67.5 min calculated for 0.067 af (100% of inflow) Center-of-Mass det. time= 67.6 min (873.0 - 805.4)

Volume	Invert	Avail.St	torage	Storage Description	1		
#1	5.60'		463 cf	Custom Stage Dat	a (Irregular)Listed	below (Recalc)	
Elevation (feet)		rf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
5.60)	2	2.0	0	0	2	
6.00)	346	75.8	50	50	459	
6.30)	425	82.0	115	165	541	
7.00)	425	82.0	298	463	598	
Device	Routing	Inver	t Outle	et Devices			
	Discarded	5.60		0 in/hr Exfiltration o			
#2	Primary	6.30		' long x 5.0' breadtl d (feet) 0.20 0.40 0		Rectangular Weir 20	0

2.50 3.00 3.50 4.00 4.50 5.00 5.50

Coef. (English) 2.34 2.50 2.70 2.68 2.68 2.66 2.65 2.65 2.65 2.65 2.67 2.66 2.68 2.70 2.74 2.79 2.88

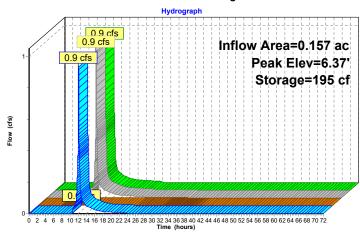
Discarded OutFlow Max=0.0 cfs @ 10.67 hrs HW=6.30' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=0.9 cfs @ 12.09 hrs HW=6.37' (Free Discharge)
—2=Broad-Crested Rectangular Weir (Weir Controls 0.9 cfs @ 0.61 fps)

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Pond 3P: Rain garden





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Thorndike Place - Proposed Conditions

Type III 24-hr 25-Year Rainfall=7.49"

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Summary for Pond TD2:

Inflow Area	a =	0.011 ac,100	0.00% Impervious,	Inflow Depth =	7.25" for	25-Year event
Inflow	=	0.1 cfs @	12.08 hrs, Volume	e= 0.007	af	
Outflow	=	0.0 cfs @	7.85 hrs, Volume	e= 0.007	af, Atten=	98%, Lag= 0.0 min
Discarded	=	0.0 cfs @	7.85 hrs, Volume	e= 0.007	af	
Drimon	_	0 0 ofc	0.00 brs Volume	- 0.000	of	

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 8.49' @ 16.94 hrs Surf.Area= 152 sf Storage= 183 cf Flood Elev= 10.60' Surf.Area= 152 sf Storage= 300 cf

Plug-Flow detention time= 861.4 min calculated for 0.007 af (100% of inflow) Center-of-Mass det. time= 861.5 min (1,603.6 - 742.1)

Volume	Invert	Avail.Storage	Storage Description
#1A	6.50'	91 cf	8.90'W x 17.06'L x 3.67'H Field A
			557 cf Overall - 329 cf Embedded = 228 cf x 40.0% Voids
#2A	7.00'	209 cf	StormTrap ST1 SingleTrap 2-6 Inside #1
			Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf
			Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf
			6.90' x 14.06' Core + 0.00' x 0.50' Border = 6.90' x 15.06' System
		300 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.50'	0.520 in/hr Exfiltration over Surface area
#2	Primary	10.60'	6.0" x 240.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Discarded OutFlow Max=0.0 cfs @ 7.85 hrs HW=6.54' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=6.50' (Free Discharge) 2=Orifice/Grate (Controls 0.0 cfs)

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Thorndike Place - Proposed Conditions
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Pond TD2: - Chamber Wizard Field A

Chamber Model = StormTrap ST1 SingleTrap 2-6 (StormTrap ST1 SingleTrap® Type VI)

Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf

1 Chambers/Row x 14.06' Long = 14.06' Row Length +6.0" Border x 2 +12.0" End Stone x 2 = 17.06' Base Length

1 Rows x 82.7" Wide + 12.0" Side Stone x 2 = 8.90' Base Width 6.0" Base + 38.0" Chamber Height = 3.67' Field Height

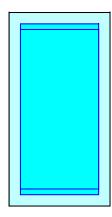
1 Chambers x 208.5 cf = 208.5 cf Chamber Storage

1 Chambers x 307.1 cf + 21.8 cf Border = 328.9 cf Displacement

556.5 cf Field - 328.9 cf Chambers = 227.6 cf Stone x 40.0% Voids = 91.1 cf Stone Storage

Chamber Storage + Stone Storage = 299.6 cf = 0.007 af Overall Storage Efficiency = 53.8% Overall System Size = 17.06' x 8.90' x 3.67'

1 Chambers (plus border) 20.6 cy Field 8.4 cy Stone



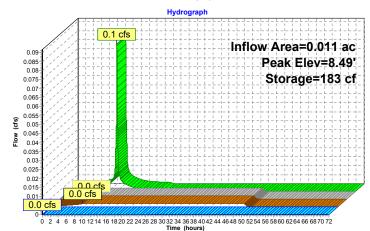


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Pond TD2:





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Summary for Pond TD3:

 Inflow Area = Inflow = O.011 ac,100.00% Impervious, Inflow Depth = 7.25" for 25-Year event

 Inflow = O.1 cfs @ 12.08 hrs, Volume= O.007 af

 Outflow = Discarded = O.0 cfs @ 7.85 hrs, Volume= O.007 af, Atten= 98%, Lag= 0.0 min

 Discarded = Primary = O.0 cfs @ 0.00 frs, Volume= O.007 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 8.49' @ 16.94 hrs Surf.Area= 152 sf Storage= 183 cf Flood Elev= 10.60' Surf.Area= 152 sf Storage= 300 cf

Plug-Flow detention time= 861.4 min calculated for 0.007 af (100% of inflow) Center-of-Mass det. time= 861.5 min (1,603.6 - 742.1)

Volume	Invert	Avail.Storage	Storage Description
#1A	6.50'	91 cf	8.90'W x 17.06'L x 3.67'H Field A
			557 cf Overall - 329 cf Embedded = 228 cf x 40.0% Voids
#2A	7.00'	209 cf	StormTrap ST1 SingleTrap 2-6 Inside #1
			Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf
			Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf
			6.90' x 14.06' Core + 0.00' x 0.50' Border = 6.90' x 15.06' System
		300 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.50'	0.520 in/hr Exfiltration over Surface area
#2	Primary	10.60'	6.0" x 240.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Discarded OutFlow Max=0.0 cfs @ 7.85 hrs HW=6.54' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=6.50' (Free Discharge)
2=Orifice/Grate (Controls 0.0 cfs)

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Pond TD3: - Chamber Wizard Field A

Chamber Model = StormTrap ST1 SingleTrap 2-6 (StormTrap ST1 SingleTrap® Type VI)

Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06"L = 208.5 cf Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06"L = 307.1 cf

1 Chambers/Row x 14.06' Long = 14.06' Row Length +6.0" Border x 2 +12.0" End Stone x 2 = 17.06' Base Length

1 Rows x 82.7" Wide + 12.0" Side Stone x 2 = 8.90' Base Width 6.0" Base + 38.0" Chamber Height = 3.67' Field Height

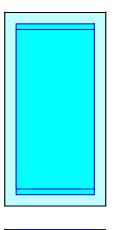
1 Chambers x 208.5 cf = 208.5 cf Chamber Storage

1 Chambers x 307.1 cf + 21.8 cf Border = 328.9 cf Displacement

556.5 cf Field - 328.9 cf Chambers = 227.6 cf Stone x 40.0% Voids = 91.1 cf Stone Storage

Chamber Storage + Stone Storage = 299.6 cf = 0.007 af Overall Storage Efficiency = 53.8% Overall System Size = 17.06' x 8.90' x 3.67'

1 Chambers (plus border) 20.6 cy Field 8.4 cy Stone



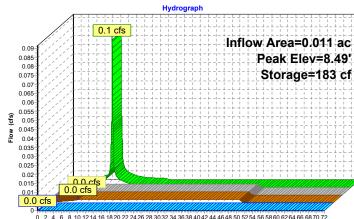
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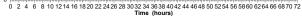
Thorndike Place - Proposed Conditions Type III 24-hr 25-Year Rainfall=7.49" Printed 6/4/2021 ions LLC Page 112

Inflow
Outflow
Discarded

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Pond TD3:





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Type III 24-hr 25-Year Rainfall=7.49"

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Summary for Pond TD4:

Inflow Area	a =	0.011 ac,100	0.00% Impervious,	Inflow Depth =	7.25" for	25-Year event
Inflow	=	0.1 cfs @	12.08 hrs, Volume	e= 0.007	af	
Outflow	=	0.0 cfs @	7.85 hrs, Volume	e= 0.007	af, Atten=	98%, Lag= 0.0 min
Discarded	=	0.0 cfs @	7.85 hrs, Volume	e= 0.007	af	
Drimon	_	0 0 ofc	0.00 brs Volume	- 0.000	of	

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 8.49' @ 16.94 hrs Surf.Area= 152 sf Storage= 183 cf Flood Elev= 10.60' Surf.Area= 152 sf Storage= 300 cf

Plug-Flow detention time= 861.4 min calculated for 0.007 af (100% of inflow) Center-of-Mass det. time= 861.5 min (1,603.6 - 742.1)

Volume	Invert	Avail.Storage	Storage Description
#1A	6.50'	91 cf	8.90'W x 17.06'L x 3.67'H Field A
			557 cf Overall - 329 cf Embedded = 228 cf x 40.0% Voids
#2A	7.00'	209 cf	StormTrap ST1 SingleTrap 2-6 Inside #1
			Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf
			Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf
			6.90' x 14.06' Core + 0.00' x 0.50' Border = 6.90' x 15.06' System
		300 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.50'	0.520 in/hr Exfiltration over Surface area
#2	Primary	10.60'	6.0" x 240.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Discarded OutFlow Max=0.0 cfs @ 7.85 hrs HW=6.54' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=6.50' (Free Discharge) 2=Orifice/Grate (Controls 0.0 cfs)

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Thorndike Place - Proposed Conditions
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Pond TD4: - Chamber Wizard Field A

Chamber Model = StormTrap ST1 SingleTrap 2-6 (StormTrap ST1 SingleTrap® Type VI)

Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf

1 Chambers/Row x 14.06' Long = 14.06' Row Length +6.0" Border x 2 + 12.0" End Stone x 2 = 17.06' Base Length

1 Rows x 82.7" Wide + 12.0" Side Stone x 2 = 8.90' Base Width 6.0" Base + 38.0" Chamber Height = 3.67' Field Height

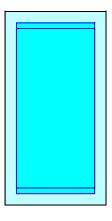
1 Chambers x 208.5 cf = 208.5 cf Chamber Storage

1 Chambers x 307.1 cf + 21.8 cf Border = 328.9 cf Displacement

556.5 cf Field - 328.9 cf Chambers = 227.6 cf Stone x 40.0% Voids = 91.1 cf Stone Storage

Chamber Storage + Stone Storage = 299.6 cf = 0.007 af Overall Storage Efficiency = 53.8% Overall System Size = 17.06' x 8.90' x 3.67'

1 Chambers (plus border) 20.6 cy Field 8.4 cy Stone



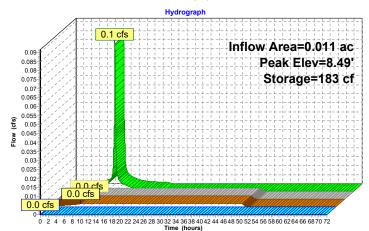


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Pond TD4:





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Summary for Pond TD5:

 Inflow Area = Inflow = O.011 ac,100.00% Impervious, Inflow Depth = 7.25" for 25-Year event

 Inflow = O.1 cfs @ 12.08 hrs, Volume= O.007 af

 Outflow = Discarded = O.0 cfs @ 7.85 hrs, Volume= O.007 af, Atten= 98%, Lag= 0.0 min

 Discarded = Primary = O.0 cfs @ 0.00 frs, Volume= O.007 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 8.49' @ 16.94 hrs Surf.Area= 152 sf Storage= 183 cf Flood Elev= 10.60' Surf.Area= 152 sf Storage= 300 cf

Plug-Flow detention time= 861.4 min calculated for 0.007 af (100% of inflow) Center-of-Mass det. time= 861.5 min (1,603.6 - 742.1)

Volume	Invert	Avail.Storage	Storage Description
#1A	6.50'	91 cf	8.90'W x 17.06'L x 3.67'H Field A
			557 cf Overall - 329 cf Embedded = 228 cf x 40.0% Voids
#2A	7.00'	209 cf	StormTrap ST1 SingleTrap 2-6 Inside #1
			Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf
			Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf
			6.90' x 14.06' Core + 0.00' x 0.50' Border = 6.90' x 15.06' System
		300 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.50'	0.520 in/hr Exfiltration over Surface area
#2	Primary	10.60'	6.0" x 240.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Discarded OutFlow Max=0.0 cfs @ 7.85 hrs HW=6.54' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=6.50' (Free Discharge)
2=Orifice/Grate (Controls 0.0 cfs)

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Pond TD5: - Chamber Wizard Field A

Chamber Model = StormTrap ST1 SingleTrap 2-6 (StormTrap ST1 SingleTrap® Type VI)

Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf

1 Chambers/Row x 14.06' Long = 14.06' Row Length +6.0" Border x 2 +12.0" End Stone x 2 = 17.06' Base Length

1 Rows x 82.7" Wide + 12.0" Side Stone x 2 = 8.90' Base Width 6.0" Base + 38.0" Chamber Height = 3.67' Field Height

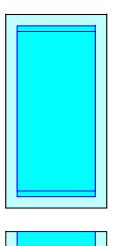
1 Chambers x 208.5 cf = 208.5 cf Chamber Storage

1 Chambers x 307.1 cf + 21.8 cf Border = 328.9 cf Displacement

556.5 cf Field - 328.9 cf Chambers = 227.6 cf Stone x 40.0% Voids = 91.1 cf Stone Storage

Chamber Storage + Stone Storage = 299.6 cf = 0.007 af Overall Storage Efficiency = 53.8% Overall System Size = 17.06' x 8.90' x 3.67'

1 Chambers (plus border) 20.6 cv Field 8.4 cy Stone

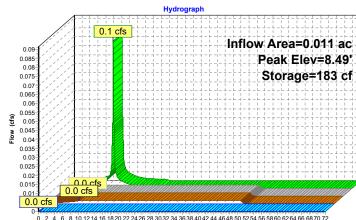


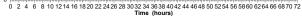
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Pond TD5:







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Type III 24-hr 25-Year Rainfall=7.49"

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Summary for Pond TD6:

Inflow Area	a =	0.011 ac,100	0.00% Impervious,	Inflow Depth =	7.25" for	25-Year event
Inflow	=	0.1 cfs @	12.08 hrs, Volume	e= 0.007	af	
Outflow	=	0.0 cfs @	7.85 hrs, Volume	e= 0.007	af, Atten=	98%, Lag= 0.0 min
Discarded	=	0.0 cfs @	7.85 hrs, Volume	e= 0.007	af	
Drimon	_	0 0 ofc	0.00 brs Volume	- 0.000	of	

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 8.49' @ 16.94 hrs Surf.Area= 152 sf Storage= 183 cf Flood Elev= 10.60' Surf.Area= 152 sf Storage= 300 cf

Plug-Flow detention time= 861.4 min calculated for 0.007 af (100% of inflow) Center-of-Mass det. time= 861.5 min (1,603.6 - 742.1)

Volume	Invert	Avail.Storage	Storage Description
#1A	6.50'	91 cf	8.90'W x 17.06'L x 3.67'H Field A
			557 cf Overall - 329 cf Embedded = 228 cf x 40.0% Voids
#2A	7.00'	209 cf	StormTrap ST1 SingleTrap 2-6 Inside #1
			Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf
			Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf
			6.90' x 14.06' Core + 0.00' x 0.50' Border = 6.90' x 15.06' System
		300 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.50'	0.520 in/hr Exfiltration over Surface area
#2	Primary	10.60'	6.0" x 240.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Discarded OutFlow Max=0.0 cfs @ 7.85 hrs HW=6.54' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=6.50' (Free Discharge) 2=Orifice/Grate (Controls 0.0 cfs)

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Thorndike Place - Proposed Conditions
Type III 24-hr 25-Year Rainfall=7.49"
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Pond TD6: - Chamber Wizard Field A

Chamber Model = StormTrap ST1 SingleTrap 2-6 (StormTrap ST1 SingleTrap® Type VI)

Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf

1 Chambers/Row x 14.06' Long = 14.06' Row Length +6.0'' Border x 2 + 12.0'' End Stone x 2 = 17.06' Base Length

1 Rows x 82.7" Wide + 12.0" Side Stone x 2 = 8.90' Base Width 6.0" Base + 38.0" Chamber Height = 3.67' Field Height

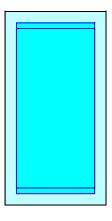
1 Chambers x 208.5 cf = 208.5 cf Chamber Storage

1 Chambers x 307.1 cf + 21.8 cf Border = 328.9 cf Displacement

556.5 cf Field - 328.9 cf Chambers = 227.6 cf Stone x 40.0% Voids = 91.1 cf Stone Storage

Chamber Storage + Stone Storage = 299.6 cf = 0.007 af Overall Storage Efficiency = 53.8% Overall System Size = 17.06' x 8.90' x 3.67'

1 Chambers (plus border) 20.6 cy Field 8.4 cy Stone



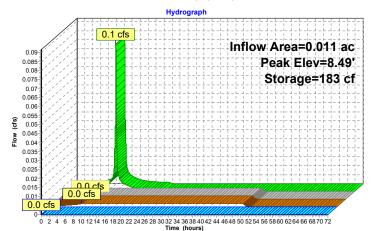


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Pond TD6:



Inflow
Outflow
Discarded
Primary

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Summary for Link 1L: Towards Wetlands

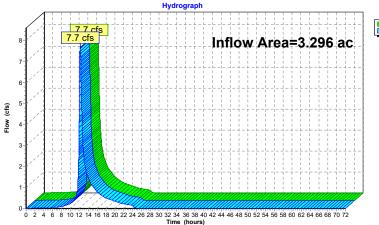
3.296 ac, 47.55% Impervious, Inflow Depth = 4.28" for 25-Year event 7.7 cfs @ 12.20 hrs, Volume= 1.175 af Inflow Area =

Inflow

1.175 af, Atten= 0%, Lag= 0.0 min Primary = 7.7 cfs @ 12.20 hrs, Volume=

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Link 1L: Towards Wetlands



Inflow Primary

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Summary for Link 2L: Towards Street

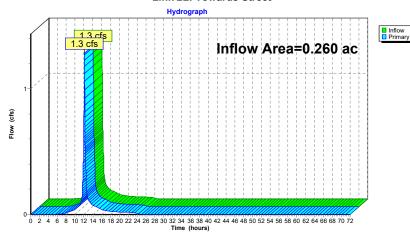
Inflow Area = 0.260 ac, 51.68% Impervious, Inflow Depth = 4.31" for 25-Year event

Inflow = 1.3 cfs @ 12.09 hrs, Volume= 0.093 af

Primary = 1.3 cfs @ 12.09 hrs, Volume= 0.093 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Link 2L: Towards Street



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Thorndike Place - Proposed Conditions

Type III 24-hr 25-Year Rainfall=7.49"

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Summary for Link 100L: Total Flows

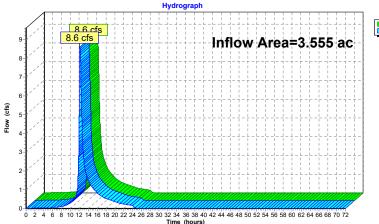
Inflow Area = 3.555 ac, 47.85% Impervious, Inflow Depth = 4.28" for 25-Year event

Inflow = 8.6 cfs @ 12.14 hrs, Volume= 1.268 af

Primary = 8.6 cfs @ 12.14 hrs, Volume= 1.268 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Link 100L: Total Flows



Inflow Primary

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Thorndike Place - Proposed Conditions Type III 24-hr 50-Year Rainfall=8.72"

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Time span=0.00-72.00 hrs, dt=0.01 hrs, 7201 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1S: CB-1 Runoff Area=22.742 sf 72.16% Impervious Runoff Depth=7.64" Tc=6.0 min CN=91 Runoff=4.3 cfs 0.332 af

Subcatchment 2.1S: Building Runoff Area=16,789 sf 100,00% Impervious Runoff Depth=8,48" Tc=6.0 min CN=98 Runoff=3.3 cfs 0.272 af

Subcatchment 2S: Building Roof Runoff Area=15.928 sf 100.00% Impervious Runoff Depth=8.48"

Tc=6.0 min CN=98 Runoff=3.1 cfs 0.258 af

Subcatchment 3.1S: Backyard ADs Runoff Area=13,693 sf 8.51% Impervious Runoff Depth=5.70"

Flow Length=147' Tc=10.3 min UI Adjusted CN=75 Runoff=1.8 cfs 0.149 af

Subcatchment 3S: Townhouse Roofs Runoff Area=13,067 sf 100.00% Impervious Runoff Depth=8.48" Tc=6.0 min CN=98 Runoff=2.6 cfs 0.212 af

Subcatchment 4.2S: Townhouse TDs Runoff Area=485 sf 100.00% Impervious Runoff Depth=8.48" Tc=6.0 min CN=98 Runoff=0.1 cfs 0.008 af

Subcatchment 4.3S: Townhouse TDs Runoff Area=485 sf 100.00% Impervious Runoff Depth=8.48" Tc=6.0 min CN=98 Runoff=0.1 cfs 0.008 af

Runoff Area=485 sf 100.00% Impervious Runoff Depth=8.48" Subcatchment 4.4S: Townhouse TDs

Tc=6.0 min CN=98 Runoff=0.1 cfs 0.008 af

Subcatchment 4.5S: Townhouse TDs Runoff Area=485 sf 100.00% Impervious Runoff Depth=8.48" Tc=6.0 min CN=98 Runoff=0.1 cfs 0.008 af

Subcatchment 4.6S: Townhouse TDs Runoff Area=485 sf 100.00% Impervious Runoff Depth=8.48" Tc=6.0 min CN=98 Runoff=0.1 cfs 0.008 af

Subcatchment 5S: TD-1 Runoff Area=5,851 sf 51.63% Impervious Runoff Depth=7.03"

Tc=6.0 min CN=86 Runoff=1.1 cfs 0.079 af

Runoff Area=6.850 sf 25.93% Impervious Runoff Depth=6.30" Subcatchment 6.1S: East driveway Tc=6.0 min CN=80 Runoff=1.1 cfs 0.083 af

Runoff Area=48.647 sf 0.22% Impervious Runoff Depth=5.45" Subcatchment 6S: Bypass Towards Slope=0.0133 '/' Tc=15.4 min CN=73 Runoff=5.3 cfs 0.507 af Flow Length=80'

Runoff Area=8.882 sf 38.49% Impervious Runoff Depth=6.67" Subcatchment 7S: To Street Tc=6.0 min CN=83 Runoff=1.5 cfs 0.113 af

Peak Elev=8.57' Storage=16.701 cf Inflow=9.8 cfs 1.030 af

Pond 1P: Underground Infiltration System Discarded=0.1 cfs 0.395 af Primary=3.5 cfs 0.635 af Outflow=3.6 cfs 1.030 af

Pond 2P: Rooftop Detention Peak Elev=57.66' Storage=4.963 cf Inflow=3.1 cfs 0.258 af Outflow=0.3 cfs 0.258 af 2340700-PR-2021-06-03

Thorndike Place - Proposed Conditions Type III 24-hr 50-Year Rainfall=8.72"

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Pond 3P: Rain garden Peak Elev=6.38' Storage=199 cf Inflow=1.1 cfs 0.083 af Discarded=0.0 cfs 0.011 af Primary=1.1 cfs 0.072 af Outflow=1.1 cfs 0.083 af

Pond TD2: Peak Elev=8.89' Storage=224 cf Inflow=0.1 cfs 0.008 af

Discarded=0.0 cfs 0.008 af Primary=0.0 cfs 0.000 af Outflow=0.0 cfs 0.008 af

Pond TD3: Peak Elev=8.89' Storage=224 cf Inflow=0.1 cfs 0.008 af

Discarded=0.0 cfs 0.008 af Primary=0.0 cfs 0.000 af Outflow=0.0 cfs 0.008 af

Pond TD4: Peak Elev=8.89' Storage=224 cf Inflow=0.1 cfs 0.008 af Discarded=0.0 cfs 0.008 af Primary=0.0 cfs 0.000 af Outflow=0.0 cfs 0.008 af

Peak Elev=8.89' Storage=224 cf Inflow=0.1 cfs 0.008 af

Pond TD5: Discarded=0.0 cfs 0.008 af Primary=0.0 cfs 0.000 af Outflow=0.0 cfs 0.008 af

Pond TD6: Peak Elev=8.89' Storage=224 cf Inflow=0.1 cfs 0.008 af Discarded=0.0 cfs 0.008 af Primary=0.0 cfs 0.000 af Outflow=0.0 cfs 0.008 af

Inflow=10.7 cfs 1.487 af Link 1L: Towards Wetlands Primary=10.7 cfs 1.487 af

Link 2L: Towards Street Inflow=1.5 cfs 0.113 af

Primary=1.5 cfs 0.113 af

Link 100L: Total Flows Inflow=11.8 cfs 1.600 af

Primary=11.8 cfs 1.600 af

Total Runoff Area = 3.555 ac Runoff Volume = 2.046 af Average Runoff Depth = 6.90" 52.15% Pervious = 1.854 ac 47.85% Impervious = 1.701 ac

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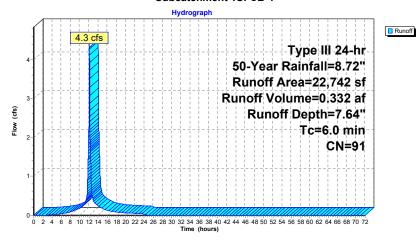
Summary for Subcatchment 1S: CB-1

Runoff = 4.3 cfs @ 12.08 hrs, Volume= 0.332 af, Depth= 7.64"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 50-Year Rainfall=8.72"

Α	rea (sf)	CN	Description			
	16,410					
	6,332					
	22,742	91	Weighted A	verage		
	6,332		27.84% Per	vious Area		
	16,410 72.16% Impervious Are				ea	
Тс	Length	Slope	,	Capacity	Description	
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)		
6.0					Direct Entry, Min. Tc	

Subcatchment 1S: CB-1



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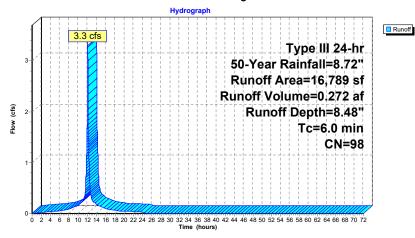
Summary for Subcatchment 2.1S: Building Roof-Southeast

Runoff = 3.3 cfs @ 12.08 hrs, Volume= 0.272 af, Depth= 8.48"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 50-Year Rainfall=8.72"

A	rea (sf)					
	16,789	98	Roofs, HSG	G C		
	16,789		100.00% In	pervious A	rea	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
6.0					Direct Entry Min To	

Subcatchment 2.1S: Building Roof-Southeast



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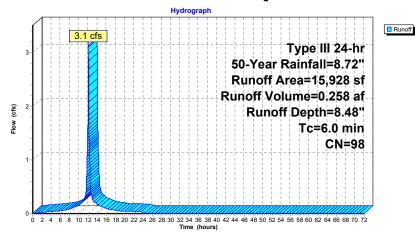
Summary for Subcatchment 2S: Building Roof

Runoff = 3.1 cfs @ 12.08 hrs, Volume= 0.258 af, Depth= 8.48"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 50-Year Rainfall=8.72"

A	rea (sf)	CN I	Description		
	15,928	98 I	Roofs, HSC	C C	
	15,928	•	100.00% Im	npervious A	Area
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Min. Tc

Subcatchment 2S: Building Roof



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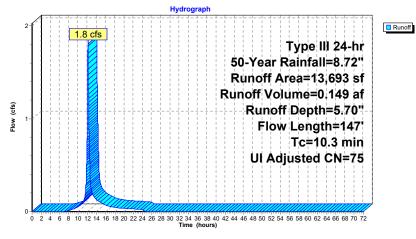
Summary for Subcatchment 3.1S: Backyard ADs

Runoff = 1.8 cfs @ 12.14 hrs, Volume= 0.149 af, Depth= 5.70"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 50-Year Rainfall=8.72"

	Α	rea (sf)	CN	Adj Desc	cription			
		1,165	98	Unco	onnected pa	avement, HSG C		
		12,528	74	>75%	% Grass co	ver, Good, HSG C		
		13,693	76	75 Weig	hted Avera	ige, UI Adjusted		
	12,528				91.49% Pervious Area			
		1,165		8.51	% Impervio	us Area		
		1,165		100.	00% Uncor	nected		
	т.	1	01	\	0	Description		
	Tc	Length	Slope		Capacity	Description		
-	(min)	(feet)	(ft/ft)		(cfs)		_	
	9.4	50	0.0142	0.09		Sheet Flow,		
						Grass: Dense n= 0.240 P2= 3.23"		
	0.9	97	0.0154	1.86		Shallow Concentrated Flow,		
_						Grassed Waterway Kv= 15.0 fps		
	10.3	147	Total					

Subcatchment 3.1S: Backyard ADs



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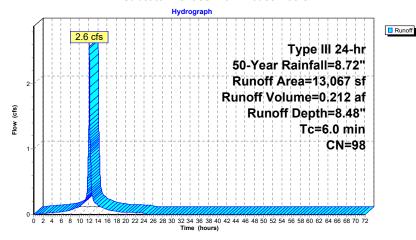
Summary for Subcatchment 3S: Townhouse Roofs

Runoff = 2.6 cfs @ 12.08 hrs, Volume= 0.212 af, Depth= 8.48"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 50-Year Rainfall=8.72"

A	rea (sf)	CN [Description					
	13,067	98 F	98 Roofs, HSG C					
	13,067	100.00% Impervious A			ırea			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
6.0	•				Direct Entry, Min. Tc			

Subcatchment 3S: Townhouse Roofs



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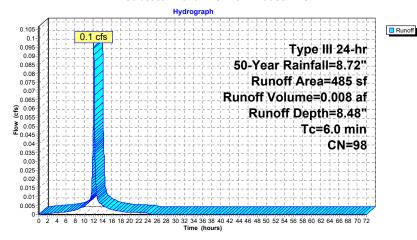
Summary for Subcatchment 4.2S: Townhouse TDs

Runoff = 0.1 cfs @ 12.08 hrs, Volume= 0.008 af, Depth= 8.48"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 50-Year Rainfall=8.72"

Α	rea (sf)	CN [Description						
	485	98 F	Paved parking, HSG C						
	485	1	00.00% In	pervious A	rea				
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
6.0					Direct Entry Min To				

Subcatchment 4.2S: Townhouse TDs



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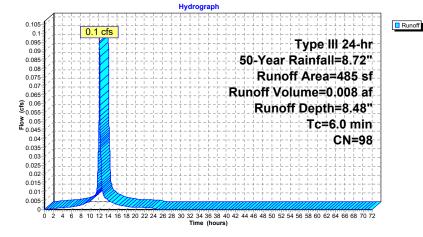
Summary for Subcatchment 4.3S: Townhouse TDs

Runoff = 0.1 cfs @ 12.08 hrs, Volume= 0.008 af, Depth= 8.48"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 50-Year Rainfall=8.72"

A	rea (sf)	CN [Description					
	485	98 F	Paved parking, HSG C					
	485	1	00.00% In	npervious A	Area			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
6.0					Direct Entry, Min. Tc			

Subcatchment 4.3S: Townhouse TDs



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Thorndike Place - Proposed Conditions
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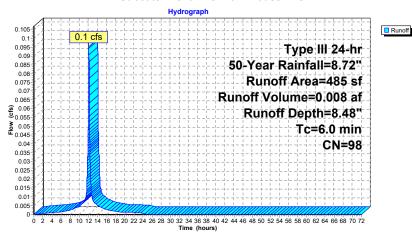
Summary for Subcatchment 4.4S: Townhouse TDs

Runoff = 0.1 cfs @ 12.08 hrs, Volume= 0.008 af, Depth= 8.48"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 50-Year Rainfall=8.72"

Α	rea (sf)	CN I	Description					
	485	98 I	Paved parking, HSG C					
	485		100.00% In	pervious A	rea			
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description			
6.0					Direct Entry Min To			

Subcatchment 4.4S: Townhouse TDs



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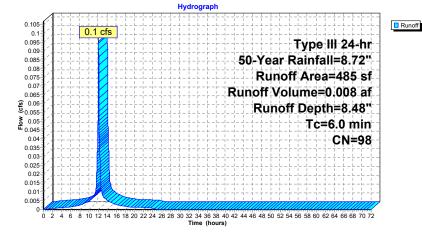
Summary for Subcatchment 4.5S: Townhouse TDs

Runoff = 0.1 cfs @ 12.08 hrs, Volume= 0.008 af, Depth= 8.48"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 50-Year Rainfall=8.72"

A	rea (sf)	CN [Description					
	485	98 F	Paved parking, HSG C					
	485	1	00.00% In	npervious A	Area			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
6.0					Direct Entry, Min. Tc			

Subcatchment 4.5S: Townhouse TDs



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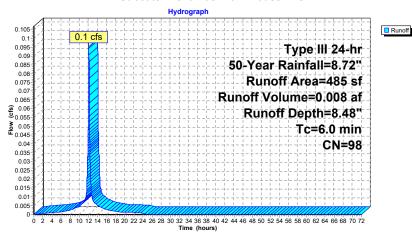
Summary for Subcatchment 4.6S: Townhouse TDs

Runoff = 0.1 cfs @ 12.08 hrs, Volume= 0.008 af, Depth= 8.48"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 50-Year Rainfall=8.72"

Α	rea (sf)	CN I	Description						
	485	98 I	Paved parking, HSG C						
	485		100.00% In	npervious A	rea				
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
6.0					Direct Entry Min To				

Subcatchment 4.6S: Townhouse TDs



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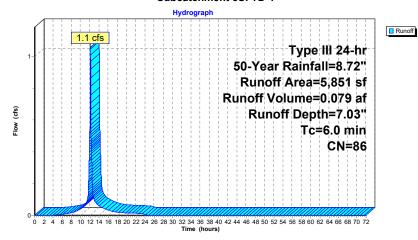
Summary for Subcatchment 5S: TD-1

Runoff = 1.1 cfs @ 12.08 hrs, Volume= 0.079 af, Depth= 7.03"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 50-Year Rainfall=8.72"

A	rea (sf)	CN	Description			
	3,021	98	Paved park	ing, HSG C		
	2,830	74	>75% Ġras	s cover, Go	ood, HSG C	
,	5,851	86	Neighted A	verage		
	2,830		48.37% Pervious Area			
	3,021		51.63% lmp	ervious Ar	rea	
Tc	Length	Slope	,	Capacity	Description	
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
6.0					Direct Entry, Min. Tc	

Subcatchment 5S: TD-1



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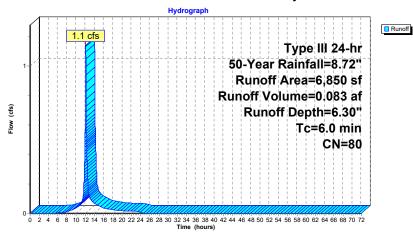
Summary for Subcatchment 6.1S: East driveway

Runoff = 1.1 cfs @ 12.09 hrs, Volume= 0.083 af, Depth= 6.30"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 50-Year Rainfall=8.72"

A	rea (sf)	CN	Description	Description						
	5,074	74	>75% Grass	>75% Grass cover, Good, HSG C						
	1,776	98	Paved road	s w/curbs &	& sewers, HSG C					
	6,850	80	Weighted Average							
	5,074		74.07% Pervious Area							
	1,776		25.93% Impervious Area							
Tc (min)	Length (feet)	Slop (ft/f	,	Capacity (cfs)						
6.0					Direct Entry,					

Subcatchment 6.1S: East driveway



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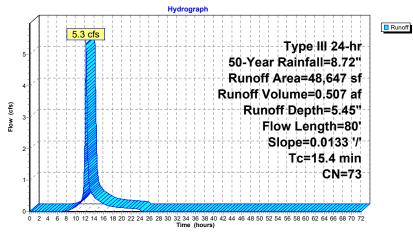
Summary for Subcatchment 6S: Bypass Towards Wetlands

Runoff = 5.3 cfs @ 12.20 hrs, Volume= 0.507 af, Depth= 5.45"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 50-Year Rainfall=8.72"

	Δ	rea (sf)	CN	Description		
-		13.497	_	Woods, Go		
		35.043				ood, HSG C
		107		Roofs, HSC	, -	, , , , , , , , , , , , , , , , , , , ,
-		48.647	73	Weighted A	verage	
		48,540		99.78% Per		
		107		0.22% Impe	ervious Are	a
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	14.5	50	0.0133	0.06		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 3.23"
	0.9	30	0.0133	0.58		Shallow Concentrated Flow,
_						Woodland Kv= 5.0 fps
	15 4	80	Total			

Subcatchment 6S: Bypass Towards Wetlands



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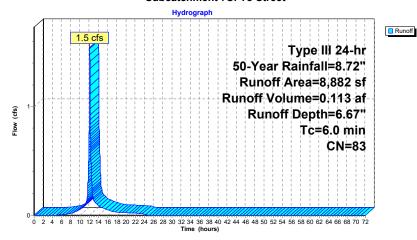
Summary for Subcatchment 7S: To Street

Runoff = 1.5 cfs @ 12.09 hrs, Volume= 0.113 af, Depth= 6.67"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 50-Year Rainfall=8.72"

	Area (sf)	CN	Description						
	3,419	98	Paved parking, HSG C						
	5,463	74	>75% Grass cover, Good, HSG C						
	8,882	83	Weighted A	verage					
	5,463		61.51% Pervious Area						
	3,419		38.49% Imp	pervious Are	rea				
Tc (min)	Length (feet)	Slop (ft/f	,	Capacity (cfs)	Description				
6.0					Direct Entry, Min. Tc				

Subcatchment 7S: To Street



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Summary for Pond 1P: Underground Infiltration System

 Inflow Area =
 1.636 ac, 69.57% Impervious, Inflow Depth = 7.56" for 50-Year event

 Inflow =
 9.8 cfs @ 12.09 hrs, Volume=
 1.030 af

 Outflow =
 3.6 cfs @ 12.40 hrs, Volume=
 1.030 af, Atten= 63%, Lag= 18.3 min

Discarded = 0.1 cfs @ 5.76 hrs, Volume= 0.395 af Primary = 3.5 cfs @ 12.40 hrs, Volume= 0.635 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 8.57' @ 12.40 hrs Surf.Area= 7,556 sf Storage= 16,701 cf

Plug-Flow detention time= 437.5 min calculated for 1.030 af (100% of inflow) Center-of-Mass det. time= 437.5 min (1,246.6 - 809.1)

Volume	Invert	Avail.Storage	Storage Description
#1	6.00'	19,495 cf	6.89'W x 14.06'L x 3.00'H StormTrap ST-1 Units (Irregular Shape)x 78
			22,668 cf Overall x 86.0% Voids

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.00'	0.520 in/hr Exfiltration over Surface area
#2	Primary	7.45'	15.0" Round Culvert
			L= 260.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 7.45' / 6.15' S= 0.0050 '/' Cc= 0.900
			n= 0.013, Flow Area= 1.23 sf

Discarded OutFlow Max=0.1 cfs @ 5.76 hrs HW=6.03' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.1 cfs)

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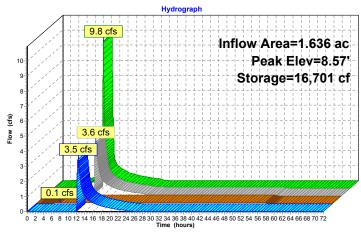
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Pond 1P: Underground Infiltration System





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Summary for Pond 2P: Rooftop Detention

Inflow Area = 0.366 ac,100.00% Impervious, Inflow Depth = 8.48" for 50-Year event

3.1 cfs @ 12.08 hrs, Volume= 0.258 af Inflow

Outflow 0.3 cfs @ 12.73 hrs, Volume= 0.258 af, Atten= 89%, Lag= 39.0 min

Primary = 0.3 cfs @ 12.73 hrs, Volume= 0.258 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 57.66' @ 12.73 hrs Surf.Area= 7,500 sf Storage= 4,963 cf

Plug-Flow detention time= 179.5 min calculated for 0.258 af (100% of inflow)

Center-of-Mass det. time= 179.8 min (919.9 - 740.2)

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Volume	Inve	ert Avail.Stora	ige Storage D	escription	
#1	57.0	7,500	of Rooftop D	Detention (Prism	atic)Listed below (Recalc)
Elevation (fee		Surf.Area (sq-ft) (Inc.Store cubic-feet)	Cum.Store (cubic-feet)	
57.0	00	7,500	0	0	
58.0	00	7,500	7,500	7,500	
Device	Routing	Invert	Outlet Devices		
#1	Primary	8.02'	12.0" Round F	Roof Drain	
		1	L= 16.0' CPP,	mitered to confor	m to fill, Ke= 0.700
			Inlet / Outlet Inv	ert= 8.02' / 7.70'	S= 0.0200 '/' Cc= 0.900
		1	n= 0.013, Flow	Area= 0.79 sf	
#2	Device 1	57.00'	4.0" Horiz. Orif	ice/Grate C= 0.	600
		ĺ	Limited to weir f	low at low heads	

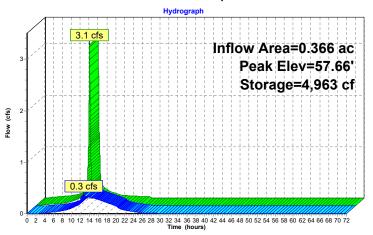
Primary OutFlow Max=0.3 cfs @ 12.73 hrs HW=57.66' (Free Discharge)
1=Roof Drain (Passes 0.3 cfs of 23.4 cfs potential flow)
2=Orifice/Grate (Orifice Controls 0.3 cfs @ 3.92 fps)

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Pond 2P: Rooftop Detention





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Summary for Pond 3P: Rain garden

Inflow Area = 0.157 ac, 25.93% Impervious, Inflow Depth = 6.30" for 50-Year event

Inflow = 1.1 cfs @ 12.09 hrs, Volume= 0.083 af

Outflow = 1.1 cfs @ 12.09 hrs, Volume= 0.083 af, Atten= 0%, Lag= 0.3 min

Discarded = 0.0 cfs @ 10.13 hrs, Volume= 0.011 af Primary = 1.1 cfs @ 12.09 hrs, Volume= 0.072 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 6.38' @ 12.09 hrs Surf.Area= 425 sf Storage= 199 cf

Plug-Flow detention time= 57.0 min calculated for 0.083 af (100% of inflow)

Center-of-Mass det. time= 57.0 min (856.7 - 799.7)

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Volume	Invert	Avail.S	Storage	Storage Descriptio	n	
#1	5.60'		463 cf	Custom Stage Da	ta (Irregular)Liste	d below (Recalc)
Elevation (fee		urf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
5.6	60	2	2.0	0	0	2
6.0	00	346	75.8	50	50	459
6.3	30	425	82.0	115	165	541
7.0	00	425	82.0	298	463	598
Device	Routing	Inve	rt Outle	et Devices		
#1	Discarded	5.6	0' 0.520	in/hr Exfiltration	over Surface are	a
#2	Primary	6.3	0' 22.0'	long x 5.0' breadt	th Broad-Crested	Rectangular Weir
	•		Head	d (feet) 0.20 0.40 (0.60 0.80 1.00 1	.20 1.40 1.60 1.80 2.00
			2.50	3.00 3.50 4.00 4	.50 5.00 5.50	
			Coef	. (English) 2.34 2.5	50 2.70 2.68 2.6	8 2.66 2.65 2.65 2.65
			2.65	2.67 2.66 2.68 2.	.70 2.74 2.79 2.8	38

Discarded OutFlow Max=0.0 cfs @ 10.13 hrs HW=6.30' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=1.1 cfs @ 12.09 hrs HW=6.38' (Free Discharge) —2=Broad-Crested Rectangular Weir (Weir Controls 1.1 cfs @ 0.65 fps)

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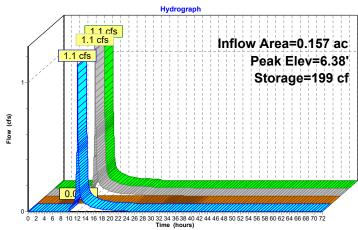
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Type III 24-hr 50-Year Rainfall=8.72"
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Inflow
Outflow
Discarded

Pond 3P: Rain garden



Thorndike Place - Proposed Conditions

Type III 24-hr 50-Year Rainfall=8.72"

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Summary for Pond TD2:

Inflow Area	a =	0.011 ac,100	0.00% Impervious	, Inflow Depth =	8.48" for	50-Year event
Inflow	=	0.1 cfs @	12.08 hrs, Volun	ne= 0.008	3 af	
Outflow	=	0.0 cfs @	7.19 hrs, Volun	ne= 0.008	3 af, Atten=	98%, Lag= 0.0 min
Discarded	=	0.0 cfs @	7.19 hrs, Volun	ne= 0.008	3 af	
Drimory	_	വ വ ക്കേക്	0.00 bre Volum	0.000) of	

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 8.89' @ 17.56 hrs Surf.Area= 152 sf Storage= 224 cf Flood Elev= 10.60' Surf.Area= 152 sf Storage= 300 cf

Plug-Flow detention time= 1,051.4 min calculated for 0.008 af (100% of inflow) Center-of-Mass det. time= 1,051.5 min (1,791.7 - 740.2)

Volume	Invert	Avail.Storage	Storage Description
#1A	6.50'	91 cf	8.90'W x 17.06'L x 3.67'H Field A
			557 cf Overall - 329 cf Embedded = 228 cf x 40.0% Voids
#2A	7.00'	209 cf	StormTrap ST1 SingleTrap 2-6 Inside #1
			Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf
			Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf
			6.90' x 14.06' Core + 0.00' x 0.50' Border = 6.90' x 15.06' System
		300 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.50'	0.520 in/hr Exfiltration over Surface area
#2	Primary	10.60'	6.0" x 240.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Discarded OutFlow Max=0.0 cfs @ 7.19 hrs HW=6.54' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=6.50' (Free Discharge) 2=Orifice/Grate (Controls 0.0 cfs)

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Pond TD2: - Chamber Wizard Field A

Chamber Model = StormTrap ST1 SingleTrap 2-6 (StormTrap ST1 SingleTrap® Type VI)

Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf

1 Chambers/Row x 14.06' Long = 14.06' Row Length +6.0" Border x 2 + 12.0" End Stone x 2 = 17.06' Base Length

1 Rows x 82.7" Wide + 12.0" Side Stone x 2 = 8.90' Base Width 6.0" Base + 38.0" Chamber Height = 3.67' Field Height

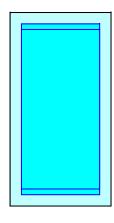
1 Chambers x 208.5 cf = 208.5 cf Chamber Storage

1 Chambers x 307.1 cf + 21.8 cf Border = 328.9 cf Displacement

556.5 cf Field - 328.9 cf Chambers = 227.6 cf Stone x 40.0% Voids = 91.1 cf Stone Storage

Chamber Storage + Stone Storage = 299.6 cf = 0.007 af Overall Storage Efficiency = 53.8% Overall System Size = 17.06' x 8.90' x 3.67'

1 Chambers (plus border) 20.6 cy Field 8.4 cy Stone



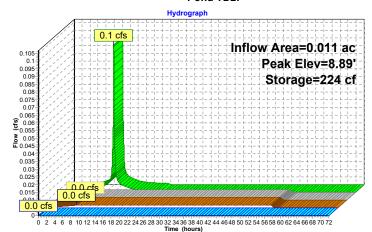


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Pond TD2:

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Summary for Pond TD3:

 Inflow Area = Inflow = O.011 ac,100.00% Impervious, Inflow Depth = 8.48" for 50-Year event

 Inflow = O.1 cfs @ 12.08 hrs, Volume= O.008 af

 Outflow = O.0 cfs @ 7.19 hrs, Volume= O.008 af, Atten= 98%, Lag= 0.0 min

 Discarded = Primary = O.0 cfs @ 0.00 hrs, Volume= O.000 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 8.89' @ 17.56 hrs Surf.Area= 152 sf Storage= 224 cf Flood Elev= 10.60' Surf.Area= 152 sf Storage= 300 cf

Plug-Flow detention time= 1,051.4 min calculated for 0.008 af (100% of inflow) Center-of-Mass det. time= 1,051.5 min (1,791.7 - 740.2)

Volume	Invert	Avail.Storage	Storage Description
#1A	6.50'	91 cf	8.90'W x 17.06'L x 3.67'H Field A
			557 cf Overall - 329 cf Embedded = 228 cf x 40.0% Voids
#2A	7.00'	209 cf	StormTrap ST1 SingleTrap 2-6 Inside #1
			Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf
			Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf
			6.90' x 14.06' Core + 0.00' x 0.50' Border = 6.90' x 15.06' System
		300 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.50'	0.520 in/hr Exfiltration over Surface area
#2	Primary	10.60'	6.0" x 240.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Discarded OutFlow Max=0.0 cfs @ 7.19 hrs HW=6.54' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=6.50' (Free Discharge) 2=Orifice/Grate (Controls 0.0 cfs)

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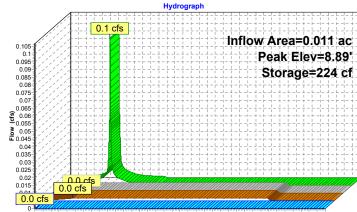
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Inflow
Outflow
Discarded

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Pond TD3:





Pond TD3: - Chamber Wizard Field A

Chamber Model = StormTrap ST1 SingleTrap 2-6 (StormTrap ST1 SingleTrap® Type VI)

Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf

1 Chambers/Row x 14.06' Long = 14.06' Row Length +6.0" Border x 2 +12.0" End Stone x 2 = 17.06' Base Length

1 Rows x 82.7" Wide + 12.0" Side Stone x 2 = 8.90' Base Width 6.0" Base + 38.0" Chamber Height = 3.67' Field Height

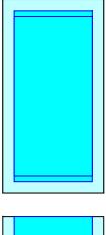
1 Chambers x 208.5 cf = 208.5 cf Chamber Storage

1 Chambers x 307.1 cf + 21.8 cf Border = 328.9 cf Displacement

556.5 cf Field - 328.9 cf Chambers = 227.6 cf Stone x 40.0% Voids = 91.1 cf Stone Storage

Chamber Storage + Stone Storage = 299.6 cf = 0.007 af Overall Storage Efficiency = 53.8% Overall System Size = 17.06' x 8.90' x 3.67'

1 Chambers (plus border) 20.6 cv Field 8.4 cy Stone





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Summary for Pond TD4:

Inflow Area	a =	0.011 ac,100	0.00% Impervious	, Inflow Depth =	8.48" for	50-Year event
Inflow	=	0.1 cfs @	12.08 hrs, Volun	ne= 0.008	3 af	
Outflow	=	0.0 cfs @	7.19 hrs, Volun	ne= 0.008	3 af, Atten=	98%, Lag= 0.0 min
Discarded	=	0.0 cfs @	7.19 hrs, Volun	ne= 0.008	3 af	
Drimory	_	വ വ ക്കേക്	0.00 bre Volum	0.000) of	

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 8.89' @ 17.56 hrs Surf.Area= 152 sf Storage= 224 cf Flood Elev= 10.60' Surf.Area= 152 sf Storage= 300 cf

Plug-Flow detention time= 1,051.4 min calculated for 0.008 af (100% of inflow) Center-of-Mass det. time= 1,051.5 min (1,791.7 - 740.2)

Volume	Invert	Avail.Storage	Storage Description
#1A	6.50'	91 cf	8.90'W x 17.06'L x 3.67'H Field A
			557 cf Overall - 329 cf Embedded = 228 cf x 40.0% Voids
#2A	7.00'	209 cf	StormTrap ST1 SingleTrap 2-6 Inside #1
			Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf
			Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf
			6.90' x 14.06' Core + 0.00' x 0.50' Border = 6.90' x 15.06' System
		300 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.50'	0.520 in/hr Exfiltration over Surface area
#2	Primary	10.60'	6.0" x 240.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Discarded OutFlow Max=0.0 cfs @ 7.19 hrs HW=6.54' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=6.50' (Free Discharge) 2=Orifice/Grate (Controls 0.0 cfs)

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Pond TD4: - Chamber Wizard Field A

Chamber Model = StormTrap ST1 SingleTrap 2-6 (StormTrap ST1 SingleTrap® Type VI)

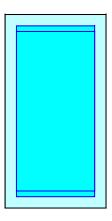
Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf

- 1 Chambers/Row x 14.06' Long = 14.06' Row Length +6.0" Border x 2 +12.0" End Stone x 2 = 17.06' Base Length
- 1 Rows x 82.7" Wide + 12.0" Side Stone x 2 = 8.90' Base Width 6.0" Base + 38.0" Chamber Height = 3.67' Field Height
- 1 Chambers x 208.5 cf = 208.5 cf Chamber Storage
- 1 Chambers x 307.1 cf + 21.8 cf Border = 328.9 cf Displacement

556.5 cf Field - 328.9 cf Chambers = 227.6 cf Stone x 40.0% Voids = 91.1 cf Stone Storage

Chamber Storage + Stone Storage = 299.6 cf = 0.007 af Overall Storage Efficiency = 53.8% Overall System Size = 17.06' x 8.90' x 3.67'

1 Chambers (plus border) 20.6 cy Field 8.4 cy Stone





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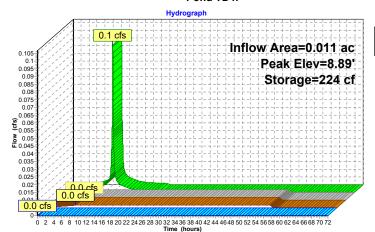
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Pond TD4:





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Summary for Pond TD5:

 Inflow Area = Inflow = O.011 ac,100.00% Impervious, Inflow Depth = 8.48" for 50-Year event

 Inflow = O.1 cfs @ 12.08 hrs, Volume= O.008 af

 Outflow = O.0 cfs @ 7.19 hrs, Volume= O.008 af, Atten= 98%, Lag= 0.0 min

 Discarded = Primary = O.0 cfs @ 0.00 hrs, Volume= O.000 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 8.89' @ 17.56 hrs Surf.Area= 152 sf Storage= 224 cf Flood Elev= 10.60' Surf.Area= 152 sf Storage= 300 cf

Plug-Flow detention time= 1,051.4 min calculated for 0.008 af (100% of inflow) Center-of-Mass det. time= 1,051.5 min (1,791.7 - 740.2)

Volume	Invert	Avail.Storage	Storage Description
#1A	6.50'	91 cf	8.90'W x 17.06'L x 3.67'H Field A
			557 cf Overall - 329 cf Embedded = 228 cf x 40.0% Voids
#2A	7.00'	209 cf	StormTrap ST1 SingleTrap 2-6 Inside #1
			Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf
			Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf
			6.90' x 14.06' Core + 0.00' x 0.50' Border = 6.90' x 15.06' System
		300 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.50'	0.520 in/hr Exfiltration over Surface area
#2	Primary	10.60'	6.0" x 240.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Discarded OutFlow Max=0.0 cfs @ 7.19 hrs HW=6.54' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=6.50' (Free Discharge) 2=Orifice/Grate (Controls 0.0 cfs)

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Pond TD5: - Chamber Wizard Field A

Chamber Model = StormTrap ST1 SingleTrap 2-6 (StormTrap ST1 SingleTrap® Type VI)

Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06"L = 208.5 cf Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06"L = 307.1 cf

1 Chambers/Row x 14.06' Long = 14.06' Row Length +6.0" Border x 2 +12.0" End Stone x 2 = 17.06' Base Length

1 Rows x 82.7" Wide + 12.0" Side Stone x 2 = 8.90' Base Width 6.0" Base + 38.0" Chamber Height = 3.67' Field Height

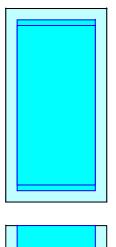
1 Chambers x 208.5 cf = 208.5 cf Chamber Storage

1 Chambers x 307.1 cf + 21.8 cf Border = 328.9 cf Displacement

556.5 cf Field - 328.9 cf Chambers = 227.6 cf Stone x 40.0% Voids = 91.1 cf Stone Storage

Chamber Storage + Stone Storage = 299.6 cf = 0.007 af Overall Storage Efficiency = 53.8% Overall System Size = 17.06' x 8.90' x 3.67'

1 Chambers (plus border) 20.6 cy Field 8.4 cy Stone

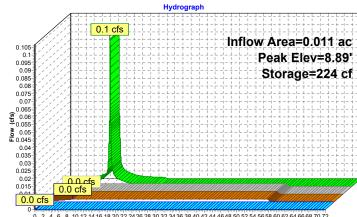


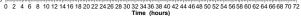
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Pond TD5:







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Summary for Pond TD6:

Inflow Area	1 =	0.011 ac,100	.00% Impervious, I	nflow Depth = 8.4	8" for 50-Year event
Inflow	=	0.1 cfs @	12.08 hrs, Volume	= 0.008 af	
Outflow	=	0.0 cfs @	7.19 hrs, Volume	= 0.008 af,	Atten= 98%, Lag= 0.0 min
Discarded	=	0.0 cfs @	7.19 hrs, Volume	= 0.008 af	_
Primary	=	0.0 cfs @	0.00 hrs, Volume	= 0.000 af	

Routing by Stor-Ind method. Time Span= 0.00-72.00 hrs. dt= 0.01 hrs. Peak Elev= 8.89' @ 17.56 hrs Surf.Area= 152 sf Storage= 224 cf Flood Elev= 10.60' Surf.Area= 152 sf Storage= 300 cf

Plug-Flow detention time= 1,051.4 min calculated for 0.008 af (100% of inflow)

Center-of-Mass det. time= 1,051.5 min (1,791.7 - 740.2)

Volume	Invert	Avail.Storage	Storage Description
#1A	6.50'	91 cf	8.90'W x 17.06'L x 3.67'H Field A
			557 cf Overall - 329 cf Embedded = 228 cf x 40.0% Voids
#2A	7.00'	209 cf	StormTrap ST1 SingleTrap 2-6 Inside #1
			Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf
			Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf
			6.90' x 14.06' Core + 0.00' x 0.50' Border = 6.90' x 15.06' System
•		300 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.50'	0.520 in/hr Exfiltration over Surface area
#2	Primary	10.60'	6.0" x 240.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Discarded OutFlow Max=0.0 cfs @ 7.19 hrs HW=6.54' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=6.50' (Free Discharge) 2=Orifice/Grate (Controls 0.0 cfs)

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Pond TD6: - Chamber Wizard Field A

Chamber Model = StormTrap ST1 SingleTrap 2-6 (StormTrap ST1 SingleTrap® Type VI)

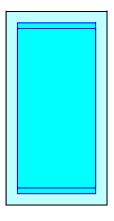
Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf

- 1 Chambers/Row x 14.06' Long = 14.06' Row Length +6.0" Border x 2 +12.0" End Stone x 2 = 17.06'
- 1 Rows x 82.7" Wide + 12.0" Side Stone x 2 = 8.90' Base Width 6.0" Base + 38.0" Chamber Height = 3.67' Field Height
- 1 Chambers x 208.5 cf = 208.5 cf Chamber Storage
- 1 Chambers x 307.1 cf + 21.8 cf Border = 328.9 cf Displacement

556.5 cf Field - 328.9 cf Chambers = 227.6 cf Stone x 40.0% Voids = 91.1 cf Stone Storage

Chamber Storage + Stone Storage = 299.6 cf = 0.007 af Overall Storage Efficiency = 53.8% Overall System Size = 17.06' x 8.90' x 3.67'

1 Chambers (plus border) 20.6 cv Field 8.4 cy Stone



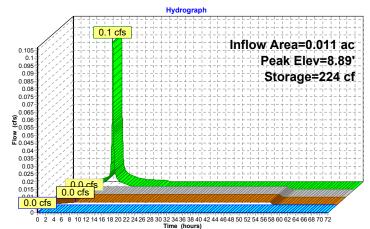


Thorndike Place - Proposed Conditions Type III 24-hr 50-Year Rainfall=8.72" Printed 6/4/2021

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Pond TD6:

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Inflow
Outflow
Discarded
Primary

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Summary for Link 1L: Towards Wetlands

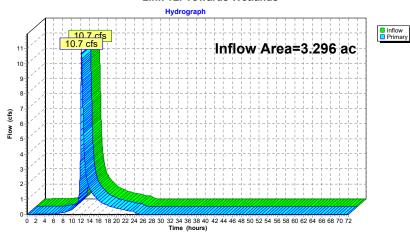
3.296 ac, 47.55% Impervious, Inflow Depth = $\,$ 5.41" for 50-Year event 10.7 cfs @ 12.19 hrs, Volume= $\,$ 1.487 af Inflow Area =

Inflow

Primary = 10.7 cfs @ 12.19 hrs, Volume= 1.487 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Link 1L: Towards Wetlands



Thorndike Place - Proposed Conditions
Type III 24-hr 50-Year Rainfall=8.72"

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Summary for Link 2L: Towards Street

Inflow Area = 0.260 ac, 51.68% Impervious, Inflow Depth = 5.24" for 50-Year event

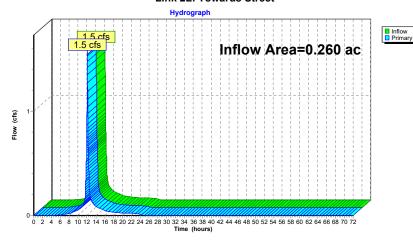
Inflow = 1.5 cfs @ 12.09 hrs, Volume= 0.113 af

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Primary = 1.5 cfs @ 12.09 hrs, Volume= 0.113 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Link 2L: Towards Street



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Thorndike Place - Proposed Conditions Type III 24-hr 50-Year Rainfall=8.72" Printed 6/4/2021

Summary for Link 100L: Total Flows

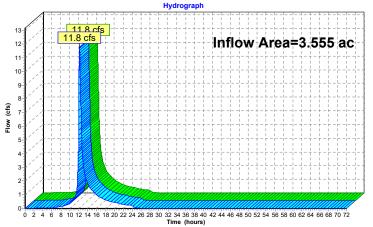
Inflow Area = 3.555 ac, 47.85% Impervious, Inflow Depth = 5.40" for 50-Year event

Inflow = 11.8 cfs @ 12.15 hrs, Volume= 1.600 af

Primary = 11.8 cfs @ 12.15 hrs, Volume= 1.600 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Link 100L: Total Flows



Inflow Primary

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Pond 2P: Rooftop Detention

Thorndike Place - Proposed Conditions Type III 24-hr 100-Year Rainfall=10.35" Printed 6/4/2021

Peak Elev=57.80' Storage=6,017 cf Inflow=3.7 cfs 0.308 af

Outflow=0.4 cfs 0.308 af

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Time span=0.00-72.00 hrs, dt=0.01 hrs, 7201 points	
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN	
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method	ł

Reach routing by Stor-Ind+I	rans method - Pond routing by Stor-Ind method
Subcatchment 1S: CB-1	Runoff Area=22,742 sf 72.16% Impervious Runoff Depth=9.25" Tc=6.0 min CN=91 Runoff=5.2 cfs 0.402 af
Subcatchment 2.1S: Building	Runoff Area=16,789 sf 100.00% Impervious Runoff Depth=10.11" Tc=6.0 min CN=98 Runoff=3.9 cfs 0.325 af
Subcatchment 2S: Building Roof	Runoff Area=15,928 sf 100.00% Impervious Runoff Depth=10.11" Tc=6.0 min CN=98 Runoff=3.7 cfs 0.308 af
Subcatchment 3.1S: Backyard ADs Flow Leng	Runoff Area=13,693 sf 8.51% Impervious Runoff Depth=7.20" th=147' Tc=10.3 min UI Adjusted CN=75 Runoff=2.3 cfs 0.189 af
Subcatchment 3S: Townhouse Roofs	Runoff Area=13,067 sf 100.00% Impervious Runoff Depth=10.11" Tc=6.0 min CN=98 Runoff=3.1 cfs 0.253 af
Subcatchment 4.2S: Townhouse TDs	Runoff Area=485 sf 100.00% Impervious Runoff Depth=10.11" Tc=6.0 min CN=98 Runoff=0.1 cfs 0.009 af
Subcatchment 4.3S: Townhouse TDs	Runoff Area=485 sf 100.00% Impervious Runoff Depth=10.11" Tc=6.0 min CN=98 Runoff=0.1 cfs 0.009 af
Subcatchment 4.4S: Townhouse TDs	Runoff Area=485 sf 100.00% Impervious Runoff Depth=10.11" Tc=6.0 min CN=98 Runoff=0.1 cfs 0.009 af
Subcatchment 4.5S: Townhouse TDs	Runoff Area=485 sf 100.00% Impervious Runoff Depth=10.11" Tc=6.0 min CN=98 Runoff=0.1 cfs 0.009 af
Subcatchment 4.6S: Townhouse TDs	Runoff Area=485 sf 100.00% Impervious Runoff Depth=10.11" Tc=6.0 min CN=98 Runoff=0.1 cfs 0.009 af
Subcatchment 5S: TD-1	Runoff Area=5,851 sf 51.63% Impervious Runoff Depth=8.62" Tc=6.0 min CN=86 Runoff=1.3 cfs 0.097 af
Subcatchment 6.1S: East driveway	Runoff Area=6,850 sf 25.93% Impervious Runoff Depth=7.86" Tc=6.0 min CN=80 Runoff=1.4 cfs 0.103 af
Subcatchment 6S: Bypass Towards Flow Length=8	Runoff Area=48,647 sf 0.22% Impervious Runoff Depth=6.94" 30' Slope=0.0133'/' Tc=15.4 min CN=73 Runoff=6.8 cfs 0.646 af
Subcatchment 7S: To Street	Runoff Area=8,882 sf 38.49% Impervious Runoff Depth=8.24" Tc=6.0 min CN=83 Runoff=1.9 cfs 0.140 af
Pond 1P: Underground Infiltration Syste Discarded=0	m Peak Elev=8.93' Storage=19,070 cf Inflow=11.8 cfs 1.248 af 0.1 cfs 0.403 af Primary=4.8 cfs 0.845 af Outflow=4.9 cfs 1.248 af

Thorndike Place - Proposed Conditions Type III 24-hr 100-Year Rainfall=10.35" 2340700-PR-2021-06-03 Printed 6/4/2021

Pond 3P: Rain garden Peak Elev=6.39' Storage=204 cf Inflow=1.4 cfs 0.103 af Discarded=0.0 cfs 0.011 af Primary=1.4 cfs 0.092 af Outflow=1.4 cfs 0.103 af

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Pond TD2: Peak Elev=9.43' Storage=280 cf Inflow=0.1 cfs 0.009 af Discarded=0.0 cfs 0.009 af Primary=0.0 cfs 0.000 af Outflow=0.0 cfs 0.009 af

Pond TD3: Peak Elev=9.43' Storage=280 cf Inflow=0.1 cfs 0.009 af

Discarded=0.0 cfs 0.009 af Primary=0.0 cfs 0.000 af Outflow=0.0 cfs 0.009 af

Pond TD4: Peak Elev=9.43' Storage=280 cf Inflow=0.1 cfs 0.009 af Discarded=0.0 cfs 0.009 af Primary=0.0 cfs 0.000 af Outflow=0.0 cfs 0.009 af

Pond TD5: Peak Elev=9.43' Storage=280 cf Inflow=0.1 cfs 0.009 af

Discarded=0.0 cfs 0.009 af Primary=0.0 cfs 0.000 af Outflow=0.0 cfs 0.009 af

Peak Elev=9.43' Storage=280 cf Inflow=0.1 cfs 0.009 af Pond TD6: Discarded=0.0 cfs 0.009 af Primary=0.0 cfs 0.000 af Outflow=0.0 cfs 0.009 af

Inflow=14.4 cfs 1.908 af Link 1L: Towards Wetlands Primary=14.4 cfs 1.908 af

Inflow=1.9 cfs 0.140 af Link 2L: Towards Street

Primary=1.9 cfs 0.140 af

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Inflow=15.9 cfs 2.048 af Link 100L: Total Flows

Primary=15.9 cfs 2.048 af

Total Runoff Area = 3.555 ac Runoff Volume = 2.509 af Average Runoff Depth = 8.47" 52.15% Pervious = 1.854 ac 47.85% Impervious = 1.701 ac

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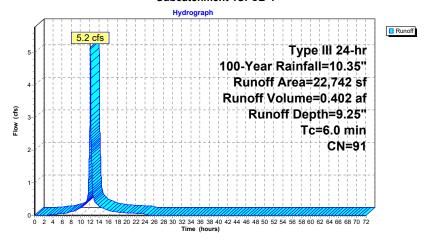
Summary for Subcatchment 1S: CB-1

Runoff = 5.2 cfs @ 12.08 hrs, Volume= 0.402 af, Depth= 9.25"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 100-Year Rainfall=10.35"

	Ar	ea (sf)	CN I	Description						
	•	16,410	98	Paved parking, HSG C						
		6,332	74	>75% Gras	s cover, Go	Good, HSG C				
	2	22,742	91	Weighted Average						
		6,332	:	27.84% Per	vious Area	a				
	•	16,410		72.16% Imp	ervious Ar	rea				
	Тс	Length	Slope	Velocity	Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		_			
	6.0					Direct Entry, Min. To				

Subcatchment 1S: CB-1



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Type III 24-hr 100-Year Rainfall=10.35"

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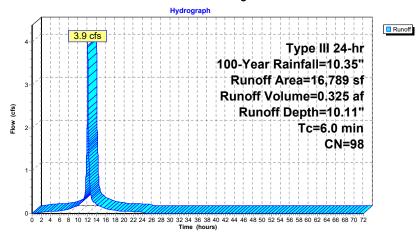
Summary for Subcatchment 2.1S: Building Roof-Southeast

Runoff = 3.9 cfs @ 12.08 hrs, Volume= 0.325 af, Depth=10.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 100-Year Rainfall=10.35"

_	Α	rea (sf)	CN	Description				
		16,789	98	Roofs, HSC	G C			
Ī		16,789		100.00% Impervious Area				
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
_	6.0					Direct Entry, Min. Tc		

Subcatchment 2.1S: Building Roof-Southeast



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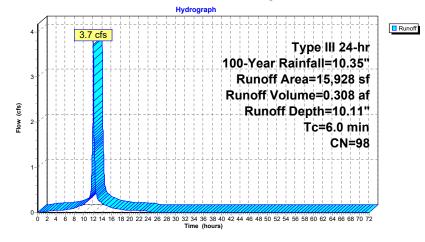
Summary for Subcatchment 2S: Building Roof

Runoff 3.7 cfs @ 12.08 hrs, Volume= 0.308 af, Depth=10.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 100-Year Rainfall=10.35"

	Α	rea (sf)	CN I	Description					
		15,928	98 I	Roofs, HSC	C C				
		15,928		100.00% Impervious Area					
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
-	6.0	, ,				Direct Entry Min Tc			

Subcatchment 2S: Building Roof



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Thorndike Place - Proposed Conditions Type III 24-hr 100-Year Rainfall=10.35" Printed 6/4/2021 Page 170

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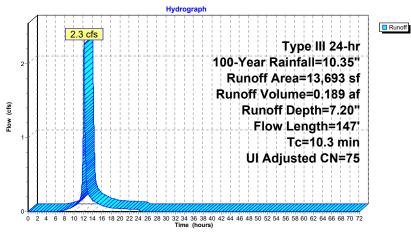
Summary for Subcatchment 3.1S: Backyard ADs

Runoff 2.3 cfs @ 12.14 hrs, Volume= 0.189 af, Depth= 7.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 100-Year Rainfall=10.35"

Α	rea (sf)	CN	Adj Desc	Description					
	1,165	98	Unco	onnected pa	avement, HSG C				
	12,528	74	>75%	>75% Grass cover, Good, HSG C					
	13,693	76	75 Weig	Weighted Average, UI Adjusted					
	12,528		91.4	9% Perviou	s Area				
	1,165		8.51	% Impervio	us Area				
	1,165		100.	00% Uncon	nected				
_					5				
Tc	Length	Slope		Capacity	Description				
(min)	(feet)	(ft/ft)		(cfs)		_			
9.4	50	0.0142	0.09		Sheet Flow,				
					Grass: Dense n= 0.240 P2= 3.23"				
0.9	97	0.0154	1.86		Shallow Concentrated Flow,				
					Grassed Waterway Kv= 15.0 fps				
10.3	147	Total							

Subcatchment 3.1S: Backyard ADs



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Direct Entry, Min. Tc

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Type III 24-hr 100-Year Rainfall=10.35"

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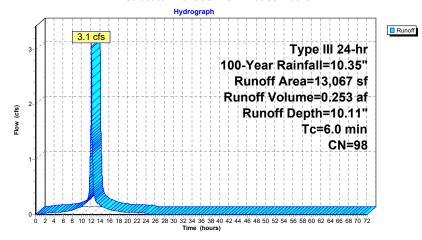
Summary for Subcatchment 3S: Townhouse Roofs

Runoff = 3.1 cfs @ 12.08 hrs, Volume= 0.253 af, Depth=10.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 100-Year Rainfall=10.35"

Ar	ea (sf)	CN E	Description		
	13,067	98 F	Roofs, HSC	C	
	13,067	1	00.00% In	pervious A	Area
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Min. Tc

Subcatchment 3S: Townhouse Roofs



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Type III 24-hr 100-Year Rainfall=10.35"

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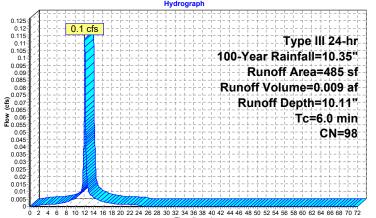
Summary for Subcatchment 4.2S: Townhouse TDs

Runoff = 0.1 cfs @ 12.08 hrs, Volume= 0.009 af, Depth=10.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 100-Year Rainfall=10.35"

Α	rea (sf)	CN I	Description					
	485	98 I	Paved parking, HSG C					
	485		100.00% Impervious Area					
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
6.0			Direct Entry Min. Tc					

Subcatchment 4.2S: Townhouse TDs



Runoff

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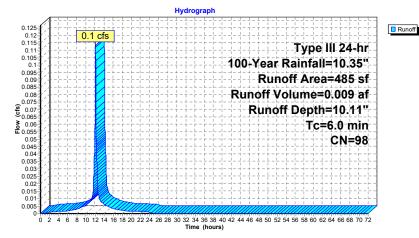
Summary for Subcatchment 4.3S: Townhouse TDs

Runoff = 0.1 cfs @ 12.08 hrs, Volume= 0.009 af, Depth=10.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 100-Year Rainfall=10.35"

A	rea (sf)	CN [Description					
	485	98 F	Paved parking, HSG C					
	485	•	100.00% Impervious Area					
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
6.0					Direct Entry, Min. Tc			

Subcatchment 4.3S: Townhouse TDs



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Type III 24-hr 100-Year Rainfall=10.35"

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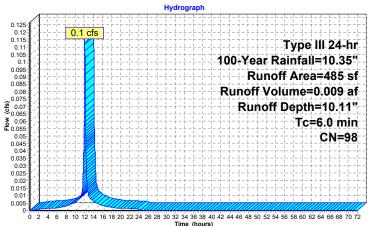
Summary for Subcatchment 4.4S: Townhouse TDs

Runoff = 0.1 cfs @ 12.08 hrs, Volume= 0.009 af, Depth=10.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 100-Year Rainfall=10.35"

Α	rea (sf)	CN I	Description					
	485	98 I	Paved parking, HSG C					
	485		100.00% Impervious Area					
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
6.0					Direct Entry, Min. Tc			

Subcatchment 4.4S: Townhouse TDs



Runoff

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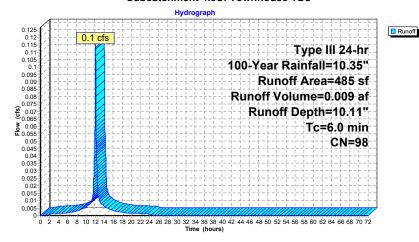
Summary for Subcatchment 4.5S: Townhouse TDs

Runoff = 0.1 cfs @ 12.08 hrs, Volume= 0.009 af, Depth=10.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 100-Year Rainfall=10.35"

A	rea (sf)	CN I	Description						
	485	98 I	Paved parking, HSG C						
	485		100.00% Impervious Area						
Тс	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·				
6.0					Direct Entry Min To				

Subcatchment 4.5S: Townhouse TDs



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Type III 24-hr 100-Year Rainfall=10.35"
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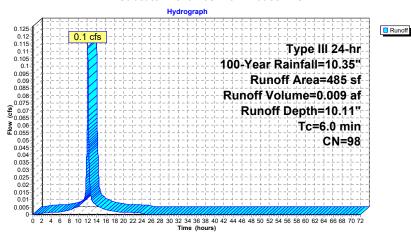
Summary for Subcatchment 4.6S: Townhouse TDs

Runoff = 0.1 cfs @ 12.08 hrs, Volume= 0.009 af, Depth=10.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 100-Year Rainfall=10.35"

Α	rea (sf)	CN I	Description					
	485	98 I	Paved parking, HSG C					
	485		100.00% Impervious Area					
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
6.0					Direct Entry, Min. Tc			

Subcatchment 4.6S: Townhouse TDs



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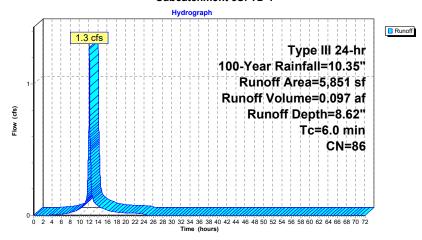
Summary for Subcatchment 5S: TD-1

Runoff = 1.3 cfs @ 12.08 hrs, Volume= 0.097 af, Depth= 8.62"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 100-Year Rainfall=10.35"

	Α	rea (sf)	CN	Description						
		3,021	98	Paved parking, HSG C						
		2,830	74	>75% Grass cover, Good, HSG C						
		5,851	86	Weighted Average						
		2,830		48.37% Pervious Area						
		3,021		51.63% Impervious Area						
	_									
		Length	Slope	,	Capacity	Description				
_	(min)	(feet)	(ft/ft	(ft/sec)	(cfs)					
	6.0					Direct Entry Min To				

Subcatchment 5S: TD-1



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Thorndike Place - Proposed Conditions

Type III 24-hr 100-Year Rainfall=10.35"

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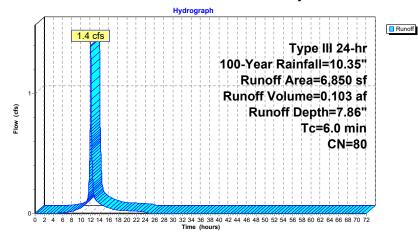
Summary for Subcatchment 6.1S: East driveway

Runoff = 1.4 cfs @ 12.09 hrs, Volume= 0.103 af, Depth= 7.86"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 100-Year Rainfall=10.35"

A	rea (sf)	CN	Description					
	5,074	74	>75% Gras	s cover, Go	ood, HSG C			
	1,776	98	Paved road	s w/curbs &	& sewers, HSG C			
	6,850	80	Weighted Average					
	5,074		74.07% Pervious Area					
	1,776		25.93% Impervious Area					
Tc (min)	Length (feet)	Slop (ft/f	,	Capacity (cfs)	Description			
6.0					Direct Entry,			

Subcatchment 6.1S: East driveway



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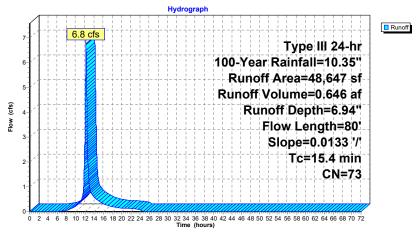
Summary for Subcatchment 6S: Bypass Towards Wetlands

Runoff = 6.8 cfs @ 12.20 hrs, Volume= 0.646 af, Depth= 6.94"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 100-Year Rainfall=10.35"

	A === (=f)	CNI	Dagarintian					
	Area (sf)	CN	CN Description					
	13,497	70	Woods, Go	od, HSG C				
	35,043	74	>75% Gras	s cover, Go	ood, HSG C			
	107	98	Roofs, HSG	G C				
	48,647	73	Weighted A	verage				
	48,540	!	99.78% Per	rvious Area				
	107	(0.22% Impe	ervious Are	a			
			•					
To	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)		(cfs)	•			
14.5	50	0.0133	0.06		Sheet Flow,			
					Woods: Light underbrush n= 0.400 P2= 3.23"			
0.9	30	0.0133	0.58		Shallow Concentrated Flow,			
					Woodland Kv= 5.0 fps			
15.4	. 80	Total			·			

Subcatchment 6S: Bypass Towards Wetlands



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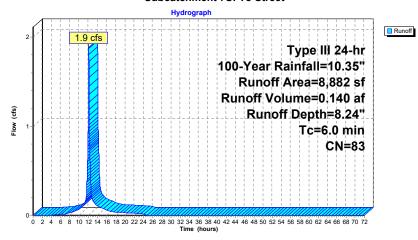
Summary for Subcatchment 7S: To Street

Runoff = 1.9 cfs @ 12.08 hrs, Volume= 0.140 af, Depth= 8.24"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 100-Year Rainfall=10.35"

A	rea (sf)	CN	Description						
	3,419	98	Paved parking, HSG C						
	5,463	74	>75% Gras	>75% Grass cover, Good, HSG C					
	8,882	83	Weighted Average						
	5,463		61.51% Pervious Area						
	3,419		38.49% Impervious Area						
Tc (min)	Length (feet)	Slop (ft/f	,	Capacity (cfs)	Description				
6.0					Direct Entry, Min. Tc				

Subcatchment 7S: To Street



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Summary for Pond 1P: Underground Infiltration System

Inflow Area = 1.636 ac, 69.57% Impervious, Inflow Depth = 9.16" for 100-Year event

Inflow = 11.8 cfs @ 12.09 hrs, Volume= 1.248 af

Outflow = 4.9 cfs @ 12.35 hrs, Volume= 1.248 af, Atten= 59%, Lag= 15.3 min

Discarded = 0.1 cfs @ 4.85 hrs, Volume= 0.403 af Primary = 4.8 cfs @ 12.35 hrs, Volume= 0.845 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 8.93' @ 12.35 hrs Surf.Area= 7,556 sf Storage= 19,070 cf

Plug-Flow detention time= 377.9 min calculated for 1.248 af (100% of inflow)

Center-of-Mass det. time= 377.9 min (1,186.3 - 808.4)

Volume	Invert	Avail.Storage	Storage Description
#1	6.00'	19,495 cf	6.89'W x 14.06'L x 3.00'H StormTrap ST-1 Units (Irregular Shape)x 78
			22,668 cf Overall x 86.0% Voids

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.00'	0.520 in/hr Exfiltration over Surface area
#2	Primary	7.45'	15.0" Round Culvert
			L= 260.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 7.45' / 6.15' S= 0.0050 '/' Cc= 0.900
			n= 0.013. Flow Area= 1.23 sf

Discarded OutFlow Max=0.1 cfs @ 4.85 hrs HW=6.03' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.1 cfs)

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Thorndike Place - Proposed Conditions

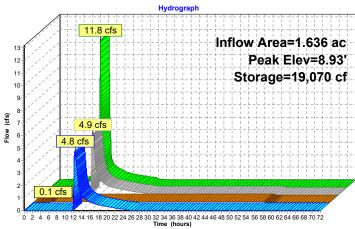
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Pond 1P: Underground Infiltration System





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Summary for Pond 2P: Rooftop Detention

0.366 ac,100.00% Impervious, Inflow Depth = 10.11" for 100-Year event Inflow Area =

3.7 cfs @ 12.08 hrs, Volume= 0.308 af Inflow

Outflow 0.4 cfs @ 12.81 hrs, Volume= 0.308 af, Atten= 90%, Lag= 43.8 min

Primary = 0.4 cfs @ 12.81 hrs, Volume= 0.308 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 57.80' @ 12.81 hrs Surf.Area= 7,500 sf Storage= 6,017 cf

Plug-Flow detention time= 192.2 min calculated for 0.308 af (100% of inflow)

Center-of-Mass det. time= 192.5 min (930.7 - 738.3)

Volume	Inv	ert Avail.Sto	rage Stor	age Description	
#1	57.0	00' 7,5	00 cf Roo	ftop Detention (Pri	smatic)Listed below (Recalc)
Elevation (fee		Surf.Area (sq-ft)	Inc.Store		
57.0	00	7,500	(0	
58.0	00	7,500	7,500	7,500	
Device	Routing	Invert	Outlet Dev	vices	
#1	Primary	8.02'	12.0" Ro	und Roof Drain	
	•		L= 16.0'	CPP, mitered to cor	form to fill, Ke= 0.700
			Inlet / Out	let Invert= 8.02' / 7.7	70' S= 0.0200 '/' Cc= 0.900
			n= 0.013,	Flow Area= 0.79 sf	
#2	Device 1	57.00'	4.0" Horiz	. Orifice/Grate C=	= 0.600
			Limited to	weir flow at low hea	ads

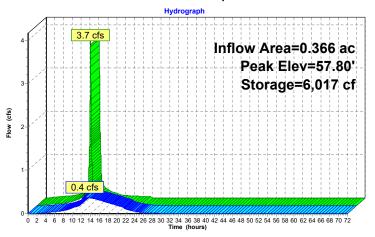
Primary OutFlow Max=0.4 cfs @ 12.81 hrs HW=57.80' (Free Discharge)
1=Roof Drain (Passes 0.4 cfs of 23.4 cfs potential flow)
2=Orifice/Grate (Orifice Controls 0.4 cfs @ 4.31 fps)

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Pond 2P: Rooftop Detention





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Summary for Pond 3P: Rain garden

Inflow Area = 0.157 ac, 25.93% Impervious, Inflow Depth = 7.86" for 100-Year event

Inflow = 1.4 cfs @ 12.09 hrs, Volume= 0.103 af

Outflow = 1.4 cfs @ 12.09 hrs, Volume= 0.103 af, Atten= 0%, Lag= 0.3 min

Discarded = 0.0 cfs @ 9.48 hrs, Volume= 0.011 af Primary = 1.4 cfs @ 12.09 hrs, Volume= 0.092 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 6.39' @ 12.09 hrs Surf.Area= 425 sf Storage= 204 cf

Plug-Flow detention time= 47.3 min calculated for 0.103 af (100% of inflow)

Center-of-Mass det. time= 47.4 min (841.0 - 793.6)

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Volume	Invert	Avail.S	torage	Storage Descriptio	n	
#1	5.60'		463 cf	Custom Stage Da	ita (Irregular)Liste	d below (Recalc)
Elevatio		rf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
5.6	30	2	2.0	0	Ó	2
6.0	00	346	75.8	50	50	459
6.3	30	425	82.0	115	165	541
7.0	00	425	82.0	298	463	598
Device	Routing	Inve	rt Outle	et Devices		
#1	Discarded	5.60	0.52	0 in/hr Exfiltration	over Surface area	 a
#2	Primary	6.30)' 22.0	long x 5.0' bread	th Broad-Crested	Rectangular Weir
						.20 1.40 1.60 1.80 2.00
			2.50	3.00 3.50 4.00 4	.50 5.00 5.50	
			Coef	f. (English) 2.34 2.5	50 2.70 2.68 2.68	8 2.66 2.65 2.65 2.65
			2.65	2.67 2.66 2.68 2	.70 2.74 2.79 2.8	38

Discarded OutFlow Max=0.0 cfs @ 9.48 hrs HW=6.30' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=1.4 cfs @ 12.09 hrs HW=6.39' (Free Discharge) —2=Broad-Crested Rectangular Weir (Weir Controls 1.4 cfs @ 0.70 fps)

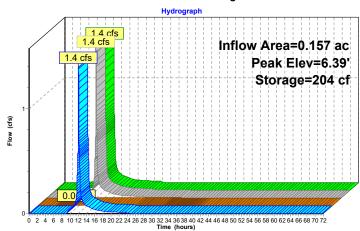
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Pond 3P: Rain garden





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Summary for Pond TD2:

Inflow Area	a =	0.011 ac,100	0.00% Impe	rvious, Inflow D	epth = 10.11"	for 100-\	∕ear event
Inflow	=	0.1 cfs @	12.08 hrs,	Volume=	0.009 af		
Outflow	=	0.0 cfs @	6.49 hrs,	Volume=	0.009 af, Att	ten= 98%,	Lag= 0.0 min
Discarded	=	0.0 cfs @	6.49 hrs,	Volume=	0.009 af		•
Drimary	_	വ വ cfc ത്	0.00 hre	Volume=	0.000 of		

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 9.43' @ 18.27 hrs Surf.Area= 152 sf Storage= 280 cf Flood Elev= 10.60' Surf.Area= 152 sf Storage= 300 cf

Plug-Flow detention time= 1,309.8 min calculated for 0.009 af (100% of inflow) Center-of-Mass det. time= 1,310.0 min (2,048.2 - 738.3)

 Volume
 Invert
 Avail.Storage
 Storage Description

 #1A
 6.50'
 91 cf
 8.90'W x 17.06'L x 3.67'H Field A

 557 cf Overall - 329 cf Embedded = 228 cf x 40.0% Voids

 #2A
 7.00'
 209 cf
 StormTrap ST1 SingleTrap 2-6 Inside #1

 Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf
 Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf

 6.90' x 14.06' Core + 0.00' x 0.50' Border = 6.90' x 15.06' System

300 cf Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.50'	0.520 in/hr Exfiltration over Surface area
#2	Primary	10.60'	6.0" x 240.0" Horiz. Orifice/Grate C= 0.600
	-		Limited to weir flow at low heads

Discarded OutFlow Max=0.0 cfs @ 6.49 hrs HW=6.54' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=6.50' (Free Discharge)

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Pond TD2: - Chamber Wizard Field A

Chamber Model = StormTrap ST1 SingleTrap 2-6 (StormTrap ST1 SingleTrap® Type VI)

Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf

1 Chambers/Row x 14.06' Long = 14.06' Row Length +6.0" Border x 2 + 12.0" End Stone x 2 = 17.06' Base Length

1 Rows x 82.7" Wide + 12.0" Side Stone x 2 = 8.90' Base Width 6.0" Base + 38.0" Chamber Height = 3.67' Field Height

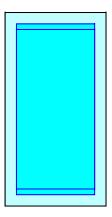
1 Chambers x 208.5 cf = 208.5 cf Chamber Storage

1 Chambers x 307.1 cf + 21.8 cf Border = 328.9 cf Displacement

556.5 cf Field - 328.9 cf Chambers = 227.6 cf Stone x 40.0% Voids = 91.1 cf Stone Storage

Chamber Storage + Stone Storage = 299.6 cf = 0.007 af Overall Storage Efficiency = 53.8% Overall System Size = 17.06' x 8.90' x 3.67'

1 Chambers (plus border) 20.6 cy Field 8.4 cy Stone



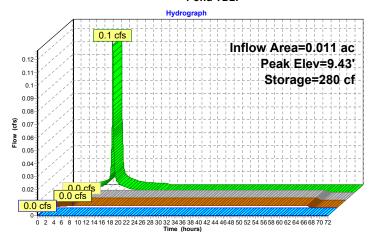


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Pond TD2:





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Summary for Pond TD3:

Inflow Area =	0.011 ac,100.00%	Impervious, Inflow I	Depth = 10.11" fo	r 100-Year event
Inflow =	0.1 cfs @ 12.08	hrs, Volume=	0.009 af	
Outflow =	0.0 cfs @ 6.49	hrs, Volume=	0.009 af, Atten	= 98%, Lag= 0.0 min
Discarded =	0.0 cfs @ 6.49	hrs, Volume=	0.009 af	_
Primary =	0.0 cfs @ 0.00	hrs, Volume=	0.000 af	

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 9.43' @ 18.27 hrs Surf.Area= 152 sf Storage= 280 cf Flood Elev= 10.60' Surf.Area= 152 sf Storage= 300 cf

Plug-Flow detention time= 1,309.8 min calculated for 0.009 af (100% of inflow) Center-of-Mass det. time= 1,310.0 min (2,048.2 - 738.3)

 Volume
 Invert
 Avail.Storage
 Storage Description

 #1A
 6.50'
 91 cf
 8.90'W x 17.06'L x 3.67'H Field A

 557 cf Overall - 329 cf Embedded = 228 cf x 40.0% Voids

 StormTrap ST1 SingleTrap 2-6 Inside #1

 Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf

 Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf

 6.90' x 14.06' Core + 0.00' x 0.50' Border = 6.90' x 15.06' System

 300 cf
 Total Available Storage

Storage Group A created with Chamber Wizard

 Device
 Routing
 Invert
 Outlet Devices

 #1
 Discarded
 6.50'
 0.520 in/hr Exfiltration over Surface area

 #2
 Primary
 10.60'
 6.0" x 240.0" Horiz. Orifice/Grate C = 0.600

 Limited to weir flow at low heads

Discarded OutFlow Max=0.0 cfs @ 6.49 hrs HW=6.54' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=6.50' (Free Discharge)
2=Orifice/Grate (Controls 0.0 cfs)

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Pond TD3: - Chamber Wizard Field A

Chamber Model = StormTrap ST1 SingleTrap 2-6 (StormTrap ST1 SingleTrap® Type VI)

Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf

1 Chambers/Row x 14.06' Long = 14.06' Row Length +6.0" Border x 2 +12.0" End Stone x 2 = 17.06'

1 Rows x 82.7" Wide + 12.0" Side Stone x 2 = 8.90' Base Width 6.0" Base + 38.0" Chamber Height = 3.67' Field Height

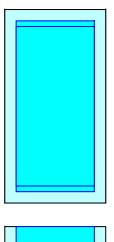
1 Chambers x 208.5 cf = 208.5 cf Chamber Storage

1 Chambers x 307.1 cf + 21.8 cf Border = 328.9 cf Displacement

556.5 cf Field - 328.9 cf Chambers = 227.6 cf Stone x 40.0% Voids = 91.1 cf Stone Storage

Chamber Storage + Stone Storage = 299.6 cf = 0.007 af Overall Storage Efficiency = 53.8% Overall System Size = 17.06' x 8.90' x 3.67'

1 Chambers (plus border) 20.6 cv Field 8.4 cy Stone



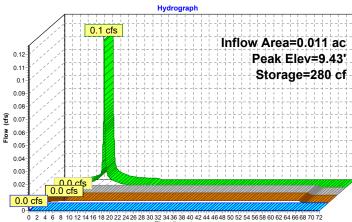
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Inflow
Outflow
Discarded

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Pond TD3:





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Summary for Pond TD4:

Inflow Area	1 =	0.011 ac,100	0.00% Impervious, Inflow D	epth = 10.11" for 100-Year event
Inflow	=	0.1 cfs @	12.08 hrs, Volume=	0.009 af
Outflow	=	0.0 cfs @	6.49 hrs, Volume=	0.009 af, Atten= 98%, Lag= 0.0 min
Discarded	=	0.0 cfs @	6.49 hrs, Volume=	0.009 af
Primary	=	0.0 cfs @	0.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 9.43' @ 18.27 hrs Surf.Area= 152 sf Storage= 280 cf Flood Elev= 10.60' Surf.Area= 152 sf Storage= 300 cf

Plug-Flow detention time= 1,309.8 min calculated for 0.009 af (100% of inflow)

Center-of-Mass det. time= 1,310.0 min (2,048.2 - 738.3)

Volume	Invert	Avail.Storage	Storage Description
#1A	6.50'	91 cf	8.90'W x 17.06'L x 3.67'H Field A
			557 cf Overall - 329 cf Embedded = 228 cf x 40.0% Voids
#2A	7.00'	209 cf	StormTrap ST1 SingleTrap 2-6 Inside #1
			Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf
			Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf
			6.90' x 14.06' Core + 0.00' x 0.50' Border = 6.90' x 15.06' System
		300 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.50'	0.520 in/hr Exfiltration over Surface area
#2	Primary	10.60'	6.0" x 240.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Discarded OutFlow Max=0.0 cfs @ 6.49 hrs HW=6.54' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=6.50' (Free Discharge) —2=Orifice/Grate (Controls 0.0 cfs)

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Thorndike Place - Proposed Conditions

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Pond TD4: - Chamber Wizard Field A

Chamber Model = StormTrap ST1 SingleTrap 2-6 (StormTrap ST1 SingleTrap® Type VI)

Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf

1 Chambers/Row x 14.06' Long = 14.06' Row Length +6.0" Border x 2 + 12.0" End Stone x 2 = 17.06' Base Length

1 Rows x 82.7" Wide + 12.0" Side Stone x 2 = 8.90' Base Width 6.0" Base + 38.0" Chamber Height = 3.67' Field Height

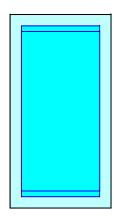
1 Chambers x 208.5 cf = 208.5 cf Chamber Storage

1 Chambers x 307.1 cf + 21.8 cf Border = 328.9 cf Displacement

556.5 cf Field - 328.9 cf Chambers = 227.6 cf Stone x 40.0% Voids = 91.1 cf Stone Storage

Chamber Storage + Stone Storage = 299.6 cf = 0.007 af Overall Storage Efficiency = 53.8% Overall System Size = 17.06' x 8.90' x 3.67'

1 Chambers (plus border) 20.6 cy Field 8.4 cy Stone





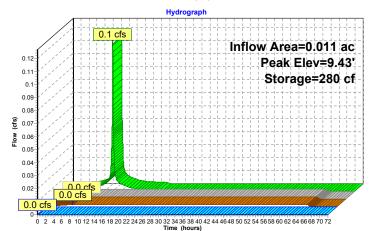
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Pond TD4:

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Inflow
Outflow
Discarded
Primary

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Summary for Pond TD5:

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 9.43' @ 18.27 hrs Surf.Area= 152 sf Storage= 280 cf Flood Elev= 10.60' Surf.Area= 152 sf Storage= 300 cf

Plug-Flow detention time= 1,309.8 min calculated for 0.009 af (100% of inflow) Center-of-Mass det. time= 1,310.0 min (2,048.2 - 738.3)

Volume	Invert	Avail.Storage	Storage Description
#1A	6.50'	91 cf	8.90'W x 17.06'L x 3.67'H Field A
			557 cf Overall - 329 cf Embedded = 228 cf x 40.0% Voids
#2A	7.00'	209 cf	StormTrap ST1 SingleTrap 2-6 Inside #1
			Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf
			Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf
			6.90' x 14.06' Core + 0.00' x 0.50' Border = 6.90' x 15.06' System
		300 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.50'	0.520 in/hr Exfiltration over Surface area
#2	Primary	10.60'	6.0" x 240.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Discarded OutFlow Max=0.0 cfs @ 6.49 hrs HW=6.54' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=6.50' (Free Discharge)
2=Orifice/Grate (Controls 0.0 cfs)

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Pond TD5: - Chamber Wizard Field A

Chamber Model = StormTrap ST1 SingleTrap 2-6 (StormTrap ST1 SingleTrap® Type VI)

Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf

1 Chambers/Row x 14.06' Long = 14.06' Row Length +6.0" Border x 2 +12.0" End Stone x 2 = 17.06'

1 Rows x 82.7" Wide + 12.0" Side Stone x 2 = 8.90' Base Width 6.0" Base + 38.0" Chamber Height = 3.67' Field Height

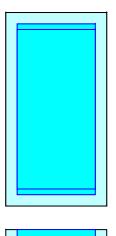
1 Chambers x 208.5 cf = 208.5 cf Chamber Storage

1 Chambers x 307.1 cf + 21.8 cf Border = 328.9 cf Displacement

556.5 cf Field - 328.9 cf Chambers = 227.6 cf Stone x 40.0% Voids = 91.1 cf Stone Storage

Chamber Storage + Stone Storage = 299.6 cf = 0.007 af Overall Storage Efficiency = 53.8% Overall System Size = 17.06' x 8.90' x 3.67'

1 Chambers (plus border) 20.6 cv Field 8.4 cy Stone



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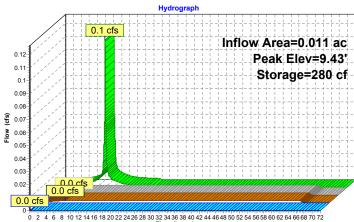
Thorndike Place - Proposed Conditions Type III 24-hr 100-Year Rainfall=10.35" Printed 6/4/2021

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Inflow
Outflow
Discarded

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Pond TD5:



0 2 4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 34 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70 72 Time (hours)

Thorndike Place - Proposed Conditions Type III 24-hr 100-Year Rainfall=10.35" Printed 6/4/2021

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Summary for Pond TD6:

Inflow Area	a =	0.011 ac,100	0.00% Impervious,	Inflow Depth = 10.11	1" for 100-\	∕ear event
Inflow	=	0.1 cfs @	12.08 hrs, Volume	e= 0.009 af		
Outflow	=	0.0 cfs @	6.49 hrs, Volume	e= 0.009 af,	Atten= 98%,	Lag= 0.0 min
Discarded	=	0.0 cfs @	6.49 hrs, Volume	e= 0.009 af		-
Primary	=	0.0 cfs @	0.00 hrs, Volume	e= 0.000 af		

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 9.43' @ 18.27 hrs Surf.Area= 152 sf Storage= 280 cf Flood Elev= 10.60' Surf.Area= 152 sf Storage= 300 cf

Plug-Flow detention time= 1,309.8 min calculated for 0.009 af (100% of inflow)

Center-of-Mass det. time= 1,310.0 min (2,048.2 - 738.3)

Volume	Invert	Avail.Storage	Storage Description
#1A	6.50'	91 cf	8.90'W x 17.06'L x 3.67'H Field A
			557 cf Overall - 329 cf Embedded = 228 cf x 40.0% Voids
#2A	7.00'	209 cf	StormTrap ST1 SingleTrap 2-6 Inside #1
			Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf
			Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf
			6.90' x 14.06' Core + 0.00' x 0.50' Border = 6.90' x 15.06' System
		300 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.50'	0.520 in/hr Exfiltration over Surface area
#2	Primary	10.60'	6.0" x 240.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Discarded OutFlow Max=0.0 cfs @ 6.49 hrs HW=6.54' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=6.50' (Free Discharge) 2=Orifice/Grate (Controls 0.0 cfs)

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Thorndike Place - Proposed Conditions
Type III 24-hr 100-Year Rainfall=10.35"
Printed 6/4/2021

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Pond TD6: - Chamber Wizard Field A

Chamber Model = StormTrap ST1 SingleTrap 2-6 (StormTrap ST1 SingleTrap® Type VI)

Inside= 82.7"W x 30.0"H => 14.83 sf x 14.06'L = 208.5 cf Outside= 82.7"W x 38.0"H => 21.84 sf x 14.06'L = 307.1 cf

1 Chambers/Row x 14.06' Long = 14.06' Row Length +6.0" Border x 2 +12.0" End Stone x 2 = 17.06' Base Length

1 Rows x 82.7" Wide + 12.0" Side Stone x 2 = 8.90' Base Width 6.0" Base + 38.0" Chamber Height = 3.67' Field Height

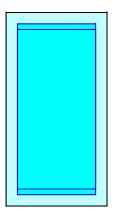
1 Chambers x 208.5 cf = 208.5 cf Chamber Storage

1 Chambers x 307.1 cf + 21.8 cf Border = 328.9 cf Displacement

556.5 cf Field - 328.9 cf Chambers = 227.6 cf Stone x 40.0% Voids = 91.1 cf Stone Storage

Chamber Storage + Stone Storage = 299.6 cf = 0.007 af Overall Storage Efficiency = 53.8% Overall System Size = 17.06' x 8.90' x 3.67'

1 Chambers (plus border) 20.6 cy Field 8.4 cy Stone





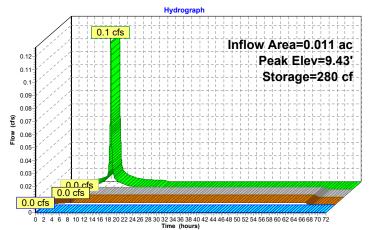
Thorndike Place - Proposed Conditions Type III 24-hr 100-Year Rainfall=10.35"

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Pond TD6:

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Inflow Outflow Discarded

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Thorndike Place - Proposed Conditions Type III 24-hr 100-Year Rainfall=10.35" Printed 6/4/2021 Page 202

Summary for Link 1L: Towards Wetlands

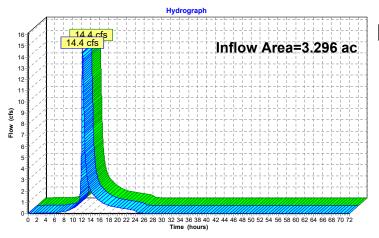
3.296 ac, 47.55% Impervious, Inflow Depth = 6.95" for 100-Year event 14.4 cfs @ 12.16 hrs, Volume= 1.908 af 1.908 af, Atten= 0%, Lag= 0.0 mi Inflow Area =

Inflow

1.908 af, Atten= 0%, Lag= 0.0 min Primary =

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Link 1L: Towards Wetlands





Thorndike Place - Proposed Conditions Type III 24-hr 100-Year Rainfall=10.35" Printed 6/4/2021

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Summary for Link 2L: Towards Street

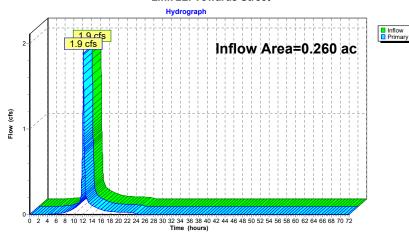
Inflow Area = 0.260 ac, 51.68% Impervious, Inflow Depth = 6.47" for 100-Year event

Inflow = 1.9 cfs @ 12.08 hrs, Volume= 0.140 af

Primary = 1.9 cfs @ 12.08 hrs, Volume= 0.140 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Link 2L: Towards Street



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Thorndike Place - Proposed Conditions

Type III 24-hr 100-Year Rainfall=10.35"

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Summary for Link 100L: Total Flows

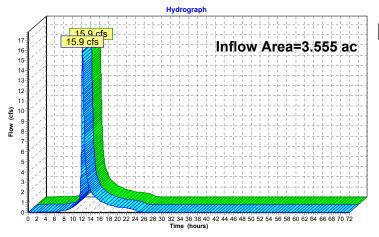
Inflow Area = 3.555 ac, 47.85% Impervious, Inflow Depth = 6.91" for 100-Year event

Inflow = 15.9 cfs @ 12.14 hrs, Volume= 2.048 af

Primary = 15.9 cfs @ 12.14 hrs, Volume= 2.048 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Link 100L: Total Flows





SECTION 6.0

ADDITIONAL DRAINAGE CALCULATIONS

6.01 TSS REMOVAL CALCULATIONS

TSS Removal Calculation Worksheet

Location: Thorndike Place, Arlington, MA

Project: 23407.00



Prepared By: D. Guerriero

Date: 6/03/2021

AREA 1 - CB-1

Total Impervious Area, Acres = 0.377

A	В	С	D	E
	TSS Removal	Starting TSS	Amount	Remaining Load
BMP	Rate	Load*	Removed (BxC)	(C-D)
Deep Sump and Hooded				
Catchbasins	0.25	1.00	0.25	0.75
Hydrodynamic Separator	0.7	0.75	0.53	0.23
Infiltration Basin	0.8	0.23	0.18	0.05

TSS Removal = 0.96

AREA 2 - TD-1

Total Impervious Area, Acres = 0.069

Α	В	C	D	<u>E</u>
	TSS Removal	Starting TSS	Amount	Remaining Load
BMP	Rate	Load*	Removed (BxC)	(C-D)
Hydrodynamic Separator	0.7	1.00	0.70	0.30
Infiltration Basin	0.8	0.30	0.24	0.06

TSS Removal = 0.94

AREA 3 - TD-2-6

Total Impervious Area, Acres= 0.056

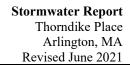
Α	В	С	D	Е
	TSS Removal	Starting TSS	Amount	Remaining Load
BMP	Rate	Load*	Removed (BxC)	(C-D)
Infiltration Basin	8.0	1.00	0.80	0.20

TSS Removal = 0.80

AREA 4 - Bypass to Street Total Impervious Area, Acres = 0.078 В D Amount Remaining Load TSS Removal Starting TSS **BMP** Rate Load* Removed (BxC) (C-D) 1.00 TSS Removal = AREA 5 - East Driveway Total Impervious Area, Acres = 0.041 D TSS Removal Starting TSS Amount Remaining Load **BMP** Load* Rate Removed (BxC) (C-D) Rain Garden 8.0 1.00 08.0 0.20 TSS Removal = 08.0 Weighted Annual Average TSS Removal Rate

[TSS Removal-1 (Area-1) + TSS Revoval-2 (Area-2) +] / [Area-1 + Area-2 + ...] = 0.81

Project Site TSS Removal = 0.81



6.02 GROUNDWATER RECHARGE VOLUME CALCULATIONS

Required Recharge Volume

 $Rv = F \times Impervious Area$

Where:

Rv = Recharge Volume

F=Target Depth Factor associated with each Hydrologic Soil Group

Impervious Area = Proposed Pavement and Rooftop area on-site

$$Rv = \left(\frac{0.25in}{12}\right)(74,100sft) =$$

Rv = 1,543 cf (required recharge volume)

As not all impervious surfaces are directed to an infiltration BMP, an adjusted Required Volume must be provided. The adjusted Required Volume (Rva) is calculated as:

$$Rva = \frac{Total\ Imp.Area}{Imp.Area\ to\ BMP} (Rv) =$$

$$Rva = \left(\frac{74{,}100sft}{53{,}785sft}\right)(1{,}543cf) =$$

$$Rva = 2,125 cf$$

Storage Provided

Underground Infiltration System = 9,422 cubic feet provided.
 Refer to the HydroCAD storage table provided for more information.

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Stage-Area-Storage for Pond 1P: Underground Infiltration System

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
6.00	7,556	(Cubic-leet)	6.37	7,556	2,404	6.74	7,556	4,809
6.01	7,556	65	6.38	7,556	2,469	6.75	7,556	4,874
6.02	7,556	130	6.39	7,556	2,534	6.76	7,556	4,939
6.03	7,556	195	6.40	7,556	2,599	6.77	7,556	5,004
6.04	7,556	260	6.41	7,556	2,664	6.78	7,556	5,069
6.05	7,556	325	6.42	7,556	2,729	6.79	7,556	5,134
6.06	7,556	390	6.43	7,556	2,794	6.80	7,556	5,199
6.07	7,556	455	6.44	7,556	2,859	6.81	7,556	5,264
6.08	7,556	520	6.45	7,556	2,924	6.82	7,556	5,329
6.09	7,556	585	6.46	7,556	2,989	6.83	7,556	5,394
6.10	7,556	650	6.47	7,556	3,054	6.84	7,556	5,459
6.11	7,556	715	6.48	7,556	3,119	6.85	7,556	5,524
6.12	7,556	780	6.49	7,556	3,184	6.86	7,556	5,589
6.13	7,556	845	6.50	7,556	3,249	6.87	7,556	5,653
6.14	7,556	910	6.51	7,556	3,314	6.88	7,556	5,718
6.15	7,556	975	6.52	7,556	3,379	6.89	7,556	5,783
6.16	7,556	1,040	6.53	7,556	3,444	6.90	7,556	5,848
6.17	7,556	1,105	6.54	7,556	3,509	6.91	7,556	5,913
6.18	7,556	1,170	6.55	7,556	3,574	6.92	7,556	5,978
6.19	7,556	1,235	6.56	7,556	3,639	6.93	7,556	6,043
6.20	7,556	1,300	6.57	7,556	3,704	6.94	7,556	6,108
6.21	7,556	1,365	6.58	7,556	3,769	6.95	7,556	6,173
6.22	7,556	1,430	6.59	7,556	3,834	6.96	7,556	6,238
6.23	7,556	1,495	6.60	7,556	3,899	6.97	7,556	6,303
6.24	7,556	1,560	6.61	7,556	3,964	6.98	7,556	6,368
6.25	7,556	1,625	6.62	7,556	4,029	6.99	7,556	6,433
6.26	7,556	1,690	6.63	7,556	4,094	7.00	7,556	6,498
6.27	7,556	1,755	6.64	7,556	4,159	7.01	7,556	6,563
6.28	7,556	1,820	6.65	7,556	4,224	7.02	7,556	6,628
6.29	7,556	1,884	6.66	7,556	4,289	7.03	7,556	6,693
6.30	7,556	1,949	6.67	7,556	4,354	7.04	7,556	6,758
6.31	7,556	2,014	6.68	7,556	4,419	7.05	7,556	6,823
6.32	7,556	2,079	6.69	7,556	4,484	7.06	7,556	6,888
6.33	7,556	2,144	6.70	7,556	4,549	7.07	7,556	6,953
6.34	7,556	2,209	6.71	7,556	4,614	7.08	7,556	7,018
6.35	7,556	2,274	6.72	7,556	4,679	7.09	7,556	7,083
6.36	7,556	2,339	6.73	7,556	4,744	7.10	7,556	7,148

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Stage-Area-Storage for Pond 1P: Underground Infiltration System (continued)

Elevation	Surface	Storage	Elevation	Surface	Storage	Elevation	Surface	Storage
(feet)	(sq-ft)	(cubic-feet)	(feet)	(sq-ft)	(cubic-feet)	(feet)	(sq-ft)	(cubic-feet)
7.11	7,556	7,213	7.48	7,556	9,617	7.85	7,556	12,022
7.12	7,556	7,278	7.49	7,556	9,682	7.86	7,556	12,087
7.13	7,556	7,343	7.50	7,556	9,747	7.87	7,556	12,152
7.14	7,556	7,408	7.51	7,556	9,812	7.88	7,556	12,217
7.15	7,556	7,473	7.52	7,556	9,877	7.89	7,556	12,282
7.16	7,556	7,538	7.53	7,556	9,942	7.90	7,556	12,347
7.17	7,556	7,603	7.54	7,556	10,007	7.91	7,556	12,412
7.18	7,556	7,668	7.55	7,556	10,072	7.92	7,556	12,477
7.19	7,556	7,733	7.56	7,556	10,137	7.93	7,556	12,542
7.20	7,556	7,798	7.57	7,556	10,202	7.94	7,556	12,607
7.21	7,556	7,863	7.58	7,556	10,267	7.95	7,556	12,672
7.22	7,556	7,928	7.59	7,556	10,332	7.96	7,556	12,737
7.23	7,556	7,993	7.60	7,556	10,397	7.97	7,556	12,802
7.24	7,556	8,058	7.61	7,556	10,462	7.98	7,556	12,867
7.25	7,556	8,123	7.62	7,556	10,527	7.99	7,556	12,932
7.26	7,556	8,188	7.63	7,556	10,592	8.00	7,556	12,997
7.27	7,556	8,253	7.64	7,556	10,657	8.01	7,556	13,062
7.28	7,556	8,318	7.65	7,556	10,722	8.02	7,556	13,127
7.29	7,556	8,383	7.66	7,556	10,787	8.03	7,556	13,191
7.30	7,556	8,448	7.67	7,556	10,852	8.04	7,556	13,256
7.31	7,556	8,513	7.68	7,556	10,917	8.05	7,556	13,321
7.32	7,556	8,578	7.69	7,556	10,982	8.06	7,556	13,386
7.33	7,556	8,643	7.70	7,556	11,047	8.07	7,556	13,451
7.34	7,556	8,708	7.71	7,556	11,112	8.08	7,556	13,516
7.35	7,556	8,773	7.72	7,556	11,177	8.09	7,556	13,581
7.36	7,556	8,838	7.73	7,556	11,242	8.10	7,556	13,646
7.37	7,556	8,903	7.74	7,556	11,307	8.11	7,556	13,711
7.38	7,556	8,968	7.75	7,556	11,372	8.12	7,556	13,776
7.39	7,556	9,033	7.76	7,556	11,437	8.13	7,556	13,841
7.40	7,556	9,098	7.77	7,556	11,502	8.14	7,556	13,906
7.41	7,556	9,163	7.78	7,556	11,567	8.15	7,556	13,971
7.42	7,556	9,228	7.79	7,556	11,632	8.16	7,556	14,036
7.43	7,556	9,293	7.80	7,556	11,697	8.17	7,556	14,101
7 44	7 556	9 358	7.81	7,556	11,762	8.18	7,556	14,166
7.45	7,556	9,422	7.82	7,556	11,827	8.19	7,556	14,231
7.46	7,556	9,487	7.83	7,556	11,892	8.20	7,556	14,296
7.47	7,556	9,552	7.84	7,556	11,957	8.21	7,556	14,361

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Stage-Area-Storage for Pond 1P: Underground Infiltration System (continued)

Elevation	Surface	Storage	Elevation	Surface	Storage	Elevation	Surface	Storage
(feet)	(sq-ft)	(cubic-feet)	(feet)	(sq-ft)	(cubic-feet)	(feet)	(sq-ft)	(cubic-feet)
8.22	7,556	14,426	8.59	7,556	16,831	8.96	7,556	19,235
8.23	7,556	14,491	8.60	7,556	16,895	8.97	7,556	19,300
8.24	7,556	14,556	8.61	7,556	16,960	8.98	7,556	19,365
8.25	7,556	14,621	8.62	7,556	17,025	8.99	7,556	19,430
8.26	7,556	14,686	8.63	7,556	17,090	9.00	7,556	19,495
8.27	7,556	14,751	8.64	7,556	17,155			•
8.28	7,556	14,816	8.65	7,556	17,220			
8.29	7,556	14,881	8.66	7,556	17,285			
8.30	7,556	14,946	8.67	7,556	17,350			
8.31	7,556	15,011	8.68	7,556	17,415			
8.32	7,556	15,076	8.69	7,556	17,480			
8.33	7,556	15,141	8.70	7,556	17,545			
8.34	7,556	15,206	8.71	7,556	17,610			
8.35	7,556	15,271	8.72	7,556	17,675			
8.36	7,556	15,336	8.73	7,556	17,740			
8.37	7,556	15,401	8.74	7,556	17,805			
8.38	7,556	15,466	8.75	7,556	17,870			
8.39	7,556	15,531	8.76	7,556	17,935			
8.40	7,556	15,596	8.77	7,556	18,000			
8.41	7,556	15,661	8.78	7,556	18,065			
8.42	7,556	15,726	8.79	7,556	18,130			
8.43	7,556	15,791	8.80	7,556	18,195			
8.44	7,556	15,856	8.81	7,556	18,260			
8.45	7,556	15,921	8.82	7,556	18,325			
8.46	7,556	15,986	8.83	7,556	18,390			
8.47	7,556	16,051	8.84	7,556	18,455			
8.48	7,556	16,116	8.85	7,556	18,520			
8.49	7,556	16,181	8.86	7,556	18,585			
8.50	7,556	16,246	8.87	7,556	18,650			
8.51	7,556	16,311	8.88	7,556	18,715			
8.52	7,556	16,376	8.89	7,556	18,780			
8.53	7,556	16,441	8.90	7,556	18,845			
8.54	7,556	16,506	8.91	7,556	18,910			
8.55	7,556	16,571	8.92	7,556	18,975			
8.56	7,556	16,636	8.93	7,556	19,040			
8.57	7,556	16,701	8.94	7,556	19,105			
8.58	7,556	16,766	8.95	7,556	19,170			
		·			•			

Drawdown Within 72-Hours

Rv = Required Recharge Volume, cu.ft. (see above)

K = Saturated Hydraulic Conductivity, in/hr (from Rawls Table)

Bottom Area = Area of Infiltration System Bottom, sq.ft.

$$Time = \frac{Rv}{(K)(Bottom\ Area)}$$

$$Time = \left(\frac{2,125\ cu.\ ft.}{(0.52in/hr)(7,556sq.\ ft.)}\right) =$$

 $Time = 6.49 \ hours$

o 6.49 hours < 72 hours

6.03 WATER QUALITY VOLUME CALCULATIONS

Water Quality Volume Calculation

 $V_{WQ} = (D_{WQ}/12 \text{ inches/foot}) * (A_{IMP} \text{ square feet})$

 V_{WO} = Required Water Quality Volume (in cubic feet)

 D_{WO} = Water Quality Depth: **0.5-inch**

A_{IMP} = Total Impervious Area (in acres) used for driveways, parking, etc.

Underground Infiltration Systems and Bio-Retention Areas

 $A_{IMP} = 74,100 \text{ sq.ft.}$

 $V_{WQ} = (0.5 \text{ inches/12 inches/foot}) * (74,100 \text{ sq.ft.})$

 $V_{\rm WQ}$ = 3,088 cubic feet (required volume), provided volume = 9,422 cubic feet (refer to the HydroCAD storage table provided in groundwater recharge section)

6.04 RIP-RAP OUTLET PROTECTION SIZING

OUTLET PROTECTION SIZING



Project No.23407.00SubjectOutlet Protection Sizing CalcsLocationArlington, MA

Calc By <u>DG</u>

Date <u>6/1/2021</u>

Checked by <u>DRR</u> Date 6/2/2021

3.19 inches

FES-1

Q=Design Discharge, (ft^3/s) 4.8 cfs D=Culvert Diameter, (ft) 1.25 ft TW=Tailwater Depth, (ft)

0.5 ft, (0.4xD for unknow tailwater, or enter known tailwater) (Tailwater depth is to be limited to between 0.4D and 1.0D)

Riprap Rock Sizing

$$D_{50} = 0.2D$$
 $\left[\begin{array}{c} Q \\ \sqrt{gD^{2.5}} \end{array}\right] 4/3 \left[\begin{array}{c} D \\ \overline{TW} \end{array}\right]$ $\begin{array}{c} g=32.2 \text{ fps} \\ D_{50} = \text{ median rock size, ft} \end{array}$ $D_{50} = 0.28$ $\begin{array}{c} 4.80 \\ \overline{TW} \end{array}$ $\begin{array}{c} 1.25 \\ \overline{TW} \end{array}$ $\begin{array}{c} 0 \\ \overline{$

Table 1: Riprap Classes and Apron Dimensions

Table 1: Triplap Classes and Apron Dimensions								
	Apron	Apron	D50					
	Depth	Length	(in)	Class				
Use Class 1	3.5D ₅₀	4D	5	1				
	3.5D50	4D	6	2				
	3.3D50	5D	10	3				
	2.2D50	6D	14	4				
	2.0D50	7D	20	5				
	2.0D50	8D	22	6				

Apron Dimensions

Length, L=5D 6 ft Depth=3.3D50 16.50 Inches

Width=3D+(2/3)L 7.92 ft (at apron end) Riprap Rock Sizing Gradation

Given Size	Size of Stone, inches				
100	8	to	10		
85	7	to	9		
50	5	to	8		
15	•	+0	7		

OUTLET PROTECTION SIZING



Project No. 23407.00

Subject Outlet Protection Sizing Calcs Arlington, MA Location

Calc By DG
Date 6/1/2021 Checked by DRR Date 6/2/2021

Roof Drain Q=Design Discharge, (ft^3/s) = 3.9 cfs D=Culvert Diameter, (ft)

TW=Tailwater Depth, (ft) 0.4 ft, (0.4xD for unknow tailwater, or enter known tailwater) (Tailwater depth is to be limited to between 0.4D and 1.0D)

Riprap Rock Sizing

$$D_{50} = 0.2D \left[\begin{array}{c} Q \\ \sqrt{9D^{2.5}} \end{array} \right] 4/3 \left[\begin{array}{c} D \\ \overline{TW} \end{array} \right] \begin{array}{c} g=32.2 \text{ fps} \\ D_{50} = \text{ median rock size, ft} \end{array}$$
 $D_{50} = 0.28 \left[\begin{array}{c} 3.90 \\ 5.67 \end{array} \right] (4/3) \left[\begin{array}{c} 1.00 \\ 0.40 \end{array} \right] = 0.42 \text{ ft}$

5.09 inches

Table 1 : Riprap Classes and Apron Dimensions
D50 Apron Apron

	Depth	Length	(in)	Class
	3.5D50	4D	5	1
Use Class 2	3.5D50	4D	6	2
	3.3D50	5D	10	3
	2.2D50	6D	14	4
	2.0D50	7D	20	5
l	2.0D50	8D	22	6

Riprap Rock Sizing Gradation

Given Size	Size of Stone, inches				
100	9	to	12		
85	8	to	11		
50	6	to	9		
45	•	to.			

Apron Dimensions Length, L=5D

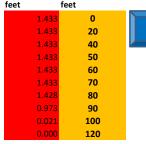
5 ft Depth=3.3D50 19 80 Inches

Width=3D+(2/3)L 6.33 ft (at apron end) 6.05 GROUNDWATER MOUNDING ANALYSIS

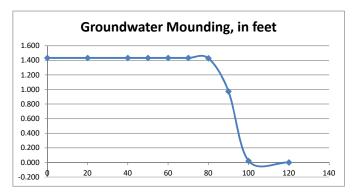
Time	Inflow	Storage	e Elevati	on Outflow	Discarde	ed Primary		
(hours)	(cfs)	(cubic-	feet) (feet)	(cfs)	(cfs)	(cfs)		Infiltration System
	11.91	0.1	102	6.02	0	0	0	
	11.92	0.1	106	6.02	0	0	0	74100 Impervious Surface (sft)
	11.93	0.1	109	6.02	0.1	0.1	0	
	11.94	0.2	112	6.02	0.1	0.1	0	0.049 Required recharge volume (acre-ft)
	11.95	0.2	116	6.02	0.1	0.1	0	
	11.96	0.2	120	6.02	0.1	0.1	0	0.100 Average infiltration rate (cfs)
	11.97	0.2	124	6.02	0.1	0.1	0	
	11.98	0.2	128	6.02	0.1	0.1	0	8640.00 Average infiltration rate (cft/day)
	11.99	0.2	133	6.02	0.1	0.1	0	
	12	0.2	139	6.02	0.1	0.1	0	7556 System bottom area (sft)
	12.01	0.3	145	6.02	0.1	0.1	0	
	12.02	0.3	152	6.02	0.1	0.1	0	
	12.03	0.3	160	6.02	0.1	0.1	0	1.143 Percoloation/application rate (ft/day)
	12.04	0.3	169	6.03	0.1	0.1	0	
								11.93 Infiltration start time
	15.95	0	116	6.02	0.1	0.1	0	
	15.96	0	115	6.02	0.1	0.1	0	16.08 Infiltration end time
	15.97	0	114	6.02	0.1	0.1	0	
	15.98	0	113	6.02	0.1	0.1	0	4.15 Time (hrs)
	15.99	0	113	6.02	0.1	0.1	0	
	16	0	112	6.02	0.1	0.1	0	0.173 Time (days)
	16.01	0	112	6.02	0.1	0.1	0	
	16.02	0	111	6.02	0.1	0.1	0	1.04 Hydraulic conductivity (ft/day)
	16.03	0	110	6.02	0.1	0.1	0	
	16.04	0	110	6.02	0.1	0.1	0	0.138 Specific yield
	16.05	0	109	6.02	0.1	0.1	0	
	16.06	0	108	6.02	0.1	0.1	0	10 Initial saturated thickness (ft)
	16.07	0	108	6.02	0.1	0.1	0	
	16.08	0	107	6.02	0.1	0.1	0	1.433 Increase in hydraulic head (ft)
	16.09	0	107	6.02	0	0	0	
	16.1	0	106	6.02	0	0	0	Note that full tabular hydrograph not printed for brevity

Input Values			inch/h	our	feet/day	y
1.1430	R	Recharge (infiltration) rate (feet/day)		0.67	,	1.33
0.138	Sy	Specific yield, Sy (dimensionless, between 0 and 1)				
1.04	K	Horizontal hydraulic conductivity, Kh (feet/day)*		2.00)	4.00 In the report accompanying this spreadsheet (USGS SIR 2010-5102), vertical soil permeability (ft/d) is assumed to be one-tenth horizontal
91.390	x	1/2 length of basin (x direction, in feet)				
20.670	У	1/2 width of basin (y direction, in feet)	hours	days	days	
0.173	t	duration of infiltration period (days)		36	;	1.50 hydraulic conductivity (ft/d).
10.000	hi(0)	initial thickness of saturated zone (feet)				
11.433 1.433	h(max) Δh(max)	maximum thickness of saturated zone (beneath center o maximum groundwater mounding (beneath center of ba				· · · · ·

Ground- Distance from water center of basin Mounding, in in x direction, in







Disclaimer

This spreadsheet solving the Hantush (1967) equation for ground-water mounding beneath an infiltration basin is made available to the general public as a convenience for those wishing to replicate values documented in the USGS Scientific Investigations Report 2010-5102 "Groundwater mounding beneath hypothetical stormwater infiltration basins" or to calculate values based on user-specified site conditions. Any changes made to the spreadsheet (other than values identified as user-specified) after transmission from the USGS could have unintended, undesirable consequences. These consequences could include, but may not be limited to: erroneous output, numerical instabilities, and violations of underlying assumptions that are inherent in results presented in the accompanying USGS published report. The USGS assumes no responsibility for the consequences of any changes made to the spreadsheet. If changes are made to the spreadsheet, the user is responsible for documenting the changes and justifying the results and conclusions.

6.06 ILLICIT DISCHARGE COMPLIANCE STATEMENT

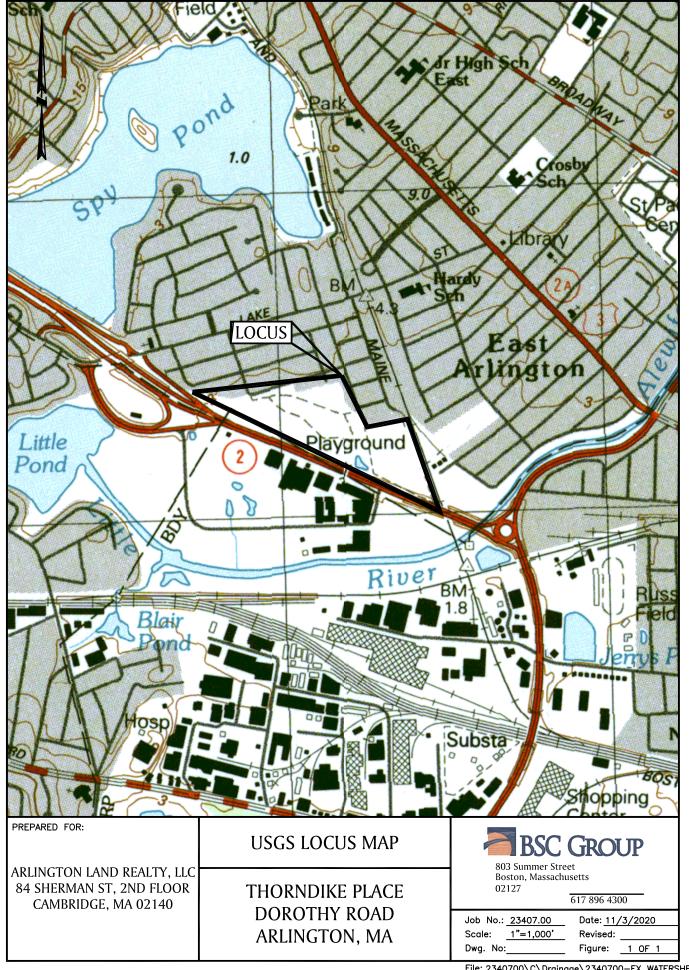
Illicit Discharge Compliance Statement

Date

This statement is to document that, to the best of my knowledge and belief, there are no and will be no
illicit discharges to the stormwater management systems or protected wetland resource areas for the
Thorndike Place residential development on Dorothy Road in Arlington, Massachusetts.
Authorized Signature/Title

APPENDIX A

USGS LOCUS MAP

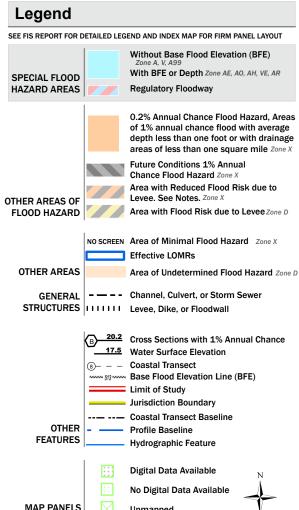


APPENDIX B

FEMA MAP

National Flood Hazard Layer FIRMette



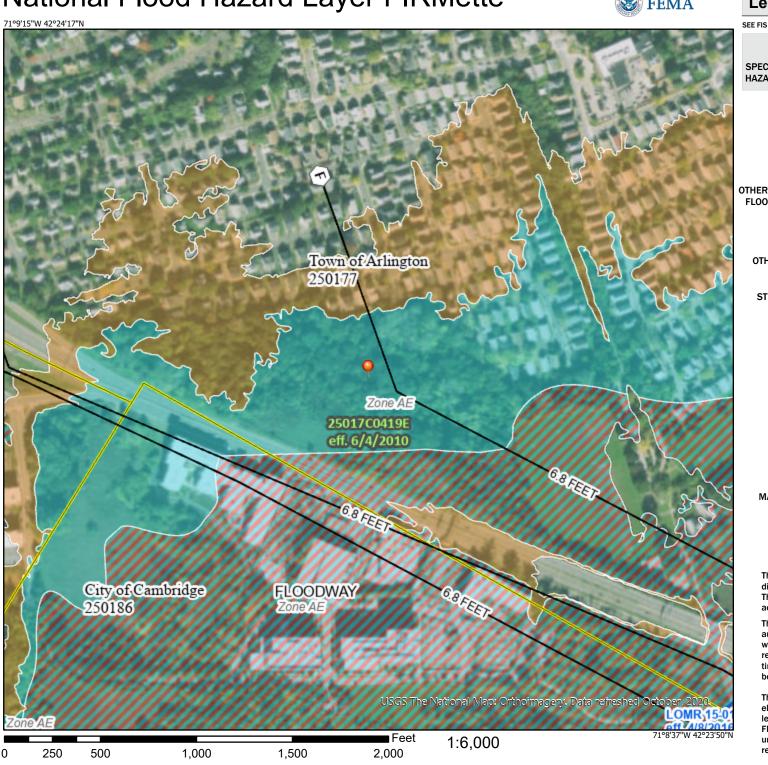


MAP PANELS Unmapped The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 11/2/2020 at 3:34 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.



APPENDIX C

WEB SOIL SURVEY



NRCS

Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for Middlesex County, Massachusetts



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2 053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



0 200 400 800 1200
Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 19N WGS84

MAP LEGEND

Area of Interest (AOI)

Area of Interest (AOI)

Soils

Soil Map Unit Polygons

Soil Map Unit Lines

Soil Map Unit Points

Special Point Features

(o)

Blowout

Borrow Pit

Clay Spot

Closed Depression

Gravel Pit

Gravelly Spot

Landfill Lava Flow

Marsh or swamp

Mine or Quarry

Miscellaneous Water Perennial Water

Rock Outcrop

Saline Spot

Sandy Spot

Slide or Slip

Severely Eroded Spot

Sinkhole

Sodic Spot

Spoil Area



Stony Spot



Very Stony Spot



Wet Spot Other



Special Line Features

Water Features

Streams and Canals

Transportation

Rails

Interstate Highways

US Routes



Major Roads

00

Local Roads

Background

Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:25.000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Middlesex County, Massachusetts Survey Area Data: Version 20, Jun 9, 2020

Soil map units are labeled (as space allows) for map scales 1:50.000 or larger.

Date(s) aerial images were photographed: Sep 11, 2019—Oct 5, 2019

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
51A	Swansea muck, 0 to 1 percent slopes	4.3	4.6%
52A	Freetown muck, 0 to 1 percent slopes	10.4	11.2%
603	Urban land, wet substratum	32.1	34.5%
626B	Merrimac-Urban land complex, 0 to 8 percent slopes	14.3	15.4%
655	Udorthents, wet substratum	31.9	34.3%
Totals for Area of Interest	'	92.9	100.0%

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Middlesex County, Massachusetts

51A—Swansea muck, 0 to 1 percent slopes

Map Unit Setting

National map unit symbol: 2trl2 Elevation: 0 to 1,140 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

Map Unit Composition

Swansea and similar soils: 80 percent Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Swansea

Setting

Landform: Swamps, bogs

Landform position (three-dimensional): Dip

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Highly decomposed organic material over loose sandy and

gravelly glaciofluvial deposits

Typical profile

Oa1 - 0 to 24 inches: muck
Oa2 - 24 to 34 inches: muck
Cg - 34 to 79 inches: coarse sand

Properties and qualities

Slope: 0 to 1 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Very poorly drained

Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: About 0 to 6 inches

Frequency of flooding: Rare Frequency of ponding: Frequent

Available water capacity: Very high (about 16.5 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8w

Hydrologic Soil Group: B/D

Ecological site: F144AY043MA - Acidic Organic Wetlands

Hydric soil rating: Yes

Minor Components

Freetown

Percent of map unit: 10 percent Landform: Bogs, swamps

Landform position (three-dimensional): Dip

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

Whitman

Percent of map unit: 5 percent

Landform: Depressions, drainageways

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

Scarboro

Percent of map unit: 5 percent

Landform: Drainageways, depressions

Landform position (two-dimensional): Toeslope

Landform position (three-dimensional): Base slope, tread, dip

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

52A—Freetown muck, 0 to 1 percent slopes

Map Unit Setting

National map unit symbol: 2t2q9

Elevation: 0 to 1,110 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

Map Unit Composition

Freetown and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Freetown

Setting

Landform: Depressions, depressions, bogs, marshes, kettles, swamps

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread, dip

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Highly decomposed organic material

Typical profile

Oe - 0 to 2 inches: mucky peat Oa - 2 to 79 inches: muck

Properties and qualities

Slope: 0 to 1 percent

Surface area covered with cobbles, stones or boulders: 0.0 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Very poorly drained

Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: About 0 to 6 inches

Frequency of flooding: Rare Frequency of ponding: Frequent

Available water capacity: Very high (about 19.2 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 5w

Hydrologic Soil Group: B/D

Ecological site: F144AY043MA - Acidic Organic Wetlands

Hydric soil rating: Yes

Minor Components

Swansea

Percent of map unit: 5 percent

Landform: Kettles, depressions, depressions, marshes, swamps, bogs

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread, dip

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

Scarboro

Percent of map unit: 5 percent

Landform: Depressions, drainageways

Landform position (two-dimensional): Toeslope

Landform position (three-dimensional): Base slope, tread, dip

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

Whitman

Percent of map unit: 5 percent

Landform: Depressions, drainageways

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

603—Urban land, wet substratum

Map Unit Setting

National map unit symbol: 9951

Mean annual precipitation: 32 to 50 inches
Mean annual air temperature: 45 to 50 degrees F

Frost-free period: 110 to 200 days

Farmland classification: Not prime farmland

Map Unit Composition

Urban land: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Urban Land

Setting

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Linear Across-slope shape: Linear

Parent material: Excavated and filled land over alluvium and/or marine deposits

Minor Components

Udorthents, loamy

Percent of map unit: 10 percent

Hydric soil rating: No

Rock outcrop

Percent of map unit: 5 percent

Landform: Ledges

Landform position (two-dimensional): Summit Landform position (three-dimensional): Head slope

Down-slope shape: Concave Across-slope shape: Concave

626B—Merrimac-Urban land complex, 0 to 8 percent slopes

Map Unit Setting

National map unit symbol: 2tyr9

Elevation: 0 to 820 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 250 days

Farmland classification: Not prime farmland

Map Unit Composition

Merrimac and similar soils: 45 percent

Urban land: 40 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Merrimac

Setting

Landform: Eskers, moraines, outwash terraces, outwash plains, kames Landform position (two-dimensional): Backslope, footslope, summit, shoulder

Landform position (three-dimensional): Side slope, crest, riser, tread

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Loamy glaciofluvial deposits derived from granite, schist, and gneiss over sandy and gravelly glaciofluvial deposits derived from granite,

schist, and gneiss

Typical profile

Ap - 0 to 10 inches: fine sandy loam Bw1 - 10 to 22 inches: fine sandy loam

Bw2 - 22 to 26 inches: stratified gravel to gravelly loamy sand 2C - 26 to 65 inches: stratified gravel to very gravelly sand

Properties and qualities

Slope: 0 to 8 percent

Depth to restrictive feature: More than 80 inches Drainage class: Somewhat excessively drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very

high (1.42 to 99.90 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum content: 2 percent Maximum salinity: Nonsaline (0.0 to 1.4 mmhos/cm)

Sodium adsorption ratio, maximum: 1.0

Available water capacity: Low (about 4.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: A

Ecological site: F144AY022MA - Dry Outwash

Hydric soil rating: No

Description of Urban Land

Typical profile

M - 0 to 10 inches: cemented material

Properties and qualities

Slope: 0 to 8 percent

Depth to restrictive feature: 0 inches to manufactured layer

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Very low (0.00 to 0.00

in/hr)

Available water capacity: Very low (about 0.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8

Hydrologic Soil Group: D Hydric soil rating: Unranked

Minor Components

Windsor

Percent of map unit: 5 percent

Landform: Dunes, outwash terraces, deltas, outwash plains

Landform position (three-dimensional): Tread, riser

Down-slope shape: Convex, linear Across-slope shape: Convex, linear

Hydric soil rating: No

Sudbury

Percent of map unit: 5 percent

Landform: Outwash plains, terraces, deltas
Landform position (two-dimensional): Footslope
Landform position (three-dimensional): Tread, dip

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

Hinckley

Percent of map unit: 5 percent

Landform: Eskers, kames, deltas, outwash plains

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Nose slope, side slope, crest, head slope,

rise

Down-slope shape: Convex Across-slope shape: Convex, linear

Hydric soil rating: No

655—Udorthents, wet substratum

Map Unit Setting

National map unit symbol: vr1n Elevation: 0 to 3.000 feet

Mean annual precipitation: 32 to 54 inches Mean annual air temperature: 43 to 54 degrees F

Frost-free period: 110 to 240 days

Farmland classification: Not prime farmland

Map Unit Composition

Udorthents, wet substratum, and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Udorthents, Wet Substratum

Setting

Parent material: Loamy alluvium and/or sandy glaciofluvial deposits and/or loamy glaciolacustrine deposits and/or loamy marine deposits and/or loamy basal till and/or loamy lodgment till

Properties and qualities

Slope: 0 to 8 percent

Depth to restrictive feature: More than 80 inches Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Minor Components

Urban land

Percent of map unit: 8 percent

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Linear Across-slope shape: Linear

Freetown

Percent of map unit: 4 percent Landform: Depressions, bogs

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Dip

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

Swansea

Percent of map unit: 3 percent Landform: Bogs, depressions

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Dip

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

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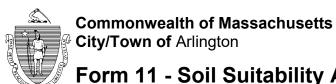
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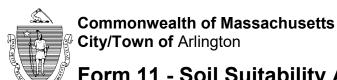
APPENDIX D

TEST PIT LOGS



Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

Α.	Facility Information					
	Arlington Land Realty, LLC					
	Owner Name					
	Dorothy Road		16-8-2, 16-8-3, 16	6-8-4, 16-8-5,	16-8-6, 16	5-8-7A
	Street Address		Map/Lot #			
		MA	02474			
	City	State	Zip Code			
В.	Site Information					
1.	(Check one) ⊠ New Construction ☐ Upgr	rade 🗌 Repair				
2.	Soil Survey Available? ☐ Yes ☐ No	If yes:		Web Soil S Source	urvey	655, 51A Soil Map Unit
	Udorthents, Swansea Muck	Fill throughout site; clay base la	yer in one test pit			
	Soil Name	Soil Limitations	,			
	Glaciofluvial deposit	Depression				
	Soil Parent material	Landform				
3.	Surficial Geological Report Available? ⊠ Yes ☐ No	If yes: 2018/USGS		Glaciomarine	e fine depo	osits, stagnant ice deposits
-		Year Published/	Source	Map Unit		
	fine/very fine sand down to very fine sand, silt, silty clared Description of Geologic Map Unit:	ay, and clay				
4.	Flood Rate Insurance Map Within a regulatory	floodway?)			
5.	Within a velocity zone? ☐ Yes ☒ No					
6.	Within a Mapped Wetland Area? ☐ Yes ☐ 1	No If yes, Mass	GIS Wetland Data	Layer:	Shallow I Wetland Ty	marsh meadow
7.		11/25/2020 Month/Day/ Year	Range: 🛛 Abo	ve Normal	☐ Norm	·
8.		ne I, II, or IWPA (OLIVER)				



	Form	11 - Soi	l Suitabilit	y Ass	sessmei	nt for	On-Si	te Sew	age Dis	posal			
C. On-	Site Revi	ew (minim	um of two hole	es requi	ired at ever	ry propo	sed prim	nary and r	eserve disp	osal area)			
Deep	Observation	n Hole Numb		11/25/	2020	7:45 A	M	Cloudy	, 30deg	42.40 N		71.15 W	
	Woodl	and adjacent	Hole # to residential/hig	Date hway	Forest	Time		Weather Some large	boulders	Latitude		Longitude: 0-2%	
1. Land			ural field, vacant lot, e		Vegetation				s (e.g., cobbles,	stones, boulder	rs, etc.)	Slope (%)	
De	scription of Lo	ocation:											
2. Soil F	Parent Materia	al: Glacioflu	vial deposits		De	epression		SU					
			•		La	ndform		Posi	tion on Landscap	e (SU, SH, BS,	FS, TS)		
3. Dista	nces from:	Oper	n Water Body	>100 feet		D	rainage W	/ay <u>>100</u> fe	et	We	tlands	<u>>100</u> feet	
		ļ	Property Line >	<u>>100</u> feet		Drinking	g Water W	/ell <u>>100</u> fe	et	(Other	feet	
4. Unsuita	able Materials	s Present: 🗵] Yes 🗌 No	If Yes: [☐ Disturbed S	Soil 🛛 I	Fill Material	ı 🗆 \	Neathered/Fra	ctured Rock	Bed	lrock	
- 0					If								
o. Groui	ndwater Obse	erved: X Yes	s 🗌 No		If yes		epth Weepir	ng from Pit	<u>1</u>	08" Depth Sta	nding Wat	er in Hole	
						Soil Log							
Depth (in)	Soil Horizon	Soil Texture	Soil Matrix: Color-	Red	oximorphic Fea	tures		Fragments Volume	Cail Churchuna	Soil		Other	
Depth (in)	/Layer	(USDA	Moist (Munsell)	Depth	Color	Percent	Gravel	Cobbles & Stones	Soil Structure	(Moist)		Other	
0"-10	Α	SL	7.5YR 2.5/1				0	0	massive	friable			
10"-36"	B (fill)	gravelly sandy loam	10YR 3/3				10	2-4	massive	very friable			
36"-48"													
10" 100"	C1 (fill)	gravelly	10VD 2/1				15 20	4.6	maaaiya	von frieble			

15-20

0

15-20

4-6

0

4-6

massive

single grain

massive

Additional Notes:

C1 (fill)

C2 (fill)

2C2 (fill)

48"-108"

36"-78"

78"-108"

Elevation of TP-1 = 12.0. Groundwater at bottom of test pit (9' - elevation 3.0). Test pit mostly fill

10YR 2/1

10YR 5/4

10YR 2/1

sandy loam

loamy sand

gravelly

sandy loam

very friable

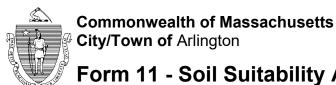
loose

very friable

sandy layer (only on E side

of test pit) gravelly layer below sandy

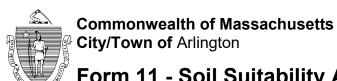
layer on É side of test pit



Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

Deep	Observation	Hole Numl	ber: <u>TP-2</u> Hole #		1/25/20	8:45AM		Cloudy, 35deg	42.40 N	1	71.15 W
				20		Time		/eather	Latitude		Longitude:
Land I			ent to resider		<u>vay</u>	Forest		Some larg	ge boulders arc	ound	0-2%
	(e.g.,	woodland, agr	icultural field, vad	cant lot, etc	.)	Vegetation		Surrace Sto	nes (e.g., copples,	stones, boulders,	etc.) Slope (%)
Descr	ption of Loca	ation:									
		. Glaciofl	luvial deposits	S			Depression	on		SU	
Soil P	arent Materia	ıl: = = = = = = = = = = = = = = = = = = =					Landform				cape (SU, SH, BS, FS, T
Distar	ces from:	Open Wate	r Body <u>>100</u>	o feet		Drain	age Way	>100 feet	Wetla	nds <u>>100</u> feet	
		Propert	ty Line >100) feet		Drinking W	ater Well	>100 feet	Ot	her fee	et
. Unsuita	ble		-, <u></u>								
Materia	ls Present: [⊠ Yes 🔲 I	No If Yes:	☐ Distu	rbed Soil		erial	☐ Weathered	Fractured Rock	☐ Bedrock	
Groun	dwater Obse	rved: Ye	s 🛛 No			ľ	f yes:	Depth Weepin	g from Pit	Depth S	tanding Water in Hole
						So	il Log				
		0 11 7 1	Cail Matrix	Redo	ximorphic	Features		e Fragments		Soil	
Depth (in)	Soil Horizon /Layer	Soil Texture (USDA)	Soil Matrix: Color-Moist					y Volume Cobbles &	Soil Structure	Consistence	Other
		` ,	(Munsell)	Depth	Color	Percent	Gravel	Stones		(Moist)	
0-7	Α	sandy loam	10YR 2.5/1				0	0	massive	friable	
7 400	0 (511)	gravelly	40)/17 0/0				45.00	1.0		6	
7-132	C (fill)	sandy loam	10YR 3/2				15-20	4-6	massive	friable	
					l			1	1	l l	

Elevation of TP-2 = 11.2. Estimated groundwater elevation (to bottom of test pit) = 0.2. Fill throughout test pit. No groundwater observed



Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

D. Determination of High Groundwater Elevation

1.	Method Used:		Obs. Hole #TP-1	Obs.	Hole # <u>TP-2</u>	
	$oxed{oxed}$ Depth observed standing water in observation	hole	<u>108</u> inches		_ inches	
	Double continue from the of the continue halo		to the		to the co	
	Depth weeping from side of observation hole		inches		_ inches	
	☐ Depth to soil redoximorphic features (mottles)		inches		_ inches	
	Depth to adjusted seasonal high groundwater ((USGS methodology)	S _h)	inches		_ inches	
	Index Well Number	Reading Date				
	$S_h = S_c - [S_r \times (OW_c - OW_{max})/OW_r]$					
	Obs. Hole/Well# S _c	S _r	OW _c	OW _{max}	OW _r	S _h
2. E	Estimated Depth to High Groundwater: 108 inches					
E.	Depth of Pervious Material					
1.	Depth of Naturally Occurring Pervious Material					
	a. Does at least four feet of naturally occurring pe system?	rvious material exis	st in all areas observed	throughout the	e area proposed for th	ne soil absorption
	☐ Yes					
	b. If yes, at what depth was it observed (exclude A Horizons)?	A and O	Upper boundary:	inches	ower boundary:	inches
	c. If no, at what depth was impervious material ob	served?	Upper boundary:		ower boundary:	>108 (fill material)



F. Certification

I certify that I am currently approved by the Department of Environmental Protection pursuant to 310 CMR 15.017 to conduct soil evaluations and that the above analysis has been performed by me consistent with the required training, expertise and experience described in 310 CMR 15.017. I further certify that the results of my soil evaluation, as indicated in the attached Soil Evaluation Form, are accurate and in accordance with 310 CMR 15.100 through 15.107.

	11/25/2020	
Signature of Soil Evaluator	Date	
Emily Derrig SE14158	12/1/2020	
Typed or Printed Name of Soil Evaluator / License #	Expiration Date of License	
Name of Approving Authority Witness	Approving Authority	

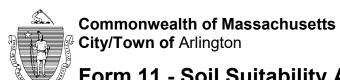
Note: In accordance with 310 CMR 15.018(2) this form must be submitted to the approving authority within 60 days of the date of field testing, and to the designer and the property owner with <u>Percolation Test Form 12</u>.

Field Diagrams: Use this area for field diagrams:



Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

Α.	Facility Information						
	Arlington Land Realty, LLC						
	Owner Name						
	Dorothy Road		16-8-2, 16-8-3, 16	6-8-4, 16-8-5,	16-8-6, 1	6-8-7A	
	Street Address		Map/Lot #				
		MA	02474				
	City	State	Zip Code				
В.	Site Information						
1.	(Check one) New Construction Upg	rade 🗌 Repair					
2.	Soil Survey Available? ☐ Yes ☐ No	If yes:		Web Soil S	Survey	655, 51A	
	, – –	•		Source		Soil Map Unit	
	Udorthents, Swansea Muck	Fill throughout site; clay base la	ayer in one test pit				
	Soil Name	Soil Limitations					
	Glaciofluvial deposit	Depression					
	Soil Parent material	Landform					
3.	Surficial Geological Report Available? ⊠ Yes ☐ No	If yes: 2018/USGS		Glaciomarin	e fine dep	posits, stagnant ice depo	site
	v i L L	Year Published	/Source	Map Unit		, , ,	
	fine/very fine sand down to very fine sand, silt, silty cl	ay, and clay					
	Description of Geologic Map Unit:						
4.	Flood Rate Insurance Map Within a regulatory	floodway? 🗌 Yes 🖂 No	o				
5.	Within a velocity zone? ☐ Yes ☐ No						
6.	Within a Mapped Wetland Area? ☐ Yes ☐ ☐	No If yes, Mass	GIS Wetland Data	Layer:	Shallow Wetland T	v marsh meadow Type	
7.	` '	11/25/2020 Month/Day/ Year	Range: 🛛 Abo	ve Normal	☐ Norr	mal 🔲 Below Norma	1
8.	Other references reviewed: Not in Zor	ne I, II, or IWPA (OLIVER)					

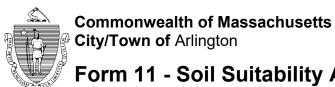


	Form	11 - Soi	l Suitabilit	y Ass	sessmei	nt for	On-Si	te Sew	age Dis	posal			
C. On-	Site Revi	ew (minim	um of two hole	es requ	ired at ever	ry propo	sed prim	nary and r	eserve disp	osal area)			
Deep	Observation	n Hole Numb	er: <u>TP-3</u> Hole #	11/25/ Date	2020	9:45 A Time	M	Cloudy Weather	, 40deg	42.40 N Latitude		71.15 W Longitude:	
I. Land			to residential/hig ural field, vacant lot, e		Forest Vegetation			Some large	e boulders es (e.g., cobbles,	stones boulder	s etc.)	0-2% Slope (%)	
Des	scription of Lo	•	arar nora, vacam rot, c	,,	vogotation			ouridoo otorio	,o (o.g., oobbioo,	otorioo, bouldor	0, 0.0.,	0.000 (70)	
	' arent Materia		vial deposits		De	epression		FS					
					La	ndform		Posi	tion on Landscap	e (SU, SH, BS,	FS, TS)		
3. Distar	nces from:	Ope	n Water Body	>100 feet		D	rainage W	/ay <u>>100</u> fe	eet	We	tlands	<u>>100</u> feet	
			Property Line	>100 feet		Drinking	g Water W	/ell <u>>100</u> fe	eet	(Other	feet	
I. Unsuita	ıble Materials	s Present: 🗵	Yes No	If Yes: [☐ Disturbed S	Soil 🛛 I	- Fill Material		Weathered/Fra	ctured Rock	□Ве	drock	
5. Grour	ndwater Obse	erved: X Yes	s 🗌 No		If yes	3: <u>84"</u> De	pth Weeping	g from Pit	<u>1</u>	44" Depth Sta	nding Wa	ter in Hole	
						Soil Log							
Donth (in)	Soil Horizon	Soil Texture	Soil Matrix: Color-	Red	oximorphic Fea	tures		Fragments Volume	Soil Structure	Soil		Other	
Depth (in)	/Layer	(USDA	Moist (Munsell)	Depth	Color	Percent	Gravel	Cobbles & Stones	Son Structure	(Moist)		Other	
0"-8"	Α	SL	10YR 2/1				0	0	massive	very friable			
8"-84"	R	SI	7 5VR 2 5/2	36"	7 5VR 5/8	2-4%	2-4	0	massive	friable			

Donth (in)	Soil Horizon	Soil Texture	Soil Matrix: Color-	Rede	oximorphic Fea	tures		Volume	Soil Structure	Soil Consistence	Other
Depth (in)	/Layer	(USDA	Moist (Munsell)	Depth	Color	Percent	Gravel	Cobbles & Stones	Son Structure	(Moist)	Other
0"-8"	Α	SL	10YR 2/1	1			0	0	massive	very friable	
8"-84"	В	SL	7.5YR 2.5/2	36"	7.5YR 5/8	2-4%	2-4	0	massive	friable	
84"-108"	C1	Sandy Clay Loam	10YR 2/1				0	0	massive	firm	
108"- 144"	C2	Clay	GLEY 2 4/5B				0	0	massive	very firm	

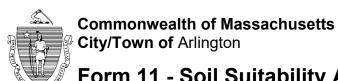
Additional Notes:

TP-3 Elevation = 6.5. Groundwater observed at bottom of test pit (12') and weeping from sides at 7' - estimated groundwater elevation = -0.5



Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

Deep Observation Land Use: 76	on Hole Num	ber:								
Land Use:		Hole #	Da	ite	Time	Wea	ather	Latitude		Longitude:
(6	.g., woodland, agı	icultural field, va	cant lot, etc	.) Ve	getation		Surface Sto	nes (e.g., cobbles,	stones, boulders, e	etc.) Slope (%)
Description of Lo	ocation:									
Soil Parent Mate	rial: ———					Landform			Position on Lands	cape (SU, SH, BS, FS, 1
Distances from:	Open Wate	er Body	feet		Drain	age Way _	feet	Wetla	inds fee	et
	Proper	ty Line	feet	[Orinking W	ater Well _	feet	Ot	her fee	et
Materials Present Groundwater Ob			☐ Distu	rbed Soil		f yes:	☐ Weathered/ _ Depth Weepin	Fractured Rock		standing Water in Hole
			Badas	vim ovebio Fo		il Log Coarse I	- Fragments		C-ii	
pth (in) Soil Horizo	on Soil Texture (USDA)	Soil Matrix: Color-Moist	Redox	kimorphic Fe	eatures		Volume Cobbles &	Soil Structure	Soil Consistence	Other
/Luyer	(GGDA)	(Munsell)	Depth	Color	Percent	Gravel	Stones		(Moist)	
Additional Notes			<u> </u>		1			1		



Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

D. Determination of High Groundwater Elevation

1. M	ethod Used: Depth observed standing water in observation	hole	Obs. Hole # <u>TP-3</u> <u>132</u> inches	(_	Obs. Hole # inches	
\triangleright	Depth weeping from side of observation hole		84 inches	_	inches	
	Depth to soil redoximorphic features (mottles)		inches	-	inches	
	Depth to adjusted seasonal high groundwater (USGS methodology)	(S _h)	inches	_	inches	
	Index Well Number	Reading Date			_	
	$S_h = S_c - [S_r \times (OW_c - OW_{max})/OW_r]$					
	Obs. Hole/Well# S _c	S _r	OW _c	OW _{max}	OW _r	S _h
2. Est	imated Depth to High Groundwater: <u>84</u> inches					
E. D	epth of Pervious Material					
1. D	epth of Naturally Occurring Pervious Material					
	Does at least four feet of naturally occurring poststem?	ervious material exis	st in all areas observed	l throughou	it the area proposed for	the soil absorption
	☐ Yes					
b.	If yes, at what depth was it observed (exclude orizons)?	A and O	Upper boundary:	inches	Lower boundary:	inches
C.	If no, at what depth was impervious material o	bserved?	Upper boundary:	84 inches	Lower boundary:	132 inches



F. Certification

I certify that I am currently approved by the Department of Environmental Protection pursuant to 310 CMR 15.017 to conduct soil evaluations and that the above analysis has been performed by me consistent with the required training, expertise and experience described in 310 CMR 15.017. I further certify that the results of my soil evaluation, as indicated in the attached Soil Evaluation Form, are accurate and in accordance with 310 CMR 15.100 through 15.107.

	11/25/2020
Signature of Soil Evaluator	Date
Emily Derrig SE14158	12/1/2020
Typed or Printed Name of Soil Evaluator / License #	Expiration Date of License
Name of Approving Authority Witness	Approving Authority

Note: In accordance with 310 CMR 15.018(2) this form must be submitted to the approving authority within 60 days of the date of field testing, and to the designer and the property owner with <u>Percolation Test Form 12</u>.

Field Diagrams: Use this area for field diagrams: